ATTACHMENT D

Laboratory Reports

SECTION 3.3

- Soil Analytical Summary Table
  (Laboratory issued data reports available upon request)

SECTION 3.7

- Grain Size Distribution

SECTION 3.8

- Kemron 2006 Solids Dewatering Report
  "Hudson River Dewatering Study"
  Kemron 2014 Solids Dewatering Report
- Kemron 2014 Solids Dewatering Report
  "Dewatering Bench Scale Study"
- Kemron 2015 Treatability Study Report:
  "Phase II Soil and Water Bench Scale Treatability Study"

HALEY ALDRICH

SECTION 3.3
SOIL ANALYTICAL SUMMARY TABLE

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NA-101	0 - 2 (ft)	10/28/2013	FD	-	-	-	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	0.337	ND (0.0557)	0.337
NA-101	0 - 2 (ft)	10/28/2013	N	-	-	-	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	23.7 P	ND (11.2)	223	77.3	324
NA-101	10 - 12 (ft)	10/28/2013	N	-	-	-	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	0.223	ND (0.0592)	0.223
NA-101	12 - 14 (ft)	10/28/2013	N	-	-	-	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)
NA-101	4 - 6 (ft)	5/30/2014	N	-	-	-	ND (0.596)	ND (0.596)	ND (0.596)	ND (0.596)	ND (0.596)	2.98	ND (0.596)	9.41	ND (0.596)	12.39
NA-101	6 - 8 (ft)	10/28/2013	N	-	-	-	ND (0.0551)	ND (0.0551)	ND (0.0551)	0.0778	ND (0.0551)	0.124 P	ND (0.0551)	0.597	ND (0.0551)	0.7988
NA-101	8 - 10 (ft)	10/28/2013	N	-	-	-	ND (0.747)	ND (0.747)	ND (0.747)	ND (0.747)	ND (0.747)	ND (0.747)	ND (0.747)	15	ND (0.747)	15
NA-102	0 - 2 (ft)	10/28/2013	N	-	-	-	ND (3.47)	ND (3.47)	ND (3.47)	ND (3.47)	ND (3.47)	ND (3.47)	ND (3.47)	89.1	46.4	135.5
NA-102	10 - 12 (ft)	10/28/2013	N	-	-	-	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	0.107	ND (0.0624)	0.107
NA-102	2 - 4 (ft)	5/30/2014	FD	-	-	-	ND (4.72)	ND (4.72)	ND (4.72)	ND (4.72)	ND (4.72)	ND (4.72)	ND (4.72)	106	ND (4.72)	106
NA-102	2 - 4 (ft)	5/30/2014	N	-	-	-	ND (4.78)	ND (4.78)	ND (4.78)	ND (4.78)	ND (4.78)	ND (4.78)	ND (4.78)	123	ND (4.78)	123
NA-102	4 - 6 (ft)	5/30/2014	N	-	-	-	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	1.28	ND (0.544)	4.88	ND (0.544)	6.16
NA-102	6 - 8 (ft)	10/28/2013	N	-	-	-	ND (0.419)	ND (0.419)	ND (0.419)	ND (0.419)	ND (0.419)	1.3 P	ND (0.419)	4.1	ND (0.419)	5.4
NA-102	8 - 10 (ft)	10/28/2013	N	-	-	-	ND (0.185)	ND (0.185)	ND (0.185)	ND (0.185)	ND (0.185)	ND (0.185)	ND (0.185)	3.04	ND (0.185)	3.04
NA-201	0 - 2 (ft)	5/30/2014	N	-	-	-	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	2.4	ND (0.558)	10.2	ND (0.558)	12.6
NA-201	10 - 12 (ft)	5/30/2014	N	-	-	-	ND (0.0648)	ND (0.0648)	ND (0.0648)	ND (0.0648)	ND (0.0648)	ND (0.0648)	ND (0.0648)	ND (0.0648)	ND (0.0648)	ND (0.0648)
NA-201	2 - 4 (ft)	5/30/2014	N	-	-	-	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)
NA-201	4 - 6 (ft)	5/30/2014	N	-	-	-	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	0.188	ND (0.0585)	0.91	ND (0.0585)	1.098
NA-202	2 - 4 (ft)	5/30/2014	N	-	-	-	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)
NA-202	4 - 6 (ft)	5/30/2014	N	-	-	-	ND (0.337)	ND (0.337)	ND (0.337)	ND (0.337)	ND (0.337)	0.822	ND (0.337)	4.92	ND (0.337)	5.742
NA-203	2 - 4 (ft)	5/30/2014	N	-	-	-	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)
NA-204	10 - 12 (ft)	5/30/2014	N	-	-	-	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)
NA-204	4 - 6 (ft)	5/30/2014	N	-	-	-	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)
NA-204	8 - 10 (ft)	5/30/2014	N	-	-	-	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	0.0932	ND (0.0632)	0.0932
NA-301	0 - 2 (ft)	6/9/2014	FD	-	-	-	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)
NA-301	0 - 2 (ft)	6/9/2014	N	-	-	-	ND (0.571)	ND (0.571)	ND (0.571)	ND (0.571)	ND (0.571)	ND (0.571)	ND (0.571)	8.21	ND (0.571)	8.21
NA-302	0 - 2 (ft)	6/9/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	1.29	ND (0.109)	1.29
NB-001	10 - 12 (ft)	10/28/2013	N	-	-	-	ND (0.136)	ND (0.136)	ND (0.136)	ND (0.136)	ND (0.136)	ND (0.136)	ND (0.136)	1.3	ND (0.136)	1.3
NB-001	12 - 14 (ft)	10/28/2013	N	-	-	-	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)
NB-001	6 - 8 (ft)	10/28/2013	N	-	-	-	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	1.22 P	ND (0.341)	6.65	ND (0.341)	7.87
NB-001	8 - 10 (ft)	10/28/2013	N	-	-	-	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.47	ND (0.127)	2.29	ND (0.127)	2.76
NC-001	6 - 8 (ft)	11/11/2013	N	-	-	-	ND (0.433)	ND (0.433)	ND (0.433)	ND (0.433)	ND (0.433)	1.47 P	ND (0.433)	8.1	2.66	12.23
NC-001	8 - 10 (ft)	11/11/2013	N	-	-	-	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0805)	ND (0.0878)	ND (0.0805)
NC-002	10 - 12 (ft)	11/11/2013	N	-	-	-	ND (0.685)	ND (0.685)	ND (0.685)	ND (0.685)	ND (0.685)	1.38 P	ND (0.685)	18.3	6.4	26.08
NC-002	12 - 14 (ft)	11/11/2013	N	-	-	-	ND (0.0682)	ND (0.0682)	ND (0.0682)	ND (0.0682)	ND (0.0682)	ND (0.0682)	ND (0.0682)	ND (0.0682)	ND (0.0682)	ND (0.0682)
NC-002	6 - 8 (ft)	11/11/2013	FD	-	-	-	ND (6.68)	ND (6.68)	ND (6.68)	ND (6.68)	ND (6.68)	11.5 P	ND (6.68)	211	67.4	289.9
NC-002	6 - 8 (ft)	11/11/2013	N	-	-	-	ND (6.65)	ND (6.65)	ND (6.65)	ND (6.65)	ND (6.65)	13.1 P	ND (6.65)	219	72.2	304.3
NC-002	8 - 10 (ft)	11/11/2013	N	-	-	-	ND (1.4)	ND (1.4)	ND (1.4)	ND (1.4)	ND (1.4)	ND (1.4)	ND (1.4)	40.2	ND (1.4)	40.2
NC-003	6 - 8 (ft)	11/11/2013	N	-	-	-	ND (3.32)	ND (3.32)	ND (3.32)	ND (3.32)	ND (3.32)	ND (3.32)	ND (3.32)	84	ND (3.32)	84
NC-003	8 - 10 (ft)	11/11/2013	N	-	-	-	ND (0.0773)	ND (0.0773)	ND (0.0773)	ND (0.0773)	ND (0.0773)	0.282 P	ND (0.0773)	1.33	0.432	2.044
NC-004	2 - 4 (ft)	10/15/2013	N	-	-	-	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NC-004	4 - 6 (ft)	10/15/2013	N	-	-	-	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)
NC-101	0 - 2 (ft)	10/14/2013	N	-	-	-	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	28.5	ND (1.14)	28.5
NC-102	0 - 2 (ft)	10/14/2013	N	-	-	-	ND (1.66)	ND (1.66)	ND (1.66)	ND (1.66)	ND (1.66)	ND (1.66)	ND (1.66)	49.7	ND (1.66)	49.7
NC-102	10 - 12 (ft)	6/26/2014	FD	-	-	-	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	3.16	ND (0.194)	3.16
NC-102	10 - 12 (ft)	6/26/2014	N	-	-	-	ND (0.203)	ND (0.203)	ND (0.203)	ND (0.203)	ND (0.203)	ND (0.203)	ND (0.203)	2.53	ND (0.203)	2.53
NC-103	0 - 2 (ft)	10/14/2013	N	-	-	-	ND (1.72)	ND (1.72)	ND (1.72)	ND (1.72)	ND (1.72)	ND (1.72)	ND (1.72)	43.1	ND (1.72)	43.1
NC-104	0 - 2 (ft)	10/14/2013	N	-	-	-	ND (4.41)	ND (4.41)	ND (4.41)	ND (4.41)	ND (4.41)	ND (4.41)	ND (4.41)	143	ND (4.41)	143
NC-105	4 - 6 (ft)	10/22/2013	N	-	-	-	ND (4.33)	ND (4.33)	ND (4.33)	ND (4.33)	ND (4.33)	ND (4.33)	ND (4.33)	102	ND (4.33)	102
NC-108	6 - 8 (ft)	11/21/2013	N	-	-	-	ND (2.09)	ND (2.09)	ND (2.09)	ND (2.09)	ND (2.09)	10.1 P	ND (2.09)	51	16.8	77.9
NC-108	8 - 10 (ft)	11/21/2013	N	-	-	-	ND (0.154)	ND (0.154)	ND (0.154)	ND (0.154)	ND (0.154)	ND (0.154)	ND (0.154)	0.464	ND (0.154)	0.464
NC-114	10.5 - 12.5 (ft)	11/16/2013	N	-	-	-	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	0.0789	ND (0.0608)	0.0789
NC-114	8.5 - 10.5 (ft)	11/16/2013	FD	-	-	-	ND (0.694)	ND (0.694)	ND (0.694)	ND (0.694)	ND (0.694)	2.78 P	ND (0.694)	12.3	3.36	18.44
NC-114	8.5 - 10.5 (ft)	11/16/2013	N	-	-	-	ND (0.631)	ND (0.631)	ND (0.631)	ND (0.631)	ND (0.631)	2.35 P	ND (0.631)	10.9	2.94	16.19
NC-115	8 - 10 (ft)	11/16/2013	FD	-	-	-	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	0.0974 P	ND (0.06)	0.564	0.168	0.8294
NC-115	8 - 10 (ft)	11/16/2013	N	-	-	-	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	0.259	0.078	0.337
NC-116	8 - 10 (ft)	11/16/2013	FD	-	-	-	ND (0.0579)	ND (0.0579)	ND (0.0579)	ND (0.0579)	0.268	0.195 P	ND (0.0579)	0.719	0.209	1.391
NC-116	8 - 10 (ft)	11/16/2013	N	-	-	-	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	0.281 P	ND (0.056)	1.35	0.403	2.034
NC-117	6 - 8 (ft)	11/18/2013	FD	-	-	-	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	0.268	0.0896	0.3576
NC-117	6 - 8 (ft)	11/18/2013	N	-	-	-	ND (0.0613)	ND (0.0613)	ND (0.0613)	ND (0.0613)	ND (0.0613)	ND (0.0613)	ND (0.0613)	0.358	0.111	0.469
NC-117	8 - 10 (ft)	11/18/2013	N	-	-	-	ND (0.0622)	ND (0.0622)	ND (0.0622)	ND (0.0622)	ND (0.0622)	ND (0.0622)	ND (0.0622)	ND (0.0622)	ND (0.0622)	ND (0.0622)
NC-118	10 - 12 (ft)	11/18/2013	N	-	-	-	ND (0.079)	ND (0.079)	ND (0.079)	ND (0.079)	ND (0.079)	ND (0.079)	ND (0.079)	ND (0.079)	ND (0.079)	ND (0.079)
NC-118	6 - 8 (ft)	11/18/2013	FD	-	-	-	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	0.84	0.227	1.067
NC-118	6 - 8 (ft)	11/18/2013	N	-	-	-	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	0.975	0.286	1.261
NC-118	8 - 10 (ft)	11/18/2013	N	-	-	-	ND (0.085)	ND (0.085)	ND (0.085)	ND (0.085)	ND (0.085)	ND (0.085)	ND (0.085)	ND (0.085)	ND (0.085)	ND (0.085)
NC-119	6.5 - 8.5 (ft)	11/16/2013	N	-	-	-	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	0.425 P	ND (0.0586)	2.09	0.655	3.17
NC-120	6 - 8 (ft)	11/21/2013	FD	-	-	-	ND (0.368)	ND (0.368)	ND (0.368)	ND (0.368)	ND (0.368)	1.37 P	ND (0.368)	7.16	2.16	10.69
NC-120	6 - 8 (ft)	11/21/2013	N	-	-	-	ND (0.373)	ND (0.373)	ND (0.373)	ND (0.373)	ND (0.373)	1.22 P	ND (0.373)	6.64	1.97	9.83
NC-120	8 - 10 (ft)	11/21/2013	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.127	ND (0.11)	0.127
NC-201	10 - 12 (ft)	6/3/2014	N	-	-	-	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	0.122	ND (0.0588)	0.122
NC-201	8 - 10 (ft)	6/3/2014	N	-	-	-	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	0.542	ND (0.126)	0.542
NC-202	6 - 8 (ft)	6/2/2014	FD	-	-	-	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	3.16	ND (0.166)	3.16
NC-202	6 - 8 (ft)	6/2/2014	N	-	-	-	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	2.46	ND (0.165)	2.46
NC-203	0 - 2 (ft)	5/29/2014	N	-	-	-	ND (0.222)	ND (0.222)	ND (0.222)	ND (0.222)	ND (0.222)	ND (0.222)	ND (0.222)	2.77	ND (0.222)	2.77
NC-203	6 - 8 (ft)	6/2/2014	N	-	-	-	ND (0.311)	ND (0.311)	ND (0.311)	ND (0.311)	ND (0.311)	1.4	ND (0.311)	4.9	ND (0.311)	6.3
NC-204	0 - 2 (ft)	5/30/2014	FD	-	-	-	ND (0.27)	ND (0.27)	ND (0.27)	ND (0.27)	ND (0.27)	0.895	ND (0.27)	3.98	ND (0.27)	4.875
NC-204	0 - 2 (ft)	5/30/2014	N	-	-	-	ND (1.65)	ND (1.65)	ND (1.65)	ND (1.65)	ND (1.65)	ND (1.65)	ND (1.65)	32	ND (1.65)	32
NC-204	2 - 4 (ft)	6/10/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.668	ND (0.114)	0.668
NC-205	0 - 2 (ft)	5/29/2014	N	-	-	-	ND (0.37)	ND (0.37)	ND (0.37)	ND (0.37)	ND (0.37)	ND (0.37)	ND (0.37)	5.35	ND (0.37)	5.35
NC-205	4 - 6 (ft)	5/29/2014	FD	-	-	-	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	0.469	ND (0.261)	3.75	ND (0.261)	4.219
NC-205	4 - 6 (ft)	5/29/2014	N	-	-	-	ND (0.21)	ND (0.21)	ND (0.21)	ND (0.21)	ND (0.21)	0.428	ND (0.21)	3.79	ND (0.21)	4.218
NC-205	6 - 8 (ft)	5/29/2014	N	-	-	-	ND (0.456)	ND (0.456)	ND (0.456)	ND (0.456)	ND (0.456)	ND (0.456)	ND (0.456)	7.77	ND (0.456)	7.77

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NC-205	8 - 10 (ft)	6/2/2014	N	-	-	-	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	0.285	ND (0.0586)	0.285
ND-101	4 - 6 (ft)	10/24/2013	N	-	-	-	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)
ND-102	4 - 6 (ft)	10/24/2013	N	-	-	-	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	0.0763	ND (0.0562)	0.0763
ND-102	6 - 8 (ft)	10/24/2013	N	-	-	-	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	0.168	ND (0.0554)	0.168
ND-103	4 - 6 (ft)	10/24/2013	N	-	-	-	ND (5.55)	ND (5.55)	ND (5.55)	ND (5.55)	ND (5.55)	ND (5.55)	ND (5.55)	142	60.1	202.1
ND-103	6 - 8 (ft)	10/24/2013	N	-	-	-	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	29.4 P	12.3	41.7
ND-103	8 - 10 (ft)	11/18/2013	FD	-	-	-	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	0.3	0.0986 P	0.3986
ND-103	8 - 10 (ft)	11/18/2013	N	-	-	-	ND (0.0667)	ND (0.0667)	ND (0.0667)	ND (0.0667)	ND (0.0667)	ND (0.0667)	ND (0.0667)	0.308	0.11 P	0.418
ND-104	4 - 6 (ft)	10/24/2013	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	2.29	0.809	3.099
ND-104	6 - 8 (ft)	10/24/2013	N	-	-	-	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	0.445	ND (0.0616)	0.445
ND-201	4 - 6 (ft)	6/25/2014	N	-	-	-	ND (22.3)	ND (22.3)	ND (22.3)	ND (22.3)	ND (22.3)	ND (22.3)	ND (22.3)	631	ND (22.3)	631
ND-201	6 - 8 (ft)	6/25/2014	N	-	-	-	ND (2.23)	ND (2.23)	ND (2.23)	ND (2.23)	ND (2.23)	ND (2.23)	ND (2.23)	42.8	ND (2.23)	42.8
ND-201	8 - 10 (ft)	6/25/2014	N	-	-	-	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	0.146	ND (0.064)	0.146
ND-202	10 - 12 (ft)	6/25/2014	N	-	-	-	ND (0.307)	ND (0.307)	ND (0.307)	ND (0.307)	ND (0.307)	ND (0.307)	ND (0.307)	3.64	ND (0.307)	3.64
ND-202	4 - 6 (ft)	6/25/2014	N	-	-	-	ND (0.519)	ND (0.519)	ND (0.519)	ND (0.519)	ND (0.519)	ND (0.519)	ND (0.519)	3.58	ND (0.519)	3.58
ND-202	6 - 8 (ft)	6/25/2014	N	-	-	-	ND (0.134)	ND (0.134)	ND (0.134)	ND (0.134)	ND (0.134)	ND (0.134)	ND (0.134)	1.29	ND (0.134)	1.29
NE-101	0 - 2 (ft)	10/24/2013	N	-	-	-	ND (31.8)	ND (31.8)	ND (31.8)	ND (31.8)	ND (31.8)	ND (31.8)	1220	ND (31.8)	ND (31.8)	1220
NE-101	2 - 4 (ft)	10/24/2013	N	-	-	-	ND (0.278)	ND (0.278)	ND (0.278)	ND (0.278)	ND (0.278)	ND (0.278)	8.46	ND (0.278)	ND (0.278)	8.46
NE-102	0 - 2 (ft)	10/24/2013	N	-	-	-	ND (0.509)	ND (0.509)	ND (0.509)	ND (0.509)	ND (0.509)	ND (0.509)	ND (0.509)	14.8	4.78	19.58
NE-102	2 - 4 (ft)	10/24/2013	N	-	-	-	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)
NE-103	0 - 2 (ft)	10/24/2013	N	-	-	-	ND (2.07)	ND (2.07)	ND (2.07)	ND (2.07)	ND (2.07)	29.9	ND (2.07)	45.3	11.7	86.9
NE-103	2 - 4 (ft)	10/24/2013	N	-	-	-	ND (0.0523)	ND (0.0523)	ND (0.0523)	ND (0.0523)	ND (0.0523)	ND (0.0523)	ND (0.0523)	0.119	ND (0.0523)	0.119
NE-104	0 - 2 (ft)	11/14/2013	N	-	-	-	ND (0.526)	ND (0.526)	ND (0.526)	ND (0.526)	ND (0.526)	ND (0.526)	ND (0.526)	16.7	6.15	22.85
NE-104	2 - 4 (ft)	10/24/2013	N	-	-	-	ND (0.409)	ND (0.409)	ND (0.409)	ND (0.409)	ND (0.409)	ND (0.409)	ND (0.409)	11	3.63	14.63
NE-104	6 - 8 (ft)	6/25/2014	FD	-	-	-	ND (0.0662)	ND (0.0662)	ND (0.0662)	ND (0.0662)	ND (0.0662)	ND (0.0662)	ND (0.0662)	0.109	ND (0.0662)	0.109
NE-104	6 - 8 (ft)	6/25/2014	N	-	-	-	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	0.0972	ND (0.0656)	0.0972
NE-201	0 - 2 (ft)	6/10/2014	N	-	-	-	ND (1.07)	ND (1.07)	ND (1.07)	ND (1.07)	ND (1.07)	ND (1.07)	ND (1.07)	22.4	ND (1.07)	22.4
NE-201	2 - 4 (ft)	7/8/2014	N	-	-	-	ND (0.334)	ND (0.334)	ND (0.334)	ND (0.334)	ND (0.334)	ND (0.334)	ND (0.334)	4.95	1.66	6.61
NE-202	0 - 2 (ft)	6/10/2014	FD	-	-	-	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	10.2	ND (1.14)	10.2
NE-202	0 - 2 (ft)	6/10/2014	N	-	-	-	ND (0.0534)	ND (0.0534)	ND (0.0534)	ND (0.0534)	ND (0.0534)	0.0767	ND (0.0534)	0.088	ND (0.0534)	0.1647
NE-202	2 - 4 (ft)	7/8/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.0973 J	ND (0.115)	1.78	ND (0.115)	1.8773
NE-203	0 - 2 (ft)	6/25/2014	N	-	-	-	ND (0.538)	ND (0.538)	ND (0.538)	ND (0.538)	ND (0.538)	ND (0.538)	ND (0.538)	11	ND (0.538)	11
NE-203	4 - 6 (ft)	6/25/2014	N	-	-	-	ND (0.0537)	ND (0.0537)	ND (0.0537)	ND (0.0537)	ND (0.0537)	ND (0.0537)	ND (0.0537)	0.484	0.176	0.66
NE-203	6 - 8 (ft)	6/25/2014	N	-	-	-	ND (6.37)	ND (6.37)	ND (6.37)	ND (6.37)	ND (6.37)	ND (6.37)	ND (6.37)	126	46.1	172.1
NE-203	8 - 10 (ft)	6/25/2014	N	-	-	-	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	0.0464 J	ND (0.063)	0.0464 J
NE-204	0 - 2 (ft)	6/25/2014	N	-	-	-	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	18.3	ND (1.09)	13.5	ND (1.09)	31.8
NE-204	2 - 4 (ft)	6/25/2014	N	-	-	-	ND (0.0559)	ND (0.0559)	ND (0.0559)	ND (0.0559)	ND (0.0559)	0.495	ND (0.0559)	0.96	ND (0.0559)	1.455
NE-204	4 - 6 (ft)	6/25/2014	N	-	-	-	ND (0.0693)	ND (0.0693)	ND (0.0693)	ND (0.0693)	ND (0.0693)	ND (0.0693)	ND (0.0693)	0.193	ND (0.0693)	0.193
NE-204	6 - 8 (ft)	6/25/2014	N	-	-	-	ND (0.0761)	ND (0.0761)	ND (0.0761)	ND (0.0761)	ND (0.0761)	ND (0.0761)	ND (0.0761)	0.0474 J	ND (0.0761)	0.0474 J
NE-301	0 - 2 (ft)	7/9/2014	N	-	-	-	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	3.13	ND (0.108)	3.13
NF-101	10 - 12 (ft)	11/22/2013	N	-	-	-	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NF-101	4 - 6 (ft)	11/22/2013	FD	-	-	-	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)
NF-101	4 - 6 (ft)	11/22/2013	N	-	-	-	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)
NF-102	10 - 12 (ft)	11/22/2013	N	-	-	-	ND (0.13)	ND (0.13)	ND (0.13)	ND (0.13)	ND (0.13)	ND (0.13)	ND (0.13)	0.21	ND (0.13)	0.21
NF-102	4 - 6 (ft)	11/22/2013	N	-	-	-	ND (0.052)	ND (0.052)	ND (0.052)	ND (0.052)	ND (0.052)	ND (0.052)	0.0647	ND (0.052)	ND (0.052)	0.0647
NF-202	0 - 2 (ft)	6/2/2014	FD	-	-	-	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	1.95	ND (0.106)	1.95
NF-202	0 - 2 (ft)	6/2/2014	N	-	-	-	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	1.64	ND (0.107)	1.64
NG-001	10 - 12 (ft)	11/8/2013	N	-	-	-	ND (0.681)	ND (0.681)	ND (0.681)	ND (0.681)	ND (0.681)	1.97 P	ND (0.681)	8.7	ND (0.681)	10.67
NG-001	12 - 14 (ft)	11/8/2013	N	-	-	-	ND (0.0735)	ND (0.0735)	ND (0.0735)	ND (0.0735)	ND (0.0735)	0.0793 P	ND (0.0735)	0.787	ND (0.0735)	0.8663
NG-101	10 - 12 (ft)	11/15/2013	FD	-	-	-	ND (0.304)	ND (0.304)	ND (0.304)	ND (0.304)	ND (0.304)	0.619 P	ND (0.304)	5.85	ND (0.304)	6.469
NG-101	10 - 12 (ft)	11/15/2013	N	-	-	-	ND (0.312)	ND (0.312)	ND (0.312)	ND (0.312)	ND (0.312)	0.53 P	ND (0.312)	5.63	ND (0.312)	6.16
NG-102	10 - 12 (ft)	11/15/2013	FD	-	-	-	ND (0.0655)	ND (0.0655)	ND (0.0655)	ND (0.0655)	ND (0.0655)	0.271 P	ND (0.0655)	2.17	1.16	3.601
NG-102	10 - 12 (ft)	11/15/2013	N	-	-	-	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.246 P	ND (0.127)	2.07	ND (0.127)	2.316
NG-103	10 - 12 (ft)	11/14/2013	FD	-	-	-	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	4.97	ND (0.288)	4.97
NG-103	10 - 12 (ft)	11/14/2013	N	-	-	-	ND (0.57)	ND (0.57)	ND (0.57)	ND (0.57)	ND (0.57)	ND (0.57)	ND (0.57)	8.17	ND (0.57)	8.17
NG-104	10 - 12 (ft)	11/15/2013	FD	-	-	-	ND (0.173)	ND (0.173)	ND (0.173)	ND (0.173)	1.54	4.49	1.13	ND (0.173)	ND (0.173)	7.16
NG-104	10 - 12 (ft)	11/15/2013	N	-	-	-	ND (0.243)	ND (0.243)	ND (0.243)	ND (0.243)	2.09	6.87	1.22	ND (0.243)	ND (0.243)	10.18
NG-201	10 - 12 (ft)	7/9/2014	N	-	-	-	ND (0.547)	ND (0.547)	ND (0.547)	ND (0.547)	ND (0.547)	ND (0.547)	ND (0.547)	12.2	ND (0.547)	12.2
NG-201	12 - 14 (ft)	7/9/2014	N	-	-	-	ND (0.269)	ND (0.269)	ND (0.269)	ND (0.269)	ND (0.269)	ND (0.269)	ND (0.269)	4.31	ND (0.269)	4.31
NG-201	4 - 6 (ft)	7/9/2014	N	-	-	-	ND (5.8)	ND (5.8)	ND (5.8)	ND (5.8)	ND (5.8)	ND (5.8)	ND (5.8)	171	ND (5.8)	171
NG-201	6 - 8 (ft)	7/9/2014	N	-	-	-	ND (4.75)	ND (4.75)	ND (4.75)	ND (4.75)	ND (4.75)	ND (4.75)	ND (4.75)	120	37.5	157.5
NG-201	8 - 10 (ft)	7/9/2014	N	-	-	-	ND (12.3)	ND (12.3)	ND (12.3)	ND (12.3)	ND (12.3)	ND (12.3)	ND (12.3)	261	ND (12.3)	261
NG-202	10 - 12 (ft)	7/9/2014	N	-	-	-	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	2.23	ND (0.0576)	2.23
NG-202	6 - 8 (ft)	7/9/2014	N	-	-	-	ND (66.8)	ND (66.8)	ND (66.8)	ND (66.8)	ND (66.8)	ND (66.8)	ND (66.8)	1710	ND (66.8)	1710
NG-202	8 - 10 (ft)	7/9/2014	N	-	-	-	ND (1.77)	ND (1.77)	ND (1.77)	ND (1.77)	0.911 J	ND (1.77)	ND (1.77)	32	ND (1.77)	32.911
NG-203	10 - 12 (ft)	11/19/2014	N	-	-	-	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	0.0833	ND (0.0586)	ND (0.0586)	0.0833
NG-204	10 - 12 (ft)	11/19/2014	N	-	-	-	ND (1.28)	ND (1.28)	ND (1.28)	ND (1.28)	ND (1.28)	6.63	29.5	ND (1.28)	ND (1.28)	36.13
NG-204	12 - 14 (ft)	11/19/2014	N	-	-	-	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	0.749	ND (0.0601)	0.749
NH-001	2 - 4 (ft)	10/23/2013	N	-	-	-	ND (0.271)	ND (0.271)	ND (0.271)	ND (0.271)	ND (0.271)	ND (0.271)	ND (0.271)	3.87	1.45	5.32
NH-001	4 - 6 (ft)	10/23/2013	N	-	-	-	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)
NH-002	2 - 4 (ft)	11/19/2013	FD	-	-	-	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	10.3	3.46	13.76
NH-002	2 - 4 (ft)	11/19/2013	N	-	-	-	ND (0.286)	ND (0.286)	ND (0.286)	ND (0.286)	ND (0.286)	ND (0.286)	ND (0.286)	8.05	2.8	10.85
NH-002	4 - 6 (ft)	11/19/2013	FD	-	-	-	ND (0.188)	ND (0.188)	ND (0.188)	ND (0.188)	ND (0.188)	ND (0.188)	ND (0.188)	3.89	1.2	5.09
NH-002	4 - 6 (ft)	11/19/2013	N	-	-	-	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	2.36	0.697	3.057
NH-002	6 - 8 (ft)	11/8/2013	N	-	-	-	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	0.364 P	ND (0.129)	4.5	1.4	6.264
NH-002	8 - 10 (ft)	11/8/2013	N	-	-	-	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)
NH-003	2 - 4 (ft)	11/11/2013	N	-	-	-	ND (0.632)	ND (0.632)	ND (0.632)	ND (0.632)	ND (0.632)	ND (0.632)	ND (0.632)	19.9	9.98	29.88
NH-003	4 - 6 (ft)	11/11/2013	FD	-	-	-	ND (0.0573)	ND (0.0573)	ND (0.0573)	ND (0.0573)	ND (0.0573)	ND (0.0573)	ND (0.0573)	0.248 P	ND (0.0573)	0.248
NH-003	4 - 6 (ft)	11/11/2013	N	-	-	-	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	0.539	ND (0.0611)	0.704
NH-101	0 - 2 (ft)	10/28/2013	N	-	-	-	ND (6.35)	ND (6.35)	ND (6.35)	ND (6.35)	ND (6.35)	ND (6.35)	ND (6.35)	203	56.9	259.9
NH-101	2 - 4 (ft)	10/28/2013	N	-	-	-	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	0.0922	ND (0.0588)	0.0922
NH-105	0 - 2 (ft)	10/28/2013	N	-	-	-	ND (233)	ND (233)	ND (233)	ND (233)	ND (233)	9220	ND (233)	ND (233)	ND (233)	9220

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NH-105	10 - 12 (ft)	11/14/2013	FD	-	-	-	ND (0.0804)	ND (0.0804)	ND (0.0804)	ND (0.0804)	ND (0.0804)	0.82	0.229	ND (0.0804)	ND (0.0804)	1.049
NH-105	10 - 12 (ft)	11/14/2013	N	-	-	-	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	0.931	ND (0.0801)	0.376	ND (0.0801)	1.307
NH-105	8 - 10 (ft)	10/28/2013	N	-	-	-	ND (3.72)	ND (3.72)	ND (3.72)	ND (3.72)	ND (3.72)	98.8	ND (3.72)	ND (3.72)	ND (3.72)	98.8
NH-106	0 - 2 (ft)	10/23/2013	N	-	-	-	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	6.35 P	ND (1.14)	24.2	ND (1.14)	30.55
NH-106	2 - 4 (ft)	6/6/2014	N	-	-	-	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	0.276	ND (0.057)	0.276
NH-106	4 - 6 (ft)	10/28/2013	N	-	-	-	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)
NH-106	8 - 10 (ft)	10/28/2013	N	-	-	-	ND (0.0711)	ND (0.0711)	ND (0.0711)	ND (0.0711)	ND (0.0711)	ND (0.0711)	ND (0.0711)	0.794	ND (0.0711)	0.794
NH-107	2 - 4 (ft)	11/20/2013	FD	-	-	-	ND (0.0537)	ND (0.0537)	ND (0.0537)	ND (0.0537)	ND (0.0537)	ND (0.0537)	ND (0.0537)	0.3	ND (0.0537)	0.3
NH-107	2 - 4 (ft)	11/20/2013	N	-	-	-	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	0.217	ND (0.0563)	0.217
NH-108	2 - 4 (ft)	11/20/2013	FD	-	-	-	ND (0.0551)	ND (0.0551)	ND (0.0551)	ND (0.0551)	ND (0.0551)	ND (0.0551)	ND (0.0551)	0.995	0.45	1.445
NH-108	2 - 4 (ft)	11/20/2013	N	-	-	-	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	0.9	ND (0.056)	0.9
NH-109	2 - 4 (ft)	11/20/2013	FD	-	-	-	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	28.7	12.1	40.8
NH-109	2 - 4 (ft)	11/20/2013	N	-	-	-	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	18.7	7.04	25.74
NH-109	4 - 6 (ft)	11/20/2013	N	-	-	-	ND (0.638)	ND (0.638)	ND (0.638)	ND (0.638)	ND (0.638)	ND (0.638)	ND (0.638)	13.7	ND (0.638)	13.7
NH-109	6 - 8 (ft)	11/20/2013	N	-	-	-	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)
NH-110	2 - 4 (ft)	11/20/2013	FD	-	-	-	ND (0.292)	ND (0.292)	ND (0.292)	ND (0.292)	ND (0.292)	ND (0.292)	ND (0.292)	4.89	1.65	6.54
NH-110	2 - 4 (ft)	11/20/2013	N	-	-	-	ND (1.18)	ND (1.18)	ND (1.18)	ND (1.18)	ND (1.18)	ND (1.18)	ND (1.18)	13.3	3.87	17.17
NH-110	4 - 6 (ft)	11/20/2013	N	-	-	-	ND (0.638)	ND (0.638)	ND (0.638)	ND (0.638)	ND (0.638)	ND (0.638)	ND (0.638)	10.4	ND (0.638)	10.4
NH-110	6 - 8 (ft)	11/20/2013	N	-	-	-	ND (0.0646)	ND (0.0646)	ND (0.0646)	ND (0.0646)	ND (0.0646)	ND (0.0646)	ND (0.0646)	0.146	ND (0.0646)	0.146
NH-111	2 - 4 (ft)	11/20/2013	FD	-	-	-	ND (0.0522)	ND (0.0522)	ND (0.0522)	ND (0.0522)	ND (0.0522)	ND (0.0522)	ND (0.0522)	0.199	ND (0.0522)	0.199
NH-111	2 - 4 (ft)	11/20/2013	N	-	-	-	ND (0.0535)	ND (0.0535)	ND (0.0535)	ND (0.0535)	ND (0.0535)	ND (0.0535)	ND (0.0535)	0.172	ND (0.0535)	0.172
NH-112	2 - 4 (ft)	11/20/2013	N	-	-	-	ND (0.0559)	ND (0.0559)	ND (0.0559)	ND (0.0559)	ND (0.0559)	ND (0.0559)	ND (0.0559)	0.117	ND (0.0559)	0.117
NH-112	4 - 6 (ft)	11/20/2013	N	-	-	-	ND (0.0556)	ND (0.0556)	ND (0.0556)	ND (0.0556)	ND (0.0556)	ND (0.0556)	ND (0.0556)	0.118	ND (0.0556)	0.118
NH-113	0 - 2 (ft)	10/23/2013	N	-	-	-	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	353	191	ND (11.5)	ND (11.5)	544
NH-113	4 - 6 (ft)	10/25/2013	N	-	-	-	ND (54.8)	ND (54.8)	ND (54.8)	ND (54.8)	ND (54.8)	ND (54.8)	ND (54.8)	807	ND (54.8)	807
NH-113	6 - 8 (ft)	10/25/2013	N	-	-	-	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	0.221	ND (0.0603)	0.221
NH-113	8 - 10 (ft)	10/25/2013	N	-	-	-	ND (0.0663)	ND (0.0663)	ND (0.0663)	ND (0.0663)	ND (0.0663)	ND (0.0663)	ND (0.0663)	ND (0.0663)	ND (0.0663)	ND (0.0663)
NH-114	0 - 2 (ft)	10/25/2013	N	-	-	-	ND (0.55)	ND (0.55)	ND (0.55)	ND (0.55)	ND (0.55)	5.67	ND (0.55)	11.7	3.55	20.92
NH-114	4 - 6 (ft)	10/25/2013	N	-	-	-	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	0.2	ND (0.0552)	0.2
NH-114	8 - 10 (ft)	10/25/2013	N	-	-	-	ND (0.697)	ND (0.697)	ND (0.697)	ND (0.697)	ND (0.697)	4.84	ND (0.697)	4.77	ND (0.697)	9.61
NH-115	0 - 2 (ft)	10/23/2013	N	-	-	-	ND (2.82)	ND (2.82)	ND (2.82)	ND (2.82)	ND (2.82)	13.4	ND (2.82)	77.5	ND (2.82)	90.9
NH-115	4 - 6 (ft)	10/25/2013	N	-	-	-	ND (67.8)	ND (67.8)	ND (67.8)	ND (67.8)	ND (67.8)	ND (67.8)	ND (67.8)	2130	ND (67.8)	2130
NH-115	6 - 8 (ft)	10/25/2013	N	-	-	-	ND (0.22)	ND (0.22)	ND (0.22)	ND (0.22)	ND (0.22)	ND (0.22)	ND (0.22)	2.54	ND (0.22)	2.54
NH-115	8 - 10 (ft)	10/25/2013	N	-	-	-	ND (0.316)	ND (0.316)	ND (0.316)	ND (0.316)	ND (0.316)	0.88	ND (0.316)	4.75	1.03 P	6.66
NH-116	0 - 2 (ft)	10/18/2013	N	-	-	-	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	275	ND (11.2)	275
NH-116	4 - 6 (ft)	11/19/2013	N	-	-	-	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	4.27	ND (0.231)	4.27
NH-116	6 - 8 (ft)	11/19/2013	N	-	-	-	ND (0.251)	ND (0.251)	ND (0.251)	ND (0.251)	ND (0.251)	ND (0.251)	ND (0.251)	2.86	ND (0.251)	2.86
NH-117	0 - 2 (ft)	10/18/2013	N	-	-	-	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	25.1	ND (1.7)	25.1
NH-117	2 - 4 (ft)	11/19/2013	N	-	-	-	ND (0.354)	ND (0.354)	ND (0.354)	ND (0.354)	ND (0.354)	2.37	ND (0.354)	6.26	2.1	10.73
NH-117	4 - 6 (ft)	11/19/2013	N	-	-	-	ND (16.4)	ND (16.4)	ND (16.4)	ND (16.4)	ND (16.4)	ND (16.4)	ND (16.4)	384	159	543
NH-117	6 - 8 (ft)	11/19/2013	FD	-	-	-	ND (0.654)	ND (0.654)	ND (0.654)	ND (0.654)	ND (0.654)	ND (0.654)	ND (0.654)	22.5	9.03	31.53

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NH-117	6 - 8 (ft)	11/19/2013	N	-	-	-	ND (0.647)	ND (0.647)	ND (0.647)	ND (0.647)	ND (0.647)	ND (0.647)	ND (0.647)	26.6	10.4	37
NH-117	8 - 10 (ft)	11/19/2013	N	-	-	-	ND (0.0681)	ND (0.0681)	ND (0.0681)	ND (0.0681)	ND (0.0681)	ND (0.0681)	ND (0.0681)	0.804	ND (0.0681)	0.804
NH-118	0 - 2 (ft)	10/18/2013	N	-	-	-	ND (35.2)	ND (35.2)	ND (35.2)	ND (35.2)	ND (35.2)	ND (35.2)	ND (35.2)	1140	ND (35.2)	1140
NH-118	2 - 4 (ft)	11/19/2013	N	-	-	-	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	0.532	0.203	0.735
NH-118	4 - 6 (ft)	11/19/2013	N	-	-	-	ND (2.4)	ND (2.4)	ND (2.4)	ND (2.4)	ND (2.4)	ND (2.4)	ND (2.4)	64.6	ND (2.4)	64.6
NH-118	6 - 8 (ft)	11/19/2013	N	-	-	-	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	5.87	ND (0.261)	5.87
NH-119	10 - 12 (ft)	11/19/2013	N	-	-	-	ND (2.08)	ND (2.08)	ND (2.08)	ND (2.08)	ND (2.08)	ND (2.08)	ND (2.08)	45.8	ND (2.08)	45.8
NH-119	12 - 14 (ft)	11/19/2013	N	-	-	-	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	1	ND (0.0863)	1
NH-119	2 - 4 (ft)	11/5/2013	N	-	-	-	ND (0.542)	ND (0.542)	ND (0.542)	ND (0.542)	ND (0.542)	ND (0.542)	ND (0.542)	15.9	6.88	22.78
NH-119	4 - 6 (ft)	11/5/2013	N	-	-	-	ND (18.3)	ND (18.3)	ND (18.3)	ND (18.3)	ND (18.3)	ND (18.3)	ND (18.3)	409	188	597
NH-119	6 - 8 (ft)	11/19/2013	FD	-	-	-	ND (12.6)	ND (12.6)	ND (12.6)	ND (12.6)	ND (12.6)	ND (12.6)	ND (12.6)	429	189	618
NH-119	6 - 8 (ft)	11/19/2013	N	-	-	-	ND (12.5)	ND (12.5)	ND (12.5)	ND (12.5)	ND (12.5)	ND (12.5)	ND (12.5)	375	171	546
NH-119	8 - 10 (ft)	11/19/2013	N	-	-	-	ND (3.2)	ND (3.2)	ND (3.2)	ND (3.2)	ND (3.2)	ND (3.2)	ND (3.2)	122	56.4	178.4
NH-120	2 - 4 (ft)	11/5/2013	N	-	-	-	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	3.41	0.963	4.373
NH-121	2 - 4 (ft)	11/5/2013	N	-	-	-	ND (0.216)	ND (0.216)	ND (0.216)	ND (0.216)	ND (0.216)	ND (0.216)	ND (0.216)	3.02	1.13	4.15
NH-201	4 - 6 (ft)	5/23/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	2.2	ND (0.118)	2.2
NH-202	4 - 6 (ft)	5/23/2014	FD	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	2.96	ND (0.116)	2.96
NH-202	4 - 6 (ft)	5/23/2014	N	-	-	-	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	3.28	ND (0.341)	3.28
NH-203	2 - 4 (ft)	5/22/2014	N	-	-	-	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)
NH-203	4 - 6 (ft)	5/22/2014	FD	-	-	-	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)
NH-203	4 - 6 (ft)	5/22/2014	N	-	-	-	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)
NH-204	2 - 4 (ft)	5/20/2014	FD	-	-	-	ND (0.236)	ND (0.236)	ND (0.236)	ND (0.236)	ND (0.236)	0.26	ND (0.236)	3.63	ND (0.236)	3.89
NH-204	2 - 4 (ft)	5/20/2014	N	-	-	-	ND (0.167)	ND (0.167)	ND (0.167)	ND (0.167)	ND (0.167)	0.167 J	ND (0.167)	2.29	ND (0.167)	2.457
NH-204	4 - 6 (ft)	5/20/2014	N	-	-	-	ND (0.0698)	ND (0.0698)	ND (0.0698)	ND (0.0698)	ND (0.0698)	ND (0.0698)	ND (0.0698)	0.673	ND (0.0698)	0.673
NH-205	0 - 2 (ft)	6/3/2014	N	-	-	-	ND (1.56)	ND (1.56)	ND (1.56)	ND (1.56)	ND (1.56)	4.46	ND (1.56)	32.6	ND (1.56)	37.06
NH-205	2 - 4 (ft)	6/3/2014	N	-	-	-	ND (0.582)	ND (0.582)	ND (0.582)	ND (0.582)	ND (0.582)	ND (0.582)	ND (0.582)	9.3	ND (0.582)	9.3
NH-206	0 - 2 (ft)	5/23/2014	N	-	-	-	ND (5.57)	ND (5.57)	ND (5.57)	ND (5.57)	ND (5.57)	181	ND (5.57)	ND (5.57)	ND (5.57)	181
NH-206	2 - 4 (ft)	5/23/2014	N	-	-	-	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	0.163	ND (0.0547)	0.163
NH-207	0 - 2 (ft)	6/5/2014	FD	-	-	-	ND (5.62)	ND (5.62)	ND (5.62)	ND (5.62)	ND (5.62)	68.4	ND (5.62)	67	ND (5.62)	135.4
NH-207	0 - 2 (ft)	6/5/2014	N	-	-	-	ND (3.35)	ND (3.35)	ND (3.35)	ND (3.35)	ND (3.35)	63.2	ND (3.35)	68.8	ND (3.35)	132
NH-207	2 - 4 (ft)	6/5/2014	N	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	2.16	ND (0.105)	1.22	ND (0.105)	3.38
NH-207	4 - 6 (ft)	6/5/2014	N	-	-	-	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)
NH-208	0 - 2 (ft)	6/5/2014	N	-	-	-	ND (56.5)	ND (56.5)	ND (56.5)	ND (56.5)	ND (56.5)	ND (56.5)	ND (56.5)	2680	ND (56.5)	2680
NH-208	2 - 4 (ft)	6/5/2014	N	-	-	-	ND (16.9)	ND (16.9)	ND (16.9)	ND (16.9)	ND (16.9)	ND (16.9)	ND (16.9)	298	ND (16.9)	298
NH-208	4 - 6 (ft)	6/5/2014	N	-	-	-	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	0.809	ND (0.057)	0.809
NH-209	0 - 2 (ft)	6/6/2014	N	-	-	-	ND (1.63)	ND (1.63)	ND (1.63)	ND (1.63)	ND (1.63)	6.57	ND (1.63)	26.9	8.05	41.52
NH-209	10 - 12 (ft)	6/6/2014	N	-	-	-	ND (0.0687)	ND (0.0687)	ND (0.0687)	ND (0.0687)	ND (0.0687)	ND (0.0687)	ND (0.0687)	0.0785	ND (0.0687)	0.0785
NH-209	2 - 4 (ft)	6/6/2014	N	-	-	-	ND (0.0613)	ND (0.0613)	ND (0.0613)	ND (0.0613)	ND (0.0613)	ND (0.0613)	ND (0.0613)	0.206	ND (0.0613)	0.206
NH-209	4 - 6 (ft)	6/6/2014	N	-	-	-	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	0.595	ND (0.0567)	0.595
NH-209	6 - 8 (ft)	6/6/2014	N	-	-	-	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	0.433	0.186	0.619
NH-210	10 - 12 (ft)	6/6/2014	N	-	-	-	ND (0.0795)	ND (0.0795)	ND (0.0795)	ND (0.0795)	ND (0.0795)	ND (0.0795)	ND (0.0795)	0.744	ND (0.0795)	0.744

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AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NH-210	2 - 4 (ft)	6/6/2014	FD	-	-	-	ND (17)	ND (17)	ND (17)	ND (17)	ND (17)	ND (17)	ND (17)	473	ND (17)	473
NH-210	2 - 4 (ft)	6/6/2014	N	-	-	-	ND (5.88)	ND (5.88)	ND (5.88)	ND (5.88)	ND (5.88)	ND (5.88)	ND (5.88)	182	ND (5.88)	182
NH-210	4 - 6 (ft)	6/6/2014	N	-	-	-	ND (0.604)	ND (0.604)	ND (0.604)	ND (0.604)	ND (0.604)	ND (0.604)	ND (0.604)	12.6	ND (0.604)	12.6
NH-210	6 - 8 (ft)	6/6/2014	N	-	-	-	ND (0.66)	ND (0.66)	ND (0.66)	ND (0.66)	ND (0.66)	ND (0.66)	ND (0.66)	19.5	ND (0.66)	19.5
NH-210	8 - 10 (ft)	6/6/2014	N	-	-	-	ND (0.307)	ND (0.307)	ND (0.307)	ND (0.307)	ND (0.307)	ND (0.307)	ND (0.307)	3.88	ND (0.307)	3.88
NH-211	10 - 12 (ft)	6/6/2014	FD	-	-	-	ND (0.249)	ND (0.249)	ND (0.249)	ND (0.249)	ND (0.249)	ND (0.249)	ND (0.249)	3.32	ND (0.249)	3.32
NH-211	10 - 12 (ft)	6/6/2014	N	-	-	-	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	4.24	ND (0.341)	4.24
NH-211	2 - 4 (ft)	6/6/2014	N	-	-	-	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	28.3	ND (1.12)	28.3
NH-211	4 - 6 (ft)	6/6/2014	N	-	-	-	ND (0.649)	ND (0.649)	ND (0.649)	ND (0.649)	ND (0.649)	ND (0.649)	ND (0.649)	15.7	ND (0.649)	15.7
NH-211	6 - 8 (ft)	6/6/2014	N	-	-	-	ND (3.39)	ND (3.39)	ND (3.39)	ND (3.39)	ND (3.39)	ND (3.39)	ND (3.39)	88.3	ND (3.39)	88.3
NH-211	8 - 10 (ft)	6/6/2014	N	-	-	-	ND (0.397)	ND (0.397)	ND (0.397)	ND (0.397)	ND (0.397)	ND (0.397)	ND (0.397)	7.14	3.09	10.23
NH-212	0 - 2 (ft)	6/4/2014	FD	-	-	-	ND (109)	ND (109)	ND (109)	ND (109)	ND (109)	ND (109)	ND (109)	2950	ND (109)	2950
NH-212	0 - 2 (ft)	6/4/2014	N	-	-	-	ND (57.2)	ND (57.2)	ND (57.2)	ND (57.2)	ND (57.2)	ND (57.2)	ND (57.2)	2750	ND (57.2)	2750
NH-212	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (58.1)	ND (58.1)	ND (58.1)	ND (58.1)	ND (58.1)	ND (58.1)	ND (58.1)	2120	ND (58.1)	2120
NH-212	4 - 6 (ft)	6/4/2014	N	-	-	-	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	1.01	ND (0.0606)	1.01
NH-213	0 - 2 (ft)	6/5/2014	N	-	-	-	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	803	ND (22.2)	803
NH-213	4 - 6 (ft)	6/5/2014	FD	-	-	-	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	21.2	ND (1.17)	21.2
NH-213	4 - 6 (ft)	6/5/2014	N	-	-	-	ND (0.562)	ND (0.562)	ND (0.562)	ND (0.562)	ND (0.562)	ND (0.562)	ND (0.562)	19.7	ND (0.562)	19.7
NH-213	6 - 8 (ft)	6/5/2014	N	-	-	-	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	0.923	ND (0.0858)	0.923
NH-214	8 - 10 (ft)	6/5/2014	N	-	-	-	ND (0.067)	ND (0.067)	ND (0.067)	ND (0.067)	ND (0.067)	ND (0.067)	ND (0.067)	0.334	ND (0.067)	0.334
NH-215	0 - 2 (ft)	5/22/2014	FD	-	-	-	ND (12.7)	ND (12.7)	ND (12.7)	ND (12.7)	ND (12.7)	ND (12.7)	ND (12.7)	439	ND (12.7)	439
NH-215	0 - 2 (ft)	5/22/2014	N	-	-	-	ND (6.2)	ND (6.2)	ND (6.2)	ND (6.2)	ND (6.2)	ND (6.2)	ND (6.2)	290	ND (6.2)	290
NH-215	2 - 4 (ft)	5/22/2014	N	-	-	-	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	0.881	ND (0.231)	4.32	ND (0.231)	5.201
NH-215	4 - 6 (ft)	5/22/2014	N	-	-	-	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	1.27	ND (0.129)	1.27
NH-301	0 - 2 (ft)	6/10/2014	N	-	-	-	ND (116)	ND (116)	ND (116)	ND (116)	ND (116)	ND (116)	ND (116)	4910	ND (116)	4910
NH-302	0 - 2 (ft)	6/10/2014	N	-	-	-	ND (11.4)	ND (11.4)	ND (11.4)	ND (11.4)	ND (11.4)	ND (11.4)	ND (11.4)	254	ND (11.4)	254
NH-304	0 - 2 (ft)	6/10/2014	N	-	-	-	ND (11.4)	ND (11.4)	ND (11.4)	ND (11.4)	ND (11.4)	ND (11.4)	ND (11.4)	288	ND (11.4)	288
NH-305	0 - 2 (ft)	6/24/2014	N	-	-	-	ND (1.62)	ND (1.62)	ND (1.62)	ND (1.62)	ND (1.62)	8.5	ND (1.62)	29.8	9.23	47.53
NH-305	2 - 4 (ft)	6/24/2014	N	-	-	-	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	0.516	0.215	0.731
NH-305	6 - 8 (ft)	6/24/2014	N	-	-	-	ND (0.622)	ND (0.622)	ND (0.622)	ND (0.622)	ND (0.622)	ND (0.622)	ND (0.622)	7.39	ND (0.622)	7.39
NH-306	0 - 2 (ft)	6/24/2014	N	-	-	-	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	20.2	ND (1.68)	26.9	ND (1.68)	47.1
NH-306	2 - 4 (ft)	6/24/2014	N	-	-	-	ND (0.238)	ND (0.238)	ND (0.238)	ND (0.238)	ND (0.238)	3.91	ND (0.238)	2.05	ND (0.238)	5.96
NH-307	0 - 2 (ft)	6/24/2014	FD	-	-	-	ND (2.87)	ND (2.87)	ND (2.87)	ND (2.87)	ND (2.87)	26.6	ND (2.87)	49.2	ND (2.87)	75.8
NH-307	0 - 2 (ft)	6/24/2014	N	-	-	-	ND (2.23)	ND (2.23)	ND (2.23)	ND (2.23)	ND (2.23)	20.6	ND (2.23)	38.9	ND (2.23)	59.5
NH-307	2 - 4 (ft)	6/24/2014	N	-	-	-	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	3.51	1.47	4.98
NH-308	0 - 2 (ft)	6/24/2014	N	-	-	-	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	22.7	ND (1.09)	22.7
NH-308	2 - 4 (ft)	6/24/2014	N	-	-	-	ND (0.0558)	ND (0.0558)	ND (0.0558)	ND (0.0558)	ND (0.0558)	ND (0.0558)	ND (0.0558)	0.744	ND (0.0558)	0.744
NH-309	0 - 2 (ft)	6/24/2014	N	-	-	-	ND (0.159)	ND (0.159)	ND (0.159)	ND (0.159)	ND (0.159)	ND (0.159)	ND (0.159)	2.02	ND (0.159)	2.02
NH-309	2 - 4 (ft)	6/24/2014	N	-	-	-	ND (5.5)	ND (5.5)	ND (5.5)	ND (5.5)	ND (5.5)	ND (5.5)	ND (5.5)	146	ND (5.5)	146
NH-309	4 - 6 (ft)	6/24/2014	N	-	-	-	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	0.078	ND (0.0574)	0.0466 J	ND (0.0574)	0.1246
NH-310	0 - 2 (ft)	6/23/2014	N	-	-	-	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	339	ND (22.2)	339

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NH-310	2 - 4 (ft)	6/23/2014	N	-	-	-	ND (1.61)	ND (1.61)	ND (1.61)	ND (1.61)	ND (1.61)	2.69	ND (1.61)	31.7	ND (1.61)	34.39
NH-310	4 - 6 (ft)	6/23/2014	N	-	-	-	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	3.46	ND (0.228)	3.46
NH-310	8 - 10 (ft)	6/23/2014	N	-	-	-	ND (0.0564)	ND (0.0564)	ND (0.0564)	ND (0.0564)	ND (0.0564)	ND (0.0564)	ND (0.0564)	0.302	ND (0.0564)	0.302
NH-311	6 - 8 (ft)	6/23/2014	N	-	-	-	ND (0.331)	ND (0.331)	ND (0.331)	ND (0.331)	ND (0.331)	ND (0.331)	ND (0.331)	4.48	ND (0.331)	4.48
NH-311	8 - 10 (ft)	6/23/2014	N	-	-	-	ND (0.218)	ND (0.218)	ND (0.218)	ND (0.218)	ND (0.218)	ND (0.218)	ND (0.218)	2.72	ND (0.218)	2.72
NH-312	2 - 4 (ft)	7/8/2014	N	-	-	-	ND (5.93)	ND (5.93)	ND (5.93)	ND (5.93)	ND (5.93)	ND (5.93)	ND (5.93)	98.7	ND (5.93)	98.7
NH-312	4 - 6 (ft)	7/8/2014	N	-	-	-	ND (0.565)	ND (0.565)	ND (0.565)	ND (0.565)	ND (0.565)	ND (0.565)	ND (0.565)	7.06	ND (0.565)	7.06
NH-312	6 - 8 (ft)	7/8/2014	N	-	-	-	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	4.46	1.55	6.01
NH-312	8 - 10 (ft)	7/8/2014	FD	-	-	-	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	ND (0.0633)	2.03	0.758	2.788
NH-312	8 - 10 (ft)	7/8/2014	N	-	-	-	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	2.37	0.847	3.217
NH-313	0 - 2 (ft)	7/15/2014	N	-	-	-	ND (0.62)	ND (0.62)	ND (0.62)	ND (0.62)	ND (0.62)	ND (0.62)	ND (0.62)	9.61	3.55	13.16
NH-313	2 - 4 (ft)	7/15/2014	N	-	-	-	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)
NH-314	0 - 2 (ft)	7/15/2014	N	-	-	-	ND (0.053)	ND (0.053)	ND (0.053)	ND (0.053)	ND (0.053)	0.0505 J	ND (0.053)	ND (0.053)	ND (0.053)	0.0505 J
NH-314	2 - 4 (ft)	7/15/2014	N	-	-	-	ND (0.37)	ND (0.37)	ND (0.37)	ND (0.37)	ND (0.37)	ND (0.37)	ND (0.37)	5.05	1.84	6.89
NH-315	0 - 2 (ft)	10/24/2014	N	-	-	-	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	23.1	ND (1.15)	23.1
NH-315	2 - 4 (ft)	11/3/2014	N	-	-	-	ND (0.229)	ND (0.229)	ND (0.229)	ND (0.229)	ND (0.229)	ND (0.229)	ND (0.229)	4.81	ND (0.229)	4.81
NH-316	2 - 4 (ft)	10/21/2014	FD	-	-	-	ND (0.0607)	ND (0.0607)	ND (0.0607)	ND (0.0607)	0.049 J	ND (0.0607)	ND (0.0607)	0.722	ND (0.0607)	0.771
NH-316	2 - 4 (ft)	10/21/2014	N	-	-	-	ND (0.0613)	ND (0.0613)	ND (0.0613)	ND (0.0613)	0.0932	ND (0.0613)	ND (0.0613)	0.998	ND (0.0613)	1.091
NH-318	0 - 2 (ft)	11/10/2014	N	-	-	-	ND (17)	ND (17)	ND (17)	ND (17)	99.8	ND (17)	ND (17)	446	ND (17)	546
NH-318	2 - 4 (ft)	11/10/2014	N	-	-	-	ND (5.66)	ND (5.66)	ND (5.66)	ND (5.66)	ND (5.66)	ND (5.66)	ND (5.66)	136	ND (5.66)	136
NH-318	4 - 6 (ft)	11/10/2014	N	-	-	-	ND (0.553)	ND (0.553)	ND (0.553)	ND (0.553)	ND (0.553)	ND (0.553)	ND (0.553)	13.8	ND (0.553)	13.8
NH-318	6 - 8 (ft)	11/10/2014	N	-	-	-	ND (0.575)	ND (0.575)	ND (0.575)	ND (0.575)	ND (0.575)	ND (0.575)	ND (0.575)	10.7	ND (0.575)	10.7
NH-319	0 - 2 (ft)	11/10/2014	N	-	-	-	ND (3.95)	ND (3.95)	ND (3.95)	ND (3.95)	ND (3.95)	ND (3.95)	ND (3.95)	84.1	ND (3.95)	84.1
NH-319	2 - 4 (ft)	11/10/2014	N	-	-	-	ND (0.338)	ND (0.338)	ND (0.338)	ND (0.338)	ND (0.338)	ND (0.338)	ND (0.338)	6.39	ND (0.338)	6.39
NH-319	6 - 8 (ft)	11/10/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	1.21	ND (0.118)	1.21
NH-320	0 - 2 (ft)	10/24/2014	N	-	-	-	ND (0.564)	ND (0.564)	ND (0.564)	ND (0.564)	ND (0.564)	4.23	ND (0.564)	16.2	ND (0.564)	20.43
NH-320	2 - 4 (ft)	11/10/2014	N	-	-	-	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	1.72	ND (0.126)	1.72
NH-321	0 - 2 (ft)	10/24/2014	FD	-	-	-	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	16.3	ND (1.14)	16.3
NH-321	0 - 2 (ft)	10/24/2014	N	-	-	-	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	5.77	ND (1.12)	17.1	ND (1.12)	22.87
NH-321	2 - 4 (ft)	11/6/2014	N	-	-	-	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	0.095	ND (0.0544)	0.306	ND (0.0544)	0.401
NH-322	0 - 2 (ft)	11/10/2014	N	-	-	-	ND (1.58)	ND (1.58)	ND (1.58)	ND (1.58)	ND (1.58)	ND (1.58)	ND (1.58)	29.1	ND (1.58)	29.1
NH-322	2 - 4 (ft)	11/10/2014	N	-	-	-	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	0.379	ND (0.0599)	0.379
NH-323	0 - 2 (ft)	11/6/2014	N	-	-	-	ND (0.532)	ND (0.532)	ND (0.532)	ND (0.532)	ND (0.532)	ND (0.532)	ND (0.532)	3.77	ND (0.532)	3.77
NH-324	0 - 2 (ft)	11/6/2014	N	-	-	-	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	0.434	ND (0.0545)	0.434
NH-325	0 - 2 (ft)	11/18/2014	N	-	-	-	ND (0.0635)	ND (0.0635)	ND (0.0635)	ND (0.0635)	ND (0.0635)	ND (0.0635)	ND (0.0635)	ND (0.0635)	ND (0.0635)	ND (0.0635)
NH-325	8 - 10 (ft)	11/18/2014	N	-	-	-	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)
NH-326	0 - 2 (ft)	11/18/2014	N	-	-	-	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	0.108	ND (0.0546)	0.108
NI-001	10 - 12 (ft)	11/14/2013	N	-	-	-	ND (0.368)	ND (0.368)	ND (0.368)	ND (0.368)	ND (0.368)	ND (0.368)	ND (0.368)	6.75	2.31	9.06
NI-001	12 - 14 (ft)	11/14/2013	FD	-	-	-	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	0.77	ND (0.0923)	0.77
NI-001	12 - 14 (ft)	11/14/2013	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	1.14	0.511	1.651
NI-002	2 - 4 (ft)	11/12/2013	N	-	-	-	ND (1.57)	ND (1.57)	ND (1.57)	ND (1.57)	ND (1.57)	6.55	ND (1.57)	43.9	14.1	64.55

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AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NI-002	4 - 6 (ft)	11/12/2013	FD	-	-	-	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	0.706	0.236	0.942
NI-002	4 - 6 (ft)	11/12/2013	N	-	-	-	ND (0.0551)	ND (0.0551)	ND (0.0551)	ND (0.0551)	ND (0.0551)	ND (0.0551)	ND (0.0551)	0.603	0.205	0.808
NI-101	2 - 4 (ft)	5/28/2014	FD	-	-	-	ND (0.26)	ND (0.26)	ND (0.26)	ND (0.26)	ND (0.26)	ND (0.26)	ND (0.26)	9.29	ND (0.26)	9.29
NI-101	2 - 4 (ft)	5/28/2014	N	-	-	-	ND (0.533)	ND (0.533)	ND (0.533)	ND (0.533)	ND (0.533)	ND (0.533)	ND (0.533)	12.4	ND (0.533)	12.4
NI-101	4 - 6 (ft)	5/28/2014	N	-	-	-	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	288	ND (11.5)	288
NI-101	6 - 8 (ft)	5/28/2014	N	-	-	-	ND (0.0754)	ND (0.0754)	ND (0.0754)	ND (0.0754)	ND (0.0754)	ND (0.0754)	ND (0.0754)	2.66	ND (0.0754)	2.66
NI-101	8 - 10 (ft)	5/28/2014	N	-	-	-	ND (0.328)	ND (0.328)	ND (0.328)	ND (0.328)	ND (0.328)	ND (0.328)	ND (0.328)	5.8	ND (0.328)	5.8
NI-102	4 - 6 (ft)	5/16/2014	N	-	-	-	ND (0.181)	ND (0.181)	ND (0.181)	ND (0.181)	ND (0.181)	ND (0.181)	ND (0.181)	3.1	ND (0.181)	3.1
NI-102	6 - 8 (ft)	6/20/2014	N	-	-	-	ND (0.065)	ND (0.065)	ND (0.065)	ND (0.065)	ND (0.065)	ND (0.065)	ND (0.065)	0.283	ND (0.065)	0.283
NI-103	4 - 6 (ft)	5/28/2014	N	-	-	-	ND (0.0614)	ND (0.0614)	ND (0.0614)	ND (0.0614)	ND (0.0614)	ND (0.0614)	ND (0.0614)	0.144	ND (0.0614)	0.144
NI-103	6 - 8 (ft)	5/28/2014	N	-	-	-	ND (0.152)	ND (0.152)	ND (0.152)	ND (0.152)	ND (0.152)	0.211	ND (0.152)	1.75	ND (0.152)	1.961
NI-104	4 - 6 (ft)	6/19/2014	N	-	-	-	ND (41.9)	ND (41.9)	ND (41.9)	ND (41.9)	ND (41.9)	ND (41.9)	ND (41.9)	963	ND (41.9)	963
NI-104	6 - 8 (ft)	6/19/2014	N	-	-	-	ND (1.33)	ND (1.33)	ND (1.33)	ND (1.33)	ND (1.33)	ND (1.33)	ND (1.33)	29.5	9.59	39.1
NI-104	8 - 10 (ft)	6/19/2014	N	-	-	-	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	0.779	ND (0.0674)	0.779
NI-105	2 - 4 (ft)	5/16/2014	FD	-	-	-	ND (0.554)	ND (0.554)	ND (0.554)	ND (0.554)	ND (0.554)	ND (0.554)	ND (0.554)	15.1	ND (0.554)	15.1
NI-105	2 - 4 (ft)	5/16/2014	N	-	-	-	ND (2.18)	ND (2.18)	ND (2.18)	ND (2.18)	ND (2.18)	ND (2.18)	ND (2.18)	37.8	ND (2.18)	37.8
NI-105	2.5 (ft)	5/16/2014	N	-	-	-	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	0.569	ND (0.221)	5.84	ND (0.221)	6.409
NI-105	4 - 6 (ft)	5/16/2014	N	-	-	-	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	1.05	ND (0.0639)	1.05
NI-106	2 - 4 (ft)	5/15/2014	N	-	-	-	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	29	ND (1.15)	29
NI-106	4 - 6 (ft)	5/15/2014	N	-	-	-	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	0.787	ND (0.0611)	0.787
NI-107	2 - 4 (ft)	5/15/2014	N	-	-	-	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	0.18	ND (0.0563)	0.18
NI-107	4 - 6 (ft)	5/15/2014	N	-	-	-	ND (0.238)	ND (0.238)	ND (0.238)	ND (0.238)	ND (0.238)	ND (0.238)	ND (0.238)	1.53	ND (0.238)	1.53
NI-108	4 - 6 (ft)	5/15/2014	N	-	-	-	ND (4.05)	ND (4.05)	ND (4.05)	ND (4.05)	ND (4.05)	20	ND (4.05)	105	ND (4.05)	125
NI-108	6 - 8 (ft)	5/28/2014	N	-	-	-	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	0.53	ND (0.0771)	0.53
NI-201	2 - 4 (ft)	6/20/2014	FD	-	-	-	ND (2.15)	ND (2.15)	ND (2.15)	ND (2.15)	ND (2.15)	ND (2.15)	ND (2.15)	47.4	ND (2.15)	47.4
NI-201	2 - 4 (ft)	6/20/2014	N	-	-	-	ND (2.68)	ND (2.68)	ND (2.68)	ND (2.68)	ND (2.68)	ND (2.68)	ND (2.68)	47.7	ND (2.68)	47.7
NI-201	4 - 6 (ft)	6/20/2014	N	-	-	-	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	0.854	ND (0.0592)	0.854
NI-201	6 - 8 (ft)	6/20/2014	N	-	-	-	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	0.372	ND (0.0684)	0.372
NI-202	2 - 4 (ft)	6/23/2014	FD	-	-	-	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	24	ND (1.09)	24
NI-202	2 - 4 (ft)	6/23/2014	N	-	-	-	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	38.5	ND (1.71)	38.5
NI-202	4 - 6 (ft)	6/23/2014	N	-	-	-	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	0.277	ND (0.0557)	0.277
NI-202	6 - 8 (ft)	6/23/2014	N	-	-	-	ND (0.2)	ND (0.2)	ND (0.2)	ND (0.2)	ND (0.2)	ND (0.2)	ND (0.2)	1.42	ND (0.2)	1.42
NI-202	8 - 10 (ft)	6/23/2014	N	-	-	-	ND (0.144)	ND (0.144)	ND (0.144)	ND (0.144)	ND (0.144)	ND (0.144)	ND (0.144)	0.627	ND (0.144)	0.627
NI-203	2 - 4 (ft)	6/3/2014	N	-	-	-	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	3.13	ND (1.1)	19.7	ND (1.1)	22.83
NI-203	4 - 6 (ft)	6/3/2014	N	-	-	-	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	0.578	ND (0.0674)	0.578
NI-204	2 - 4 (ft)	6/3/2014	N	-	-	-	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	0.684	ND (0.0574)	0.684
NI-204	4 - 6 (ft)	6/3/2014	N	-	-	-	ND (0.397)	ND (0.397)	ND (0.397)	ND (0.397)	ND (0.397)	ND (0.397)	ND (0.397)	5.92	ND (0.397)	5.92
NI-205	4 - 6 (ft)	6/19/2014	FD	-	-	-	ND (0.0669)	ND (0.0669)	ND (0.0669)	ND (0.0669)	ND (0.0669)	ND (0.0669)	ND (0.0669)	0.222	ND (0.0669)	0.222
NI-205	4 - 6 (ft)	6/19/2014	N	-	-	-	ND (0.07)	ND (0.07)	ND (0.07)	ND (0.07)	ND (0.07)	ND (0.07)	ND (0.07)	0.92	ND (0.07)	0.92
NI-206	4 - 6 (ft)	6/18/2014	N	-	-	-	ND (0.137)	ND (0.137)	ND (0.137)	ND (0.137)	ND (0.137)	ND (0.137)	ND (0.137)	1.67	ND (0.137)	1.67
NI-207	4 - 6 (ft)	6/11/2014	N	-	-	-	ND (0.0728)	ND (0.0728)	ND (0.0728)	ND (0.0728)	ND (0.0728)	ND (0.0728)	ND (0.0728)	0.677	ND (0.0728)	0.677

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NI-210	2 - 4 (ft)	7/8/2014	N	-	-	-	ND (2.79)	ND (2.79)	ND (2.79)	ND (2.79)	ND (2.79)	ND (2.79)	ND (2.79)	60.2	ND (2.79)	60.2
NI-210	4 - 6 (ft)	7/8/2014	FD	-	-	-	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	0.208	ND (0.0557)	0.208
NI-210	4 - 6 (ft)	7/8/2014	N	-	-	-	ND (0.0561)	ND (0.0561)	ND (0.0561)	ND (0.0561)	ND (0.0561)	ND (0.0561)	ND (0.0561)	0.517	ND (0.0561)	0.517
NI-210	6 - 8 (ft)	7/8/2014	N	-	-	-	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)	ND (0.0603)
NI-210	8 - 10 (ft)	7/8/2014	N	-	-	-	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	0.108	ND (0.0624)	0.108
NI-301	10 - 12 (ft)	6/23/2014	N	-	-	-	ND (0.0676)	ND (0.0676)	ND (0.0676)	ND (0.0676)	ND (0.0676)	0.682	ND (0.0676)	1.27	ND (0.0676)	1.952
NI-301	2 - 4 (ft)	6/23/2014	N	-	-	-	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	23.9	ND (1.16)	23.9
NI-301	4 - 6 (ft)	6/23/2014	N	-	-	-	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	0.251	ND (0.0578)	0.251
NI-302	2 - 4 (ft)	7/16/2014	N	-	-	-	ND (1.13)	ND (1.13)	ND (1.13)	ND (1.13)	ND (1.13)	ND (1.13)	ND (1.13)	21.2 B	ND (1.13)	21.2
NI-302	4 - 6 (ft)	7/16/2014	N	-	-	-	ND (2.22)	ND (2.22)	ND (2.22)	ND (2.22)	ND (2.22)	ND (2.22)	ND (2.22)	46.9	ND (2.22)	46.9
NI-302	6 - 8 (ft)	7/16/2014	N	-	-	-	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)
NI-302	8 - 10 (ft)	7/16/2014	N	-	-	-	ND (0.0643)	ND (0.0643)	ND (0.0643)	ND (0.0643)	ND (0.0643)	ND (0.0643)	ND (0.0643)	0.788	ND (0.0643)	0.788
NI-303	10 - 12 (ft)	7/16/2014	N	-	-	-	ND (0.765)	ND (0.765)	ND (0.765)	ND (0.765)	3.48	ND (0.765)	ND (0.765)	6.37	3.78	13.63
NI-303	2 - 4 (ft)	7/16/2014	N	-	-	-	ND (29.9)	ND (29.9)	ND (29.9)	ND (29.9)	ND (29.9)	ND (29.9)	ND (29.9)	621 B	ND (29.9)	621
NI-303	4 - 6 (ft)	7/16/2014	N	-	-	-	ND (109)	ND (109)	ND (109)	ND (109)	ND (109)	791	ND (109)	2200	ND (109)	2991
NI-303	6 - 8 (ft)	7/16/2014	N	-	-	-	ND (19.1)	ND (19.1)	ND (19.1)	ND (19.1)	129	ND (19.1)	ND (19.1)	280	ND (19.1)	409
NI-303	8 - 10 (ft)	7/16/2014	N	-	-	-	ND (6.1)	ND (6.1)	ND (6.1)	ND (6.1)	ND (6.1)	57.4	ND (6.1)	ND (6.1)	131	188.4
NI-304	10 - 12 (ft)	7/16/2014	N	-	-	-	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)
NI-304	2 - 4 (ft)	7/16/2014	N	-	-	-	ND (0.548)	ND (0.548)	ND (0.548)	ND (0.548)	ND (0.548)	ND (0.548)	ND (0.548)	11.3 B	ND (0.548)	11.3
NI-304	4 - 6 (ft)	7/16/2014	N	-	-	-	ND (0.0566)	ND (0.0566)	ND (0.0566)	ND (0.0566)	ND (0.0566)	ND (0.0566)	ND (0.0566)	0.618	ND (0.0566)	0.618
NI-305	4 - 6 (ft)	10/30/2014	FD	-	-	-	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	23.3	ND (1.1)	23.3
NI-305	4 - 6 (ft)	10/30/2014	N	-	-	-	ND (1.62)	ND (1.62)	ND (1.62)	ND (1.62)	ND (1.62)	ND (1.62)	ND (1.62)	43	ND (1.62)	43
NI-305	6 - 8 (ft)	10/30/2014	N	-	-	-	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	0.397	ND (0.0527)	1.16	ND (0.0527)	1.557
NI-306	10 - 12 (ft)	10/30/2014	N	-	-	-	ND (1.23)	ND (1.23)	ND (1.23)	ND (1.23)	ND (1.23)	ND (1.23)	ND (1.23)	24.4	ND (1.23)	24.4
NI-306	12 - 14 (ft)	10/30/2014	N	-	-	-	ND (0.271)	ND (0.271)	ND (0.271)	ND (0.271)	ND (0.271)	ND (0.271)	ND (0.271)	4.4	ND (0.271)	4.4
NI-306	4 - 6 (ft)	10/30/2014	N	-	-	-	ND (10.9)	ND (10.9)	ND (10.9)	ND (10.9)	ND (10.9)	ND (10.9)	ND (10.9)	260	ND (10.9)	260
NI-306	6 - 8 (ft)	10/30/2014	N	-	-	-	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	3.81	ND (1.12)	25.1	ND (1.12)	28.91
NI-306	8 - 10 (ft)	10/30/2014	N	-	-	-	ND (0.0671)	ND (0.0671)	ND (0.0671)	ND (0.0671)	ND (0.0671)	ND (0.0671)	ND (0.0671)	0.126	ND (0.0671)	0.126
NI-307	10 - 12 (ft)	10/30/2014	N	-	-	-	ND (0.379)	ND (0.379)	ND (0.379)	ND (0.379)	ND (0.379)	ND (0.379)	ND (0.379)	3.39	ND (0.379)	3.39
NI-307	4 - 6 (ft)	10/30/2014	N	-	-	-	ND (2.7)	ND (2.7)	ND (2.7)	ND (2.7)	ND (2.7)	31.4	ND (2.7)	57.2	ND (2.7)	88.6
NI-307	6 - 8 (ft)	10/30/2014	N	-	-	-	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	0.993	ND (0.128)	0.993
NI-307	8 - 10 (ft)	10/30/2014	N	-	-	-	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	2.28	ND (0.126)	2.28
NI-308	2 - 4 (ft)	10/22/2014	N	-	-	-	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	0.411	ND (0.0604)	0.411
NI-308	4 - 6 (ft)	10/22/2014	N	-	-	-	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	0.458 P	ND (0.063)	0.458
NI-309	2 - 4 (ft)	10/21/2014	N	-	-	-	ND (0.642)	ND (0.642)	ND (0.642)	ND (0.642)	ND (0.642)	ND (0.642)	ND (0.642)	8.45	ND (0.642)	8.45
NI-310	10 - 12 (ft)	10/30/2014	N	-	-	-	ND (0.143)	ND (0.143)	ND (0.143)	ND (0.143)	ND (0.143)	ND (0.143)	ND (0.143)	3.49	ND (0.143)	3.49
NI-310	4 - 6 (ft)	10/30/2014	FD	-	-	-	ND (0.367)	ND (0.367)	ND (0.367)	ND (0.367)	ND (0.367)	ND (0.367)	ND (0.367)	5.59	ND (0.367)	5.59
NI-310	4 - 6 (ft)	10/30/2014	N	-	-	-	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	7.27	ND (0.544)	7.27
NI-310	8 - 10 (ft)	10/30/2014	FD	-	-	-	ND (0.643)	ND (0.643)	ND (0.643)	ND (0.643)	ND (0.643)	ND (0.643)	ND (0.643)	11.8	4.65	16.45
NI-310	8 - 10 (ft)	10/30/2014	N	-	-	-	ND (0.312)	ND (0.312)	ND (0.312)	ND (0.312)	ND (0.312)	ND (0.312)	ND (0.312)	10.5	4.16	14.66
NJ-001	2 - 4 (ft)	10/21/2013	N	-	-	-	ND (1.08)	ND (1.08)	ND (1.08)	ND (1.08)	ND (1.08)	ND (1.08)	ND (1.08)	44.1	ND (1.08)	44.1

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NJ-001	4 - 6 (ft)	10/21/2013	N	-	-	-	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)
NJ-101	2 - 4 (ft)	11/14/2013	FD	-	-	-	ND (0.325)	ND (0.325)	ND (0.325)	ND (0.325)	ND (0.325)	ND (0.325)	ND (0.325)	2.8	0.878	3.678
NJ-101	2 - 4 (ft)	11/14/2013	N	-	-	-	ND (0.156)	ND (0.156)	ND (0.156)	ND (0.156)	ND (0.156)	ND (0.156)	ND (0.156)	3.33	1.11	4.44
NJ-101	4 - 6 (ft)	10/22/2013	N	-	-	-	ND (0.0543)	ND (0.0543)	ND (0.0543)	ND (0.0543)	ND (0.0543)	ND (0.0543)	ND (0.0543)	0.426	ND (0.0543)	0.426
NJ-102	2 - 4 (ft)	11/15/2013	FD	-	-	-	ND (0.0517)	ND (0.0517)	ND (0.0517)	ND (0.0517)	ND (0.0517)	ND (0.0517)	ND (0.0517)	ND (0.0517)	ND (0.0517)	ND (0.0517)
NJ-102	2 - 4 (ft)	11/15/2013	N	-	-	-	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	0.132	ND (0.0527)	0.132
NJ-102	4 - 6 (ft)	10/22/2013	FD	-	-	-	ND (0.218)	ND (0.218)	ND (0.218)	ND (0.218)	ND (0.218)	ND (0.218)	ND (0.218)	2.72	ND (0.218)	2.72
NJ-102	4 - 6 (ft)	10/22/2013	N	-	-	-	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	0.992	ND (0.0557)	0.992
NJ-103	2 - 4 (ft)	11/15/2013	FD	-	-	-	ND (0.0561)	ND (0.0561)	ND (0.0561)	ND (0.0561)	ND (0.0561)	ND (0.0561)	ND (0.0561)	0.289	ND (0.0561)	0.289
NJ-103	2 - 4 (ft)	11/15/2013	N	-	-	-	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	0.26	ND (0.0582)	0.26
NJ-103	4 - 6 (ft)	10/22/2013	N	-	-	-	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	0.0604	ND (0.056)	ND (0.056)	ND (0.056)	0.0604
NJ-104	2 - 4 (ft)	11/14/2013	FD	-	-	-	ND (0.525)	ND (0.525)	ND (0.525)	ND (0.525)	ND (0.525)	ND (0.525)	ND (0.525)	22.9	7.67	30.57
NJ-104	2 - 4 (ft)	11/14/2013	N	-	-	-	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	28.3	8.9	37.2
NJ-104	4 - 6 (ft)	10/21/2013	N	-	-	-	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)
NJ-105	0 - 2 (ft)	11/13/2013	N	-	-	-	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)
NJ-105	2 - 4 (ft)	10/21/2013	N	-	-	-	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	0.456	0.141	0.597
NJ-106	0 - 2 (ft)	11/13/2013	N	-	-	-	ND (0.0509)	ND (0.0509)	ND (0.0509)	ND (0.0509)	ND (0.0509)	ND (0.0509)	ND (0.0509)	0.0787	ND (0.0509)	0.0787
NJ-106	2 - 4 (ft)	10/21/2013	N	-	-	-	ND (0.0553)	ND (0.0553)	ND (0.0553)	ND (0.0553)	ND (0.0553)	ND (0.0553)	ND (0.0553)	0.465	0.163	0.628
NJ-201	2 - 4 (ft)	6/23/2014	N	-	-	-	ND (1.11)	ND (1.11)	ND (1.11)	ND (1.11)	ND (1.11)	ND (1.11)	ND (1.11)	18.6	6.36	24.96
NJ-201	4 - 6 (ft)	6/23/2014	N	-	-	-	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	1.4	ND (0.0575)	1.4
NJ-301	2 - 4 (ft)	7/15/2014	N	-	-	-	ND (0.452)	ND (0.452)	ND (0.452)	ND (0.452)	ND (0.452)	ND (0.452)	ND (0.452)	5.8	1.94	7.74
NJ-302	2 - 4 (ft)	7/15/2014	N	-	-	-	ND (4.03)	ND (4.03)	ND (4.03)	ND (4.03)	ND (4.03)	ND (4.03)	ND (4.03)	79.9	25.6	105.5
NJ-302	4 - 6 (ft)	7/15/2014	N	-	-	-	ND (0.0543)	ND (0.0543)	ND (0.0543)	ND (0.0543)	ND (0.0543)	ND (0.0543)	ND (0.0543)	0.0334 J	ND (0.0543)	0.0334 J
NJ-302	8 - 10 (ft)	7/15/2014	N	-	-	-	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	0.227	ND (0.0632)	0.227
NJ-303	2 - 4 (ft)	7/16/2014	FD	-	-	-	ND (22.1)	ND (22.1)	ND (22.1)	ND (22.1)	ND (22.1)	ND (22.1)	ND (22.1)	406 B	ND (22.1)	406
NJ-303	2 - 4 (ft)	7/16/2014	N	-	-	-	ND (54.9)	ND (54.9)	ND (54.9)	ND (54.9)	ND (54.9)	ND (54.9)	ND (54.9)	1570 B	ND (54.9)	1570
NJ-303	4 - 6 (ft)	7/16/2014	N	-	-	-	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	0.0919	ND (0.0577)	0.0919
NJ-304	0 - 2 (ft)	10/22/2014	N	-	-	-	ND (0.564)	ND (0.564)	ND (0.564)	ND (0.564)	ND (0.564)	ND (0.564)	ND (0.564)	11.9	3.64	15.54
NJ-304	2 - 4 (ft)	11/6/2014	N	-	-	-	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	0.185	ND (0.0567)	0.185
NJ-305	0 - 2 (ft)	10/22/2014	N	-	-	-	ND (1.04)	ND (1.04)	ND (1.04)	ND (1.04)	ND (1.04)	ND (1.04)	ND (1.04)	24.2	ND (1.04)	24.2
NJ-305	2 - 4 (ft)	11/6/2014	N	-	-	-	ND (57.5)	ND (57.5)	ND (57.5)	ND (57.5)	ND (57.5)	438	ND (57.5)	1980	ND (57.5)	2418
NJ-305	4 - 6 (ft)	11/6/2014	N	-	-	-	ND (12.5)	ND (12.5)	ND (12.5)	ND (12.5)	ND (12.5)	66.6	ND (12.5)	349	ND (12.5)	415.6
NJ-305	6 - 8 (ft)	11/6/2014	N	-	-	-	ND (19.7)	ND (19.7)	ND (19.7)	ND (19.7)	ND (19.7)	108	ND (19.7)	641	ND (19.7)	749
NJ-306	2 - 4 (ft)	11/6/2014	N	-	-	-	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	0.0708	ND (0.0563)	0.0708
NJ-306	6 - 8 (ft)	11/6/2014	N	-	-	-	ND (0.149)	ND (0.149)	ND (0.149)	ND (0.149)	ND (0.149)	ND (0.149)	ND (0.149)	3.81	ND (0.149)	3.81
NJ-306	8 - 10 (ft)	11/6/2014	N	-	-	-	ND (0.0733)	ND (0.0733)	ND (0.0733)	ND (0.0733)	ND (0.0733)	ND (0.0733)	ND (0.0733)	0.409	ND (0.0733)	0.409
NJ-307	0 - 2 (ft)	11/6/2014	N	-	-	-	ND (0.556)	ND (0.556)	ND (0.556)	ND (0.556)	ND (0.556)	ND (0.556)	ND (0.556)	11.5	ND (0.556)	11.5
NJ-307	2 - 4 (ft)	11/6/2014	N	-	-	-	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	0.0696	ND (0.0598)	0.0696
NJ-308	0 - 2 (ft)	11/17/2014	N	-	-	-	ND (0.44)	ND (0.44)	ND (0.44)	ND (0.44)	ND (0.44)	ND (0.44)	ND (0.44)	6.27	ND (0.44)	6.27
NK-101	2 - 4 (ft)	10/24/2013	N	-	-	-	ND (2.31)	ND (2.31)	ND (2.31)	ND (2.31)	ND (2.31)	5.78 P	ND (2.31)	60	ND (2.31)	65.78
NK-101	4 - 6 (ft)	10/24/2013	N	-	-	-	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	0.135	ND (0.058)	0.854	ND (0.058)	0.989

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NK-102	2 - 4 (ft)	10/24/2013	N	-	-	-	ND (0.336)	ND (0.336)	ND (0.336)	ND (0.336)	ND (0.336)	ND (0.336)	ND (0.336)	3.29	ND (0.336)	3.29
NK-103	2 - 4 (ft)	10/24/2013	N	-	-	-	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	3.94	ND (1.14)	16	ND (1.14)	19.94
NK-103	4 - 6 (ft)	10/24/2013	N	-	-	-	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	0.0745	ND (0.0592)	0.532	ND (0.0592)	0.6065
NK-104	2 - 4 (ft)	10/24/2013	N	-	-	-	ND (3.21)	ND (3.21)	ND (3.21)	ND (3.21)	ND (3.21)	7.4 P	ND (3.21)	75.9	ND (3.21)	83.3
NK-104	4 - 6 (ft)	10/24/2013	N	-	-	-	ND (0.385)	ND (0.385)	ND (0.385)	ND (0.385)	ND (0.385)	0.775 P	ND (0.385)	7.17	ND (0.385)	7.945
NK-201	2 - 4 (ft)	6/20/2014	N	-	-	-	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	12.7	ND (1.12)	12.7
NK-201	4 - 6 (ft)	6/20/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	1.58	ND (0.114)	1.58
NK-202	2 - 4 (ft)	6/20/2014	N	-	-	-	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)
NK-202	3.3 - 3.5 (ft)	5/21/2014	N	-	-	-	ND (0.18)	ND (0.18)	ND (0.18)	ND (0.18)	ND (0.18)	ND (0.18)	ND (0.18)	2.09	ND (0.18)	2.09
NK-202	4 - 6 (ft)	6/20/2014	N	-	-	-	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	2.04	ND (0.058)	2.04
NK-203	2 - 4 (ft)	5/28/2014	FD	-	-	-	ND (0.329)	ND (0.329)	ND (0.329)	ND (0.329)	ND (0.329)	ND (0.329)	ND (0.329)	4.54	ND (0.329)	4.54
NK-203	2 - 4 (ft)	5/28/2014	N	-	-	-	ND (0.226)	ND (0.226)	ND (0.226)	ND (0.226)	ND (0.226)	ND (0.226)	ND (0.226)	3.38	ND (0.226)	3.38
NK-203	3 - 3.3 (ft)	5/21/2014	N	-	-	-	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	0.194	ND (0.0624)	0.194
NK-203	4 - 6 (ft)	5/28/2014	N	-	-	-	ND (0.302)	ND (0.302)	ND (0.302)	ND (0.302)	ND (0.302)	ND (0.302)	ND (0.302)	5.44	ND (0.302)	5.44
NK-204	2 - 4 (ft)	5/16/2014	N	-	-	-	ND (1.62)	ND (1.62)	ND (1.62)	ND (1.62)	ND (1.62)	1.81	ND (1.62)	24.5	ND (1.62)	26.31
NK-204	4 - 6 (ft)	5/16/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	2.06	ND (0.114)	2.06
NK-301	2 - 4 (ft)	6/4/2014	FD	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	1.99	ND (0.115)	1.99
NK-301	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (0.168)	ND (0.168)	ND (0.168)	ND (0.168)	ND (0.168)	ND (0.168)	ND (0.168)	1.97	ND (0.168)	1.97
NK-302	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (6.15)	ND (6.15)	ND (6.15)	ND (6.15)	ND (6.15)	ND (6.15)	ND (6.15)	125	ND (6.15)	125
NK-302	4 - 6 (ft)	6/4/2014	N	-	-	-	ND (0.0664)	ND (0.0664)	ND (0.0664)	ND (0.0664)	ND (0.0664)	0.234	ND (0.0664)	1.31	ND (0.0664)	1.544
NK-303	2 - 4 (ft)	6/9/2014	N	-	-	-	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	ND (0.0665)	0.12	ND (0.0665)	0.12
NK-303	4 - 6 (ft)	6/9/2014	N	-	-	-	ND (0.199)	ND (0.199)	ND (0.199)	ND (0.199)	ND (0.199)	ND (0.199)	ND (0.199)	2.49	ND (0.199)	2.49
NK-303	5 (ft)	6/4/2014	N	-	-	-	ND (0.799)	ND (0.799)	ND (0.799)	ND (0.799)	ND (0.799)	ND (0.799)	ND (0.799)	12.1	ND (0.799)	12.1
NL-001	2 - 4 (ft)	11/13/2013	FD	-	-	-	ND (0.0553)	ND (0.0553)	ND (0.0553)	ND (0.0553)	ND (0.0553)	ND (0.0553)	ND (0.0553)	3.95	1.55	5.5
NL-001	2 - 4 (ft)	11/13/2013	N	-	-	-	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	6.96	2.47	9.43
NL-101	0 - 2 (ft)	11/13/2013	N	-	-	-	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	ND (22.2)	927	456	1383
NL-101	2 - 4 (ft)	11/13/2013	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	1.84	0.923	2.763
NL-102	0 - 2 (ft)	11/13/2013	FD	-	-	-	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	197	75.4	272.4
NL-102	0 - 2 (ft)	11/13/2013	N	-	-	-	ND (5.82)	ND (5.82)	ND (5.82)	ND (5.82)	ND (5.82)	ND (5.82)	ND (5.82)	164	64.6	228.6
NL-102	2 - 4 (ft)	11/13/2013	N	-	-	-	ND (0.0658)	ND (0.0658)	ND (0.0658)	ND (0.0658)	ND (0.0658)	ND (0.0658)	ND (0.0658)	2.41	0.991	3.401
NL-103	0 - 2 (ft)	11/13/2013	N	-	-	-	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	38.5	14.9	53.4
NL-103	2 - 4 (ft)	11/13/2013	N	-	-	-	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	0.127	ND (0.0588)	0.127
NL-201	0 - 2 (ft)	5/19/2014	N	-	-	-	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	23.9	ND (1.16)	23.9
NL-201	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)
NL-202	0 - 2 (ft)	5/19/2014	N	-	-	-	ND (4.63)	ND (4.63)	ND (4.63)	ND (4.63)	ND (4.63)	ND (4.63)	ND (4.63)	113	ND (4.63)	113
NL-202	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	ND (0.0576)	0.897	ND (0.0576)	0.897
NL-203	0 - 2 (ft)	5/27/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	2.29	ND (0.12)	2.29
NL-204	0 - 2 (ft)	5/19/2014	N	-	-	-	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	0.205	ND (0.0583)	0.205
NL-301	0 - 2 (ft)	6/5/2014	N	-	-	-	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	1.67	ND (0.126)	1.67
NL-302	0 - 2 (ft)	6/6/2014	N	-	-	-	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	ND (1.16)	34.2	ND (1.16)	34.2
NL-302	2 - 4 (ft)	6/18/2014	N	-	-	-	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NL-303	0 - 2 (ft)	6/6/2014	FD	-	-	-	ND (62.5)	ND (62.5)	ND (62.5)	ND (62.5)	ND (62.5)	ND (62.5)	ND (62.5)	2030	ND (62.5)	2030
NL-303	0 - 2 (ft)	6/6/2014	N	-	-	-	ND (24.4)	ND (24.4)	ND (24.4)	ND (24.4)	ND (24.4)	ND (24.4)	ND (24.4)	783	ND (24.4)	783
NL-303	2 - 4 (ft)	6/17/2014	N	-	-	-	ND (0.294)	ND (0.294)	ND (0.294)	ND (0.294)	ND (0.294)	ND (0.294)	ND (0.294)	4.68	2.08	6.76
NL-304	0 - 2 (ft)	6/18/2014	FD	-	-	-	ND (0.578)	ND (0.578)	ND (0.578)	ND (0.578)	ND (0.578)	ND (0.578)	ND (0.578)	22.4	8.75	31.15
NL-304	0 - 2 (ft)	6/18/2014	N	-	-	-	ND (0.571)	ND (0.571)	ND (0.571)	ND (0.571)	ND (0.571)	ND (0.571)	ND (0.571)	20.8	8.56	29.36
NL-304	2 - 4 (ft)	6/18/2014	N	-	-	-	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)
NL-305	0 - 2 (ft)	7/15/2014	FD	-	-	-	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	ND (0.0656)	0.242	0.0832	0.325
NL-305	0 - 2 (ft)	7/15/2014	N	-	-	-	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	0.441	0.148	0.589
NL-306	0 - 2 (ft)	7/15/2014	N	-	-	-	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	0.252	0.0958	0.348
NL-307	0 - 2 (ft)	10/22/2014	N	-	-	-	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	0.21	ND (0.057)	0.21
NL-308	0 - 2 (ft)	10/22/2014	N	-	-	-	ND (0.0584)	ND (0.0584)	ND (0.0584)	0.157	ND (0.0584)	ND (0.0584)	ND (0.0584)	0.225	ND (0.0584)	0.382
NM-101	0 - 2 (ft)	10/23/2013	N	-	-	-	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	ND (0.0606)	0.102	ND (0.0606)	0.102
NM-102	0 - 2 (ft)	10/23/2013	N	-	-	-	ND (5.35)	ND (5.35)	ND (5.35)	ND (5.35)	ND (5.35)	21.5 P	ND (5.35)	194	ND (5.35)	215.5
NM-102	2 - 4 (ft)	10/23/2013	N	-	-	-	ND (4.34)	ND (4.34)	ND (4.34)	ND (4.34)	ND (4.34)	25.4 P	ND (4.34)	126	38.4	189.8
NM-102	4 - 6 (ft)	11/20/2013	FD	-	-	-	ND (3.61)	ND (3.61)	ND (3.61)	ND (3.61)	ND (3.61)	53.6	ND (3.61)	78.4	18.8	150.8
NM-102	4 - 6 (ft)	11/20/2013	N	-	-	-	ND (4.26)	ND (4.26)	ND (4.26)	ND (4.26)	ND (4.26)	41.8	ND (4.26)	71.5	17.9	131.2
NM-102	6 - 8 (ft)	11/20/2013	N	-	-	-	ND (0.788)	ND (0.788)	ND (0.788)	ND (0.788)	ND (0.788)	ND (0.788)	ND (0.788)	14.8	ND (0.788)	14.8
NM-102	8 - 10 (ft)	11/20/2013	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	3.41	ND (0.115)	3.41
NM-103	0 - 2 (ft)	10/23/2013	N	-	-	-	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	ND (1.12)	5	ND (1.12)	5
NM-104	0 - 2 (ft)	10/23/2013	N	-	-	-	ND (0.174)	ND (0.174)	ND (0.174)	ND (0.174)	ND (0.174)	ND (0.174)	ND (0.174)	1.09	ND (0.174)	1.09
NM-201	0 - 2 (ft)	5/23/2014	N	-	-	-	ND (5.41)	ND (5.41)	ND (5.41)	ND (5.41)	ND (5.41)	ND (5.41)	ND (5.41)	85.1	ND (5.41)	85.1
NM-201	2 - 4 (ft)	5/23/2014	N	-	-	-	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	0.439	ND (0.056)	0.439
NM-201	6 - 8 (ft)	6/16/2014	FD	-	-	-	ND (0.0742)	ND (0.0742)	ND (0.0742)	ND (0.0742)	ND (0.0742)	0.35	ND (0.0742)	1.49	ND (0.0742)	1.84
NM-201	6 - 8 (ft)	6/16/2014	N	-	-	-	ND (0.144)	ND (0.144)	ND (0.144)	ND (0.144)	ND (0.144)	0.325	ND (0.144)	1.48	ND (0.144)	1.805
NM-202	0 - 2 (ft)	5/27/2014	N	-	-	-	ND (5.65)	ND (5.65)	ND (5.65)	ND (5.65)	ND (5.65)	ND (5.65)	ND (5.65)	85.8	ND (5.65)	85.8
NM-202	2 - 4 (ft)	5/27/2014	N	-	-	-	ND (4.17)	ND (4.17)	ND (4.17)	ND (4.17)	ND (4.17)	42.9	ND (4.17)	77	ND (4.17)	119.9
NM-202	4 - 6 (ft)	5/23/2014	N	-	-	-	ND (4.76)	ND (4.76)	ND (4.76)	ND (4.76)	ND (4.76)	ND (4.76)	ND (4.76)	65.7	ND (4.76)	65.7
NM-202	6 - 8 (ft)	6/16/2014	N	-	-	-	ND (1.35)	ND (1.35)	ND (1.35)	ND (1.35)	ND (1.35)	3.53	ND (1.35)	11.4	ND (1.35)	14.93
NM-202	8 - 10 (ft)	6/16/2014	N	-	-	-	ND (0.082)	ND (0.082)	ND (0.082)	ND (0.082)	ND (0.082)	0.219	ND (0.082)	0.77	ND (0.082)	0.989
NM-203	0 - 2 (ft)	6/5/2014	N	-	-	-	ND (2.19)	ND (2.19)	ND (2.19)	ND (2.19)	ND (2.19)	ND (2.19)	ND (2.19)	47.7	ND (2.19)	47.7
NM-203	4 - 6 (ft)	6/5/2014	FD	-	-	-	ND (0.407)	ND (0.407)	ND (0.407)	ND (0.407)	ND (0.407)	ND (0.407)	ND (0.407)	6.62	ND (0.407)	6.62
NM-203	4 - 6 (ft)	6/5/2014	N	-	-	-	ND (1.13)	ND (1.13)	ND (1.13)	ND (1.13)	ND (1.13)	ND (1.13)	ND (1.13)	20.9	ND (1.13)	20.9
NM-203	6 - 8 (ft)	6/16/2014	N	-	-	-	ND (0.0671)	ND (0.0671)	ND (0.0671)	ND (0.0671)	ND (0.0671)	0.198	ND (0.0671)	1.9	ND (0.0671)	2.098
NM-204	4 - 6 (ft)	5/27/2014	FD	-	-	-	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	0.89	ND (0.0631)	0.89
NM-204	4 - 6 (ft)	5/27/2014	N	-	-	-	ND (0.0697)	ND (0.0697)	ND (0.0697)	ND (0.0697)	ND (0.0697)	ND (0.0697)	ND (0.0697)	1.08	ND (0.0697)	1.08
NM-301	6 - 8 (ft)	6/17/2014	FD	-	-	-	ND (2.03)	ND (2.03)	ND (2.03)	ND (2.03)	ND (2.03)	ND (2.03)	ND (2.03)	36.7	ND (2.03)	36.7
NM-301	6 - 8 (ft)	6/17/2014	N	-	-	-	ND (3.18)	ND (3.18)	ND (3.18)	ND (3.18)	ND (3.18)	ND (3.18)	ND (3.18)	46.6	ND (3.18)	46.6
NM-301	8 - 10 (ft)	6/17/2014	N	-	-	-	ND (0.557)	ND (0.557)	ND (0.557)	ND (0.557)	ND (0.557)	ND (0.557)	ND (0.557)	9.9	ND (0.557)	9.9
NM-302	4 - 6 (ft)	6/18/2014	N	-	-	-	ND (0.0602)	ND (0.0602)	ND (0.0602)	ND (0.0602)	ND (0.0602)	ND (0.0602)	ND (0.0602)	0.29	ND (0.0602)	0.29
NM-303	2 - 4 (ft)	7/2/2014	N	-	-	-	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)
NM-303	6 - 8 (ft)	7/2/2014	N	-	-	-	ND (0.713)	ND (0.713)	ND (0.713)	ND (0.713)	ND (0.713)	ND (0.713)	ND (0.713)	6.96	ND (0.713)	6.96

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NN-001	10 - 12 (ft)	6/17/2014	N	-	-	-	ND (1.99)	ND (1.99)	ND (1.99)	ND (1.99)	ND (1.99)	13.5	ND (1.99)	14.8	ND (1.99)	28.3
NN-001	12 - 14 (ft)	6/17/2014	N	-	-	-	ND (1.18)	ND (1.18)	ND (1.18)	ND (1.18)	ND (1.18)	20.6	ND (1.18)	ND (1.18)	ND (1.18)	20.6
NN-001	6 - 8 (ft)	10/25/2013	FD	-	-	-	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	218	ND (11.5)	265	68.2	551.2
NN-001	6 - 8 (ft)	10/25/2013	N	-	-	-	ND (18.2)	ND (18.2)	ND (18.2)	ND (18.2)	ND (18.2)	277	ND (18.2)	231	42.8	550.8
NN-001	8 - 10 (ft)	10/25/2013	N	-	-	-	ND (0.767)	ND (0.767)	ND (0.767)	ND (0.767)	ND (0.767)	8.75	ND (0.767)	13.8	3.18	25.73
NN-002	2 - 4 (ft)	10/23/2013	N	-	-	-	ND (0.28)	ND (0.28)	ND (0.28)	ND (0.28)	ND (0.28)	ND (0.28)	ND (0.28)	4.5	1.36	5.86
NN-002	4 - 6 (ft)	10/23/2013	N	-	-	-	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	0.104 P	ND (0.0594)	0.763	ND (0.0594)	0.867
NN-101	0 - 2 (ft)	11/19/2013	FD	-	-	-	ND (0.568)	ND (0.568)	ND (0.568)	ND (0.568)	ND (0.568)	ND (0.568)	ND (0.568)	12.7	3.49	16.19
NN-101	0 - 2 (ft)	11/19/2013	N	-	-	-	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	7.47 P	ND (1.15)	29.7	8.17	45.34
NN-101	2 - 4 (ft)	11/8/2013	N	-	-	-	ND (0.339)	ND (0.339)	ND (0.339)	ND (0.339)	ND (0.339)	ND (0.339)	ND (0.339)	6.02	1.66	7.68
NN-102	6 - 8 (ft)	11/12/2013	N	-	-	-	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	2.31	ND (0.0788)	2.31
NN-102	8 - 10 (ft)	11/12/2013	FD	-	-	-	ND (0.0642)	ND (0.0642)	ND (0.0642)	ND (0.0642)	ND (0.0642)	ND (0.0642)	ND (0.0642)	ND (0.0642)	ND (0.0642)	ND (0.0642)
NN-102	8 - 10 (ft)	11/12/2013	N	-	-	-	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)
NN-103	4 - 6 (ft)	11/12/2013	N	-	-	-	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	2.02	ND (0.0577)	2.02
NN-103	8 - 10 (ft)	11/12/2013	N	-	-	-	ND (0.131)	ND (0.131)	ND (0.131)	ND (0.131)	ND (0.131)	0.483 P	ND (0.131)	2.17	0.721	3.374
NN-104	10 - 12 (ft)	6/17/2014	N	-	-	-	ND (4.21)	ND (4.21)	ND (4.21)	ND (4.21)	ND (4.21)	13.8	ND (4.21)	35.9	ND (4.21)	49.7
NN-104	12 - 14 (ft)	6/17/2014	N	-	-	-	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	ND (0.0744)	0.215	ND (0.0744)	0.215
NN-104	8 - 10 (ft)	11/12/2013	N	-	-	-	ND (1.48)	ND (1.48)	ND (1.48)	ND (1.48)	ND (1.48)	12.3	ND (1.48)	33.1	9.64	55.04
NN-105	0 - 2 (ft)	11/19/2013	FD	-	-	-	ND (5.37)	ND (5.37)	ND (5.37)	ND (5.37)	ND (5.37)	ND (5.37)	ND (5.37)	158	47.8	205.8
NN-105	0 - 2 (ft)	11/19/2013	N	-	-	-	ND (11)	ND (11)	ND (11)	ND (11)	ND (11)	ND (11)	ND (11)	263	ND (11)	263
NN-105	2 - 4 (ft)	11/8/2013	N	-	-	-	ND (0.35)	ND (0.35)	ND (0.35)	ND (0.35)	ND (0.35)	ND (0.35)	ND (0.35)	5.28	1.54	6.82
NN-105	6 - 8 (ft)	11/8/2013	N	-	-	-	ND (0.0808)	ND (0.0808)	ND (0.0808)	ND (0.0808)	ND (0.0808)	ND (0.0808)	ND (0.0808)	1.96	ND (0.0808)	1.96
NN-201	0 - 2 (ft)	6/16/2014	N	-	-	-	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	31.6	ND (5.63)	106	ND (5.63)	137.6
NN-201	2 - 4 (ft)	6/16/2014	N	-	-	-	ND (0.348)	ND (0.348)	ND (0.348)	ND (0.348)	ND (0.348)	ND (0.348)	ND (0.348)	6.08	ND (0.348)	6.08
NN-201	4 - 6 (ft)	6/16/2014	N	-	-	-	ND (0.0644)	ND (0.0644)	ND (0.0644)	ND (0.0644)	ND (0.0644)	ND (0.0644)	ND (0.0644)	0.32	ND (0.0644)	0.32
NN-202	10 - 12 (ft)	6/17/2014	N	-	-	-	ND (0.164)	ND (0.164)	ND (0.164)	ND (0.164)	ND (0.164)	ND (0.164)	ND (0.164)	2.23	ND (0.164)	2.23
NN-202	6 - 8 (ft)	6/17/2014	N	-	-	-	ND (6.55)	ND (6.55)	ND (6.55)	ND (6.55)	13.8	28.5	ND (6.55)	103	ND (6.55)	145.3
NN-202	8 - 10 (ft)	6/17/2014	FD	-	-	-	ND (4.54)	ND (4.54)	ND (4.54)	ND (4.54)	ND (4.54)	7.78	ND (4.54)	28.2	ND (4.54)	35.98
NN-202	8 - 10 (ft)	6/17/2014	N	-	-	-	ND (4.04)	ND (4.04)	ND (4.04)	ND (4.04)	ND (4.04)	9.47	ND (4.04)	29.4	ND (4.04)	38.87
NN-301	0 - 2 (ft)	7/7/2014	N	-	-	-	ND (4.36)	ND (4.36)	ND (4.36)	ND (4.36)	ND (4.36)	ND (4.36)	ND (4.36)	82.8	23	105.8
NN-301	2 - 4 (ft)	7/7/2014	N	-	-	-	ND (0.547)	ND (0.547)	ND (0.547)	ND (0.547)	ND (0.547)	ND (0.547)	ND (0.547)	10.6	ND (0.547)	10.6
NN-301	4 - 6 (ft)	7/7/2014	N	-	-	-	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	0.153	ND (0.0589)	1.5	ND (0.0589)	1.653
NN-302	0 - 2 (ft)	7/8/2014	FD	-	-	-	ND (5.44)	ND (5.44)	ND (5.44)	ND (5.44)	ND (5.44)	ND (5.44)	ND (5.44)	121	29.6	150.6
NN-302	0 - 2 (ft)	7/8/2014	N	-	-	-	ND (5.48)	ND (5.48)	ND (5.48)	ND (5.48)	ND (5.48)	ND (5.48)	ND (5.48)	110	27	137
NN-302	2 - 4 (ft)	7/8/2014	N	-	-	-	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	27.7	ND (1.71)	27.7
NN-302	4 - 6 (ft)	7/8/2014	N	-	-	-	ND (2.47)	ND (2.47)	ND (2.47)	ND (2.47)	ND (2.47)	2.06 J	ND (2.47)	36.3	ND (2.47)	38.36
NN-302	6 - 8 (ft)	7/8/2014	N	-	-	-	ND (0.374)	ND (0.374)	ND (0.374)	ND (0.374)	ND (0.374)	ND (0.374)	ND (0.374)	4.62	ND (0.374)	4.62
NN-303	0 - 2 (ft)	7/16/2014	N	-	-	-	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	ND (0.231)	3.02 B	ND (0.231)	3.02
NN-303	4 - 6 (ft)	7/16/2014	N	-	-	-	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	6.48	ND (0.54)	6.48
NN-304	0 - 2 (ft)	7/16/2014	N	-	-	-	ND (0.053)	ND (0.053)	ND (0.053)	ND (0.053)	ND (0.053)	ND (0.053)	ND (0.053)	0.174	ND (0.053)	0.174
NN-304	4 - 6 (ft)	7/16/2014	N	-	-	-	ND (0.067)	ND (0.067)	ND (0.067)	ND (0.067)	ND (0.067)	ND (0.067)	ND (0.067)	0.435	ND (0.067)	0.435

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
NN-305	0 - 2 (ft)	7/16/2014	FD	-	-	-	ND (2.17)	ND (2.17)	ND (2.17)	ND (2.17)	ND (2.17)	21.2	ND (2.17)	47.6 B	ND (2.17)	68.8
NN-305	0 - 2 (ft)	7/16/2014	N	-	-	-	ND (3.2)	ND (3.2)	ND (3.2)	ND (3.2)	ND (3.2)	25.3	ND (3.2)	60.6 B	ND (3.2)	85.9
NN-305	2 - 4 (ft)	7/16/2014	N	-	-	-	ND (0.342)	ND (0.342)	ND (0.342)	ND (0.342)	ND (0.342)	ND (0.342)	ND (0.342)	4.32	ND (0.342)	4.32
NN-305	4 - 6 (ft)	7/16/2014	N	-	-	-	ND (0.347)	ND (0.347)	ND (0.347)	ND (0.347)	ND (0.347)	ND (0.347)	ND (0.347)	6.83	ND (0.347)	6.83
NN-306	4 - 6 (ft)	10/29/2014	N	-	-	-	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	29.3	ND (1.17)	29.3
NN-306	6 - 8 (ft)	10/29/2014	N	-	-	-	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	2.23	ND (0.0709)	2.23
NN-307	0 - 2 (ft)	10/22/2014	N	-	-	-	ND (2.67)	ND (2.67)	ND (2.67)	ND (2.67)	ND (2.67)	ND (2.67)	ND (2.67)	59.7	15.1	74.8
NN-307	2 - 4 (ft)	10/29/2014	FD	-	-	-	ND (11)	ND (11)	ND (11)	ND (11)	ND (11)	ND (11)	ND (11)	463	ND (11)	463
NN-307	2 - 4 (ft)	10/29/2014	N	-	-	-	ND (0.274)	ND (0.274)	ND (0.274)	ND (0.274)	ND (0.274)	ND (0.274)	ND (0.274)	5.44	ND (0.274)	5.44
NN-307	4 - 6 (ft)	10/29/2014	N	-	-	-	ND (1.65)	ND (1.65)	ND (1.65)	ND (1.65)	ND (1.65)	8.47	ND (1.65)	27.8	ND (1.65)	36.27
NN-307	6 - 8 (ft)	11/11/2014	N	-	-	-	ND (0.387)	ND (0.387)	ND (0.387)	ND (0.387)	ND (0.387)	ND (0.387)	ND (0.387)	6.53	ND (0.387)	6.53
NN-308	0 - 2 (ft)	10/22/2014	FD	-	-	-	ND (1.91)	ND (1.91)	ND (1.91)	ND (1.91)	ND (1.91)	ND (1.91)	ND (1.91)	47.3	15.3	62.6
NN-308	0 - 2 (ft)	10/22/2014	N	-	-	-	ND (1.76)	ND (1.76)	ND (1.76)	ND (1.76)	ND (1.76)	ND (1.76)	ND (1.76)	44.6	16.2	60.8
NN-308	2 - 4 (ft)	10/29/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	2.89	ND (0.112)	2.89
NN-309	0 - 2 (ft)	10/28/2014	N	-	-	-	ND (0.338)	ND (0.338)	ND (0.338)	ND (0.338)	ND (0.338)	ND (0.338)	ND (0.338)	6.98	ND (0.338)	6.98
NN-309	2 - 4 (ft)	11/11/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	2.64	ND (0.116)	2.64
NN-309	4 - 6 (ft)	11/11/2014	N	-	-	-	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	1.54	ND (0.194)	1.54
NN-310	0 - 2 (ft)	10/28/2014	FD	-	-	-	ND (0.164)	ND (0.164)	ND (0.164)	ND (0.164)	ND (0.164)	ND (0.164)	ND (0.164)	2.55	ND (0.164)	2.55
NN-310	0 - 2 (ft)	10/28/2014	N	-	-	-	ND (0.223)	ND (0.223)	ND (0.223)	ND (0.223)	ND (0.223)	ND (0.223)	ND (0.223)	4.59	ND (0.223)	4.59
NN-310	2 - 4 (ft)	11/11/2014	N	-	-	-	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	1.42	ND (0.108)	1.42
NN-310	4 - 6 (ft)	11/11/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	1.57	ND (0.114)	1.57
NS-001	4 - 6 (ft)	11/18/2014	N	-	-	-	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	0.0236 J	ND (0.0552)	ND (0.0552)	0.0236 J
NS-001	6 - 8 (ft)	11/18/2014	N	-	-	-	ND (2.15)	ND (2.15)	ND (2.15)	ND (2.15)	ND (2.15)	38.3	ND (2.15)	42.8	ND (2.15)	81.1
NS-001	8 - 10 (ft)	11/18/2014	N	-	-	-	ND (0.296)	ND (0.296)	ND (0.296)	ND (0.296)	ND (0.296)	ND (0.296)	ND (0.296)	4.19	ND (0.296)	4.19
NS-101	4 - 6 (ft)	11/18/2014	N	-	-	-	ND (0.0614)	ND (0.0614)	ND (0.0614)	ND (0.0614)	ND (0.0614)	ND (0.0614)	0.0448 J	ND (0.0614)	ND (0.0614)	0.0448 J
NS-101	6 - 8 (ft)	11/18/2014	N	-	-	-	ND (1.65)	ND (1.65)	ND (1.65)	ND (1.65)	9.99	ND (1.65)	ND (1.65)	13.9	ND (1.65)	23.9
NS-101	8 - 10 (ft)	11/18/2014	N	-	-	-	ND (0.0638)	ND (0.0638)	ND (0.0638)	ND (0.0638)	ND (0.0638)	0.394	ND (0.0638)	1.67	ND (0.0638)	2.064
NS-102	4 - 6 (ft)	11/19/2014	N	-	-	-	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)
NS-102	6 - 8 (ft)	11/19/2014	N	-	-	-	ND (3.82)	ND (3.82)	ND (3.82)	ND (3.82)	ND (3.82)	ND (3.82)	ND (3.82)	52.3	ND (3.82)	52.3
NS-102	8 - 10 (ft)	11/19/2014	N	-	-	-	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.304	ND (0.1)	0.304
NS-103	10 - 12 (ft)	11/19/2014	N	-	-	-	ND (0.703)	ND (0.703)	ND (0.703)	ND (0.703)	ND (0.703)	ND (0.703)	ND (0.703)	11.6	ND (0.703)	11.6
NS-103	4 - 6 (ft)	11/19/2014	N	-	-	-	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	ND (0.0577)	0.0426 J	ND (0.0577)	ND (0.0577)	0.0426 J
NS-103	6 - 8 (ft)	11/19/2014	N	-	-	-	ND (3.75)	ND (3.75)	ND (3.75)	ND (3.75)	ND (3.75)	ND (3.75)	ND (3.75)	67.8	ND (3.75)	67.8
NS-103	8 - 10 (ft)	11/19/2014	N	-	-	-	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	5.58	ND (0.658)	5.58
NS-104	4 - 6 (ft)	11/18/2014	N	-	-	-	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	0.677	ND (0.058)	0.677
NS-104	6 - 8 (ft)	11/18/2014	N	-	-	-	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	203	ND (11.5)	203
NS-104	8 - 10 (ft)	11/18/2014	N	-	-	-	ND (0.188)	ND (0.188)	ND (0.188)	ND (0.188)	ND (0.188)	ND (0.188)	ND (0.188)	2.33	ND (0.188)	2.33
PDMW-22S	10 - 12 (ft)	11/16/2013	N	-	-	-	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	2.44	ND (0.0726)	1.41	ND (0.0726)	3.85
PDMW-22S-01	10 - 12 (ft)	7/10/2014	N	-	-	-	ND (26.2)	ND (26.2)	ND (26.2)	ND (26.2)	ND (26.2)	551	ND (26.2)	ND (26.2)	ND (26.2)	551
PDMW-22S-01	12 - 14 (ft)	7/10/2014	N	-	-	-	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)	0.0464 J	ND (0.0855)	ND (0.0855)	ND (0.0855)	0.0464 J
PDMW-22S-01	4 - 6 (ft)	7/10/2014	N	-	-	-	ND (12.6)	ND (12.6)	ND (12.6)	ND (12.6)	ND (12.6)	427	ND (12.6)	ND (12.6)	ND (12.6)	427

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
PDMW-22S-03	10 - 12 (ft)	7/10/2014	N	-	-	-	ND (0.406)	ND (0.406)	ND (0.406)	ND (0.406)	ND (0.406)	6.17	ND (0.406)	ND (0.406)	ND (0.406)	6.17
PDMW-22S-03	4 - 6 (ft)	7/10/2014	N	-	-	-	ND (1.37)	ND (1.37)	ND (1.37)	ND (1.37)	ND (1.37)	27.7	ND (1.37)	ND (1.37)	ND (1.37)	27.7
PDMW-22S-03	6 - 8 (ft)	7/10/2014	N	-	-	-	ND (4.25)	ND (4.25)	ND (4.25)	ND (4.25)	ND (4.25)	172	ND (4.25)	52	ND (4.25)	224
PDMW-22S-03	8 - 10 (ft)	7/10/2014	N	-	-	-	ND (0.431)	ND (0.431)	ND (0.431)	ND (0.431)	ND (0.431)	9.3	ND (0.431)	2.33	ND (0.431)	11.63
PDMW-22S-04	10 - 12 (ft)	7/10/2014	N	-	-	-	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)
PDMW-22S-04	4 - 6 (ft)	7/10/2014	N	-	-	-	ND (0.0531)	ND (0.0531)	ND (0.0531)	ND (0.0531)	ND (0.0531)	0.565	ND (0.0531)	0.409	ND (0.0531)	0.974
PDMW-22S-04	8 - 10 (ft)	7/10/2014	N	-	-	-	ND (0.0819)	ND (0.0819)	ND (0.0819)	ND (0.0819)	ND (0.0819)	ND (0.0819)	ND (0.0819)	0.482	ND (0.0819)	0.482
PDMW-22S-10	10 - 12 (ft)	11/7/2014	N	-	-	-	ND (2.07)	ND (2.07)	ND (2.07)	ND (2.07)	ND (2.07)	47.4	ND (2.07)	ND (2.07)	ND (2.07)	47.4
PDMW-22S-10	12 - 14 (ft)	11/7/2014	N	-	-	-	ND (0.0712)	ND (0.0712)	ND (0.0712)	ND (0.0712)	ND (0.0712)	0.117	ND (0.0712)	0.0783	ND (0.0712)	0.1953
PDMW-22S-10	4 - 6 (ft)	11/7/2014	N	-	-	-	ND (4)	ND (4)	ND (4)	ND (4)	ND (4)	87.3	ND (4)	ND (4)	ND (4)	87.3
PDMW-24S	6 - 8 (ft)	11/14/2013	N	-	-	-	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	0.117	ND (0.063)	1.13	ND (0.063)	1.247
SA-001	0 - 2 (ft)	6/30/2014	N	528	223	290	-	-	-	-	-	-	-	-	-	-
SA-001	2 - 4 (ft)	10/8/2013	N	-	-	-	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	11.3	ND (1.15)	ND (1.15)	ND (1.15)	11.3
SA-001	4 - 6 (ft)	10/8/2013	N	-	-	-	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)
SA-002	0 - 2 (ft)	10/8/2013	N	-	-	-	ND (0.0766)	ND (0.0766)	ND (0.0766)	ND (0.0766)	ND (0.0766)	0.563	ND (0.0766)	1.13	ND (0.0766)	1.693
SA-002	2 - 4 (ft)	10/8/2013	N	-	-	-	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	0.0905	ND (0.0574)	0.143	ND (0.0574)	0.2335
SA-002	4 - 6 (ft)	10/8/2013	N	-	-	-	ND (0.0617)	ND (0.0617)	ND (0.0617)	ND (0.0617)	ND (0.0617)	0.154	ND (0.0617)	ND (0.0617)	ND (0.0617)	0.154
SA-003	4 - 6 (ft)	10/8/2013	N	-	-	-	ND (6.55)	ND (6.55)	ND (6.55)	ND (6.55)	ND (6.55)	238	ND (6.55)	ND (6.55)	ND (6.55)	238
SA-003	6 - 8 (ft)	11/5/2013	N	-	-	-	ND (0.635)	ND (0.635)	ND (0.635)	ND (0.635)	ND (0.635)	14.9	2.73	ND (0.635)	ND (0.635)	17.63
SA-003	8 - 10 (ft)	11/5/2013	N	-	-	-	ND (0.294)	ND (0.294)	ND (0.294)	ND (0.294)	ND (0.294)	4.88	ND (0.294)	ND (0.294)	ND (0.294)	4.88
SA-004	2 - 4 (ft)	10/7/2013	N	-	-	-	ND (1.26)	ND (1.26)	ND (1.26)	ND (1.26)	ND (1.26)	17.7	ND (1.26)	17.9	ND (1.26)	35.6
SA-004	4 - 6 (ft)	10/7/2013	N	-	-	-	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	0.409	ND (0.0587)	0.202	ND (0.0587)	0.611
SA-103	2 - 4 (ft)	10/29/2013	N	-	-	-	ND (0.368)	ND (0.368)	ND (0.368)	ND (0.368)	ND (0.368)	5.29	ND (0.368)	2.54	ND (0.368)	7.83
SA-104	2 - 4 (ft)	11/4/2013	FD	-	-	-	ND (0.054)	ND (0.054)	ND (0.054)	ND (0.054)	ND (0.054)	ND (0.054)	ND (0.054)	0.112	ND (0.054)	0.112
SA-104	2 - 4 (ft)	11/4/2013	N	-	-	-	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)
SA-105	4 - 6 (ft)	11/4/2013	N	-	-	-	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	0.147	ND (0.0599)	ND (0.0599)	ND (0.0599)	0.147
SA-105	6 - 8 (ft)	11/4/2013	N	-	-	-	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)
SA-106	0 - 2 (ft)	6/3/2014	N	388	78.8	92	-	-	-	-	-	-	-	-	-	-
SA-107	0 - 2 (ft)	6/30/2014	FD	-	15.1	-	-	-	-	-	-	-	-	-	-	-
SA-107	0 - 2 (ft)	6/30/2014	N	50.9	19	31.7	-	-	-	-	-	-	-	-	-	-
SA-107	2 - 4 (ft)	11/5/2013	N	-	-	-	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)
SA-108	2 - 4 (ft)	10/29/2013	FD	-	-	-	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	2.01	ND (0.165)	0.826	ND (0.165)	2.836
SA-108	2 - 4 (ft)	10/29/2013	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	1.63	ND (0.112)	0.637	ND (0.112)	2.267
SA-201	0 - 2 (ft)	6/3/2014	N	532	834	1220	-	-	-	-	-	-	-	-	-	-
SA-201	0 - 2 (ft)	6/3/2014	N	-	-	-	ND (0.278)	ND (0.278)	ND (0.278)	ND (0.278)	ND (0.278)	1.21	ND (0.278)	1.73	ND (0.278)	2.94
SA-201	4 - 6 (ft)	6/3/2014	FD	-	-	-	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	0.845	ND (0.0726)	ND (0.0726)	ND (0.0726)	0.845
SA-201	4 - 6 (ft)	6/3/2014	N	-	-	-	ND (0.0717)	ND (0.0717)	ND (0.0717)	ND (0.0717)	ND (0.0717)	0.718	ND (0.0717)	ND (0.0717)	ND (0.0717)	0.718
SA-201	6 - 8 (ft)	6/10/2014	N	-	-	-	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	1.06	ND (0.0583)	1.91	ND (0.0583)	2.97
SA-202	0 - 2 (ft)	6/2/2014	N	-	1680	-	-	-	-	-	-	-	-	-	-	-
SA-202	2 - 4 (ft)	6/2/2014	N	-	-	-	ND (0.0655)	ND (0.0655)	ND (0.0655)	ND (0.0655)	ND (0.0655)	0.137	ND (0.0655)	ND (0.0655)	ND (0.0655)	0.137
SB-001	0 - 2 (ft)	6/11/2014	N	-	-	-	ND (0.568)	ND (0.568)	ND (0.568)	ND (0.568)	ND (0.568)	2.76	ND (0.568)	7.91	ND (0.568)	10.67

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
SB-001	2 - 4 (ft)	6/11/2014	FD	-	-	-	ND (0.396)	ND (0.396)	ND (0.396)	ND (0.396)	ND (0.396)	4.88	ND (0.396)	4.36	ND (0.396)	9.24
SB-001	2 - 4 (ft)	6/11/2014	N	-	-	-	ND (0.389)	ND (0.389)	ND (0.389)	ND (0.389)	ND (0.389)	4.02	ND (0.389)	4.06	ND (0.389)	8.08
SB-001	4 - 6 (ft)	6/11/2014	N	-	-	-	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	0.0429 J	ND (0.0589)	0.0429 J
SB-101	0 - 2 (ft)	10/4/2013	N	-	-	-	ND (0.565)	ND (0.565)	ND (0.565)	ND (0.565)	ND (0.565)	3.3	ND (0.565)	11.9	ND (0.565)	15.2
SB-101	2 - 4 (ft)	10/29/2013	N	-	-	-	ND (0.58)	ND (0.58)	ND (0.58)	ND (0.58)	ND (0.58)	5.82	ND (0.58)	7.14	ND (0.58)	12.96
SB-101	4 - 6 (ft)	10/29/2013	N	-	-	-	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	0.589	ND (0.0584)	0.886	ND (0.0584)	1.475
SB-201	2 - 4 (ft)	6/10/2014	N	-	-	-	ND (0.0538)	ND (0.0538)	ND (0.0538)	ND (0.0538)	ND (0.0538)	ND (0.0538)	ND (0.0538)	ND (0.0538)	ND (0.0538)	ND (0.0538)
SC-001	2 - 4 (ft)	11/6/2013	N	-	-	-	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	0.194	ND (0.0526)	0.19	ND (0.0526)	0.384
SC-001	4 - 6 (ft)	11/6/2013	N	-	-	-	ND (0.573)	ND (0.573)	ND (0.573)	ND (0.573)	ND (0.573)	12.8	ND (0.573)	9.93	ND (0.573)	22.73
SC-101	4 - 6 (ft)	11/6/2013	N	-	-	-	ND (0.569)	ND (0.569)	ND (0.569)	ND (0.569)	ND (0.569)	9.25	ND (0.569)	10.2	ND (0.569)	19.45
SC-101	6 - 8 (ft)	11/6/2013	N	-	-	-	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	1.67	ND (0.177)	3.54	0.915	6.125
SC-102	4 - 6 (ft)	11/6/2013	N	-	-	-	ND (0.57)	ND (0.57)	ND (0.57)	ND (0.57)	ND (0.57)	9.83	14.3	ND (0.57)	ND (0.57)	24.13
SC-103	4 - 6 (ft)	11/6/2013	N	-	-	-	ND (0.399)	ND (0.399)	ND (0.399)	ND (0.399)	ND (0.399)	1.12 P	ND (0.399)	10.7	ND (0.399)	11.82
SC-103	6 - 8 (ft)	11/6/2013	N	-	-	-	ND (0.24)	ND (0.24)	ND (0.24)	ND (0.24)	ND (0.24)	ND (0.24)	ND (0.24)	4.11	1.33	5.44
SC-103	8 - 10 (ft)	11/6/2013	N	-	-	-	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	0.804	ND (0.126)	0.804
SC-201	4 - 6 (ft)	6/9/2014	FD	-	-	-	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	0.262	ND (0.0598)	0.262
SC-201	4 - 6 (ft)	6/9/2014	N	-	-	-	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)
SC-202	4 - 6 (ft)	6/9/2014	N	-	-	-	ND (0.0542)	ND (0.0542)	ND (0.0542)	ND (0.0542)	ND (0.0542)	0.128	ND (0.0542)	0.209	ND (0.0542)	0.337
SC-202	6 - 8 (ft)	6/9/2014	N	-	-	-	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	0.0428 J	ND (0.0599)	ND (0.0599)	ND (0.0599)	0.0428 J
SC-203	4 - 6 (ft)	6/9/2014	N	-	-	-	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	16.8	ND (1.2)	16.2	ND (1.2)	33
SC-203	6 - 8 (ft)	6/9/2014	N	-	-	-	ND (1.18)	ND (1.18)	ND (1.18)	ND (1.18)	ND (1.18)	7.16	ND (1.18)	15.3	ND (1.18)	22.46
SC-203	8 - 10 (ft)	6/9/2014	N	-	-	-	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)
SC-204	4 - 6 (ft)	6/10/2014	FD	-	-	-	ND (1.27)	ND (1.27)	ND (1.27)	ND (1.27)	ND (1.27)	9.34	ND (1.27)	19.8	ND (1.27)	29.14
SC-204	4 - 6 (ft)	6/10/2014	N	-	-	-	ND (0.613)	ND (0.613)	ND (0.613)	ND (0.613)	ND (0.613)	6.11	ND (0.613)	12.7	ND (0.613)	18.81
SC-204	6 - 8 (ft)	6/10/2014	N	-	-	-	ND (0.592)	ND (0.592)	ND (0.592)	ND (0.592)	ND (0.592)	7.98	ND (0.592)	4.65	ND (0.592)	12.63
SC-204	8 - 10 (ft)	6/10/2014	N	-	-	-	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	0.664	ND (0.0621)	0.428	ND (0.0621)	1.092
SC-205	4 - 6 (ft)	6/10/2014	N	-	-	-	ND (0.6)	ND (0.6)	ND (0.6)	ND (0.6)	ND (0.6)	4.92	ND (0.6)	12	ND (0.6)	16.92
SC-205	6 - 8 (ft)	6/10/2014	N	-	-	-	ND (0.718)	ND (0.718)	ND (0.718)	ND (0.718)	ND (0.718)	12.5	ND (0.718)	8.91	ND (0.718)	21.41
SC-205	8 - 10 (ft)	6/10/2014	N	-	-	-	ND (0.43)	ND (0.43)	ND (0.43)	ND (0.43)	ND (0.43)	2.92	ND (0.43)	3.83	ND (0.43)	6.75
SC-301	10 - 12 (ft)	6/30/2014	N	-	-	-	ND (0.0579)	ND (0.0579)	ND (0.0579)	ND (0.0579)	ND (0.0579)	ND (0.0579)	ND (0.0579)	0.715	ND (0.0579)	0.715
SC-301	6 - 8 (ft)	6/30/2014	N	-	-	-	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	7.29	ND (0.56)	7.29
SC-301	8 - 10 (ft)	6/30/2014	N	-	-	-	ND (0.582)	ND (0.582)	ND (0.582)	ND (0.582)	ND (0.582)	ND (0.582)	ND (0.582)	11.4	3.5	14.9
SC-302	10 - 12 (ft)	6/27/2014	N	-	-	-	ND (0.376)	ND (0.376)	ND (0.376)	ND (0.376)	ND (0.376)	2.17	ND (0.376)	6.5	2.1	10.77
SC-302	6 - 8 (ft)	6/27/2014	N	-	-	-	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	18.6	ND (0.558)	18.6
SC-302	8 - 10 (ft)	6/27/2014	N	-	-	-	ND (1.52)	ND (1.52)	ND (1.52)	ND (1.52)	ND (1.52)	6.44	ND (1.52)	15.4	ND (1.52)	21.84
SC-303	6 - 8 (ft)	6/30/2014	N	-	-	-	ND (0.0634)	ND (0.0634)	ND (0.0634)	ND (0.0634)	ND (0.0634)	ND (0.0634)	ND (0.0634)	0.612	ND (0.0634)	0.612
SC-304	6 - 8 (ft)	6/30/2014	FD	-	-	-	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	0.295	ND (0.058)	0.295
SC-304	6 - 8 (ft)	6/30/2014	N	-	-	-	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	0.188	ND (0.0581)	0.188
SC-305	6 - 8 (ft)	6/30/2014	N	-	-	-	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	1.91	ND (0.192)	1.91
SC-306	6 - 8 (ft)	6/27/2014	N	-	-	-	ND (0.679)	ND (0.679)	ND (0.679)	ND (0.679)	ND (0.679)	ND (0.679)	ND (0.679)	14	ND (0.679)	14
SC-306	8 - 10 (ft)	6/27/2014	N	-	-	-	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
SC-307	10 - 12 (ft)	7/14/2014	N	-	-	-	ND (0.356)	ND (0.356)	ND (0.356)	ND (0.356)	ND (0.356)	1.18	ND (0.356)	4.97	ND (0.356)	6.15
SC-307	8 - 10 (ft)	7/14/2014	N	-	-	-	ND (2.05)	ND (2.05)	ND (2.05)	ND (2.05)	ND (2.05)	ND (2.05)	ND (2.05)	17	ND (2.05)	17
SC-308	8 - 10 (ft)	7/14/2014	FD	-	-	-	ND (0.061)	ND (0.061)	ND (0.061)	ND (0.061)	ND (0.061)	ND (0.061)	ND (0.061)	0.274	ND (0.061)	0.274
SC-308	8 - 10 (ft)	7/14/2014	N	-	-	-	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	ND (0.0616)	0.336	ND (0.0616)	0.336
SC-309	8 - 10 (ft)	7/14/2014	N	-	-	-	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)	ND (0.0601)
SC-310	6 - 8 (ft)	7/14/2014	N	-	-	-	ND (0.243)	ND (0.243)	ND (0.243)	ND (0.243)	ND (0.243)	ND (0.243)	ND (0.243)	2.36	ND (0.243)	2.36
SC-311	6 - 8 (ft)	7/14/2014	N	-	-	-	ND (0.361)	ND (0.361)	ND (0.361)	ND (0.361)	ND (0.361)	ND (0.361)	ND (0.361)	3.22	ND (0.361)	3.22
SC-312	10 - 12 (ft)	10/28/2014	N	-	-	-	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	35.3	ND (1.75)	35.3
SC-312	12 - 14 (ft)	10/28/2014	N	-	-	-	ND (0.0605)	ND (0.0605)	ND (0.0605)	ND (0.0605)	ND (0.0605)	ND (0.0605)	ND (0.0605)	1.21	ND (0.0605)	1.21
SC-312	8 - 10 (ft)	10/28/2014	N	-	-	-	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	15.6	ND (1.1)	15.6
SC-313	10 - 12 (ft)	10/28/2014	N	-	-	-	ND (0.178)	ND (0.178)	ND (0.178)	ND (0.178)	ND (0.178)	1.7	ND (0.178)	1.55	ND (0.178)	3.25
SC-313	8 - 10 (ft)	10/28/2014	FD	-	-	-	ND (0.595)	ND (0.595)	ND (0.595)	ND (0.595)	ND (0.595)	ND (0.595)	ND (0.595)	11.9	3.73	15.63
SC-313	8 - 10 (ft)	10/28/2014	N	-	-	-	ND (0.219)	ND (0.219)	ND (0.219)	ND (0.219)	ND (0.219)	ND (0.219)	ND (0.219)	3.72	ND (0.219)	3.72
SC-314	6 - 8 (ft)	10/28/2014	N	-	-	-	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	0.197	ND (0.0574)	0.197
SC-315	10 - 12 (ft)	10/28/2014	N	-	-	-	ND (0.186)	ND (0.186)	ND (0.186)	ND (0.186)	ND (0.186)	ND (0.186)	ND (0.186)	2.05	ND (0.186)	2.05
SC-315	4 - 6 (ft)	10/28/2014	N	-	-	-	ND (0.552)	ND (0.552)	ND (0.552)	ND (0.552)	ND (0.552)	ND (0.552)	ND (0.552)	12.3	3.86	16.16
SC-315	6 - 8 (ft)	10/28/2014	N	-	-	-	ND (0.22)	ND (0.22)	ND (0.22)	ND (0.22)	ND (0.22)	0.647	ND (0.22)	3.56	ND (0.22)	4.207
SC-316	10 - 12 (ft)	10/28/2014	N	-	-	-	ND (0.526)	ND (0.526)	ND (0.526)	ND (0.526)	ND (0.526)	ND (0.526)	ND (0.526)	11.6	ND (0.526)	11.6
SC-316	12 - 14 (ft)	10/28/2014	N	-	-	-	ND (0.0749)	ND (0.0749)	ND (0.0749)	ND (0.0749)	ND (0.0749)	ND (0.0749)	ND (0.0749)	0.442	ND (0.0749)	0.442
SC-316	8 - 10 (ft)	10/28/2014	FD	-	-	-	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	14.7	4.13	18.83
SC-316	8 - 10 (ft)	10/28/2014	N	-	-	-	ND (0.572)	ND (0.572)	ND (0.572)	ND (0.572)	ND (0.572)	ND (0.572)	ND (0.572)	12.9	3.67	16.57
SC-317	10 - 12 (ft)	11/5/2014	N	-	-	-	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	0.563	ND (0.0594)	0.563
SC-317	8 - 10 (ft)	11/5/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	1.81	ND (0.116)	1.81
SC-318	10 - 12 (ft)	11/5/2014	N	-	-	-	ND (0.0591)	ND (0.0591)	ND (0.0591)	ND (0.0591)	ND (0.0591)	ND (0.0591)	ND (0.0591)	0.109	ND (0.0591)	0.109
SC-318	8 - 10 (ft)	11/5/2014	N	-	-	-	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	ND (0.0536)	0.374	ND (0.0536)	0.374
SC-319	10 - 12 (ft)	11/5/2014	N	-	-	-	ND (0.41)	ND (0.41)	ND (0.41)	ND (0.41)	ND (0.41)	ND (0.41)	ND (0.41)	5.62	ND (0.41)	5.62
SC-319	8 - 10 (ft)	11/5/2014	N	-	-	-	ND (0.239)	ND (0.239)	ND (0.239)	ND (0.239)	ND (0.239)	ND (0.239)	ND (0.239)	3.22	ND (0.239)	3.22
SE-101	10 - 12 (ft)	10/30/2013	FD	-	-	-	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)
SE-101	10 - 12 (ft)	10/30/2013	N	-	-	-	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)
SE-101	6 - 8 (ft)	10/30/2013	N	-	-	-	ND (0.15)	ND (0.15)	ND (0.15)	ND (0.15)	ND (0.15)	ND (0.15)	ND (0.15)	0.238	ND (0.15)	0.238
SE-102	10 - 12 (ft)	10/29/2013	N	-	-	-	ND (11.6)	ND (11.6)	ND (11.6)	ND (11.6)	ND (11.6)	41.4 P	ND (11.6)	346	122	509.4
SE-102	12 - 14 (ft)	10/29/2013	N	-	-	-	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	0.0574	ND (0.0552)	0.0574
SE-102	6 - 8 (ft)	10/29/2013	N	-	-	-	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	0.167	ND (0.0586)	0.167
SE-103	10 - 12 (ft)	10/28/2013	N	-	-	-	ND (0.0793)	ND (0.0793)	ND (0.0793)	ND (0.0793)	ND (0.0793)	ND (0.0793)	ND (0.0793)	1.11	0.354	1.464
SE-201	10 - 12 (ft)	5/29/2014	N	-	-	-	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)
SE-202	10 - 12 (ft)	5/29/2014	FD	-	-	-	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	ND (0.0574)	0.118	ND (0.0574)	0.118
SE-202	10 - 12 (ft)	5/29/2014	N	-	-	-	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	0.292	ND (0.0726)	0.292
SG-001	6 - 8 (ft)	6/11/2014	N	-	-	-	ND (0.574)	ND (0.574)	ND (0.574)	ND (0.574)	ND (0.574)	1.86	ND (0.574)	5.57	ND (0.574)	7.43
SG-001	8 - 10 (ft)	7/14/2014	N	-	-	-	ND (0.0766)	ND (0.0766)	ND (0.0766)	ND (0.0766)	ND (0.0766)	ND (0.0766)	ND (0.0766)	ND (0.0766)	ND (0.0766)	ND (0.0766)
SG-001	9 - 11 (ft)	10/31/2013	N	-	-	-	ND (0.0777)	ND (0.0777)	ND (0.0777)	ND (0.0777)	ND (0.0777)	ND (0.0777)	ND (0.0777)	ND (0.0777)	ND (0.0777)	ND (0.0777)
SG-002	6 - 8 (ft)	11/7/2013	FD	-	-	-	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)	ND (0.0709)

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
SG-002	6 - 8 (ft)	11/7/2013	N	-	-	-	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)	ND (0.0684)
SG-002	8 - 10 (ft)	11/7/2013	N	-	-	-	ND (0.0672)	ND (0.0672)	ND (0.0672)	ND (0.0672)	ND (0.0672)	ND (0.0672)	ND (0.0672)	ND (0.0672)	ND (0.0672)	ND (0.0672)
SG-004	3 - 5 (ft)	10/31/2013	N	-	-	-	ND (55.7)	ND (55.7)	ND (55.7)	ND (55.7)	ND (55.7)	89 P	ND (55.7)	1690	647	2426
SG-006	4 - 6 (ft)	7/2/2014	FD	-	-	-	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	ND (0.221)	2.61	ND (0.221)	2.61
SG-006	4 - 6 (ft)	7/2/2014	N	-	-	-	ND (0.215)	ND (0.215)	ND (0.215)	ND (0.215)	ND (0.215)	ND (0.215)	ND (0.215)	1.84	ND (0.215)	1.84
SG-006	6 - 8 (ft)	7/2/2014	N	-	-	-	ND (0.0742)	ND (0.0742)	ND (0.0742)	ND (0.0742)	ND (0.0742)	ND (0.0742)	ND (0.0742)	ND (0.0742)	ND (0.0742)	ND (0.0742)
SG-101	3 - 5 (ft)	10/31/2013	N	-	-	-	ND (0.268)	ND (0.268)	ND (0.268)	ND (0.268)	ND (0.268)	1.03 P	ND (0.268)	4.1	ND (0.268)	5.13
SG-102	7 - 9 (ft)	10/31/2013	FD	-	-	-	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)
SG-102	7 - 9 (ft)	10/31/2013	N	-	-	-	ND (0.0673)	ND (0.0673)	ND (0.0673)	ND (0.0673)	ND (0.0673)	ND (0.0673)	ND (0.0673)	0.0945	ND (0.0673)	0.0945
SG-103	8 - 10 (ft)	10/29/2013	N	-	-	-	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	0.109	ND (0.0674)	0.109
SG-104	3 - 5 (ft)	10/30/2013	N	-	-	-	ND (2.35)	ND (2.35)	ND (2.35)	ND (2.35)	6.93	9.77 P	ND (2.35)	36.4	12	65.1
SG-104	5 - 7 (ft)	10/30/2013	N	-	-	-	ND (0.684)	ND (0.684)	ND (0.684)	ND (0.684)	ND (0.684)	ND (0.684)	ND (0.684)	23.6	ND (0.684)	23.6
SG-104	7 - 9 (ft)	10/30/2013	N	-	-	-	ND (0.077)	ND (0.077)	ND (0.077)	ND (0.077)	ND (0.077)	0.162	ND (0.077)	0.365	0.0971	0.6241
SG-201	4 - 6 (ft)	6/11/2014	FD	-	-	-	ND (1.8)	ND (1.8)	ND (1.8)	ND (1.8)	ND (1.8)	6.92	ND (1.8)	26.2	ND (1.8)	33.12
SG-201	4 - 6 (ft)	6/11/2014	N	-	-	-	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	9.05	ND (1.71)	28.7	ND (1.71)	37.75
SG-201	6 - 8 (ft)	6/11/2014	N	-	-	-	ND (0.16)	ND (0.16)	ND (0.16)	ND (0.16)	ND (0.16)	ND (0.16)	ND (0.16)	1.85	ND (0.16)	1.85
SG-202	4 - 6 (ft)	6/11/2014	N	-	-	-	ND (0.604)	ND (0.604)	ND (0.604)	ND (0.604)	ND (0.604)	2.87	ND (0.604)	13.7	4.95	21.52
SG-202	6 - 8 (ft)	6/11/2014	N	-	-	-	ND (0.388)	ND (0.388)	ND (0.388)	ND (0.388)	ND (0.388)	ND (0.388)	ND (0.388)	6	ND (0.388)	6
SG-203	3 - 5 (ft)	6/11/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.245	ND (0.116)	0.774	ND (0.116)	1.019
SG-301	4 - 6 (ft)	7/1/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	1.44	ND (0.114)	1.44
SG-302	4 - 6 (ft)	7/1/2014	FD	-	-	-	ND (0.0641)	ND (0.0641)	ND (0.0641)	ND (0.0641)	ND (0.0641)	ND (0.0641)	ND (0.0641)	0.752	ND (0.0641)	0.752
SG-302	4 - 6 (ft)	7/1/2014	N	-	-	-	ND (0.203)	ND (0.203)	ND (0.203)	ND (0.203)	ND (0.203)	ND (0.203)	ND (0.203)	0.46	ND (0.203)	0.46
SG-303	4 - 6 (ft)	7/2/2014	N	-	-	-	ND (0.0673)	ND (0.0673)	ND (0.0673)	ND (0.0673)	ND (0.0673)	ND (0.0673)	ND (0.0673)	0.204	ND (0.0673)	0.204
SG-304	4 - 6 (ft)	7/2/2014	N	-	-	-	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	0.563	ND (0.0595)	0.563
SH-001	2 - 4 (ft)	10/23/2013	N	-	-	-	ND (0.162)	ND (0.162)	ND (0.162)	ND (0.162)	ND (0.162)	ND (0.162)	ND (0.162)	1.65	ND (0.162)	1.65
SH-101	0 - 2 (ft)	10/29/2013	N	-	-	-	ND (0.0525)	ND (0.0525)	ND (0.0525)	ND (0.0525)	ND (0.0525)	ND (0.0525)	ND (0.0525)	0.0543	ND (0.0525)	0.0543
SH-102	0 - 2 (ft)	10/30/2013	N	-	-	-	ND (0.0591)	ND (0.0591)	ND (0.0591)	ND (0.0591)	ND (0.0591)	ND (0.0591)	ND (0.0591)	0.827	0.263	1.09
SH-103	0 - 2 (ft)	10/30/2013	N	-	-	-	ND (0.0532)	ND (0.0532)	ND (0.0532)	ND (0.0532)	ND (0.0532)	ND (0.0532)	ND (0.0532)	0.128	ND (0.0532)	0.128
SH-104	0 - 2 (ft)	10/31/2013	N	-	-	-	ND (0.528)	ND (0.528)	ND (0.528)	ND (0.528)	ND (0.528)	1.64 P	ND (0.528)	7	ND (0.528)	8.64
SI-101	0 - 2 (ft)	10/17/2013	N	604	280	211	-	-	-	-	-	-	-	-	-	-
SI-102	0 - 2 (ft)	10/17/2013	N	3430	543	888	-	-	-	-	-	-	-	-	-	-
SI-103	0 - 2 (ft)	10/17/2013	N	1970	2580	787	-	-	-	-	-	-	-	-	-	-
SI-104	0 - 2 (ft)	10/23/2013	N	1480	1020	388	-	-	-	-	-	-	-	-	-	-
SI-201	0 - 2 (ft)	5/30/2014	N	1420	416	650	-	-	-	-	-	-	-	-	-	-
SI-202	0 - 2 (ft)	5/30/2014	N	3010	344	445	-	-	-	-	-	-	-	-	-	-
SJ-101	0 - 2 (ft)	10/16/2013	N	1970	740	491	-	-	-	-	-	-	-	-	-	-
SJ-102	0 - 2 (ft)	10/16/2013	N	365	115	52.7	-	-	-	-	-	-	-	-	-	-
SJ-103	0 - 2 (ft)	10/16/2013	N	104	81.3	28.4	-	-	-	-	-	-	-	-	-	-
SJ-104	0 - 2 (ft)	10/16/2013	N	921	361	133	-	-	-	-	-	-	-	-	-	-
SK-101	0 - 2 (ft)	10/17/2013	N	3420	594	117	-	-	-	-	-	-	-	-	-	-
SK-102	0 - 1.5 (ft)	10/23/2013	N	14.3	41.3	36.8	-	-	-	-	-	-	-	-	-	-

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
SK-103	0 - 2 (ft)	10/17/2013	N	1010	56.1	60	-	-	-	-	-	-	-	-	-	-
SK-104	0 - 2 (ft)	10/17/2013	N	1200	129	59.9	-	-	-	-	-	-	-	-	-	-
SL-101	2 - 4 (ft)	10/22/2013	N	-	-	-	ND (0.552)	ND (0.552)	ND (0.552)	ND (0.552)	ND (0.552)	ND (0.552)	ND (0.552)	14	ND (0.552)	14
SL-101	4 - 6 (ft)	11/8/2013	N	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	3.46	1.38	4.84
SL-102	2 - 4 (ft)	10/22/2013	N	-	-	-	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	0.186	ND (0.0575)	0.186
SL-103	2 - 4 (ft)	10/22/2013	N	-	-	-	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	0.551	ND (0.0552)	0.551
SL-201	2 - 4 (ft)	5/29/2014	N	-	-	-	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)
SL-202	2 - 4 (ft)	5/29/2014	FD	-	-	-	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	ND (0.06)	0.0454 J	ND (0.06)	0.0454 J
SL-202	2 - 4 (ft)	5/29/2014	N	-	-	-	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	0.036 J	ND (0.0621)	0.036 J
SL-203	2 - 4 (ft)	5/28/2014	N	-	-	-	ND (0.0548)	ND (0.0548)	ND (0.0548)	ND (0.0548)	ND (0.0548)	ND (0.0548)	ND (0.0548)	0.436	ND (0.0548)	0.436
SM-101	0 - 2 (ft)	10/22/2013	N	-	-	-	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	ND (0.0545)	1.29	ND (0.0545)	1.29
SM-102	0 - 2 (ft)	10/23/2013	N	-	-	-	ND (5.8)	ND (5.8)	ND (5.8)	ND (5.8)	ND (5.8)	86.4	ND (5.8)	110	ND (5.8)	196.4
SM-102	2 - 4 (ft)	11/21/2013	FD	-	-	-	ND (2.2)	ND (2.2)	ND (2.2)	ND (2.2)	ND (2.2)	30.8	ND (2.2)	28.4	ND (2.2)	59.2
SM-102	2 - 4 (ft)	11/21/2013	N	-	-	-	ND (3.23)	ND (3.23)	ND (3.23)	ND (3.23)	ND (3.23)	44.3	ND (3.23)	47.3	ND (3.23)	91.6
SM-102	4 - 6 (ft)	11/21/2013	N	-	-	-	ND (0.328)	ND (0.328)	ND (0.328)	ND (0.328)	ND (0.328)	9.83	4.44	ND (0.328)	ND (0.328)	14.27
SM-201	0 - 2 (ft)	5/28/2014	FD	-	-	-	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	0.132	ND (0.0575)	0.132
SM-201	0 - 2 (ft)	5/28/2014	N	-	-	-	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	0.159	ND (0.0588)	0.159
SM-201	4 - 6 (ft)	5/28/2014	N	-	-	-	ND (0.0792)	ND (0.0792)	ND (0.0792)	ND (0.0792)	ND (0.0792)	ND (0.0792)	ND (0.0792)	1.39	ND (0.0792)	1.39
SM-201	6 - 8 (ft)	5/29/2014	N	-	-	-	ND (0.0607)	ND (0.0607)	ND (0.0607)	ND (0.0607)	ND (0.0607)	ND (0.0607)	ND (0.0607)	0.098	ND (0.0607)	0.098
SM-202	0 - 2 (ft)	5/30/2014	N	-	-	-	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	ND (0.0571)	0.0439 J	ND (0.0571)	0.0439 J
SM-202	4 - 6 (ft)	5/30/2014	N	-	-	-	ND (0.268)	ND (0.268)	ND (0.268)	ND (0.268)	ND (0.268)	ND (0.268)	ND (0.268)	2.76	ND (0.268)	2.76
SM-203	0 - 2 (ft)	5/30/2014	N	-	-	-	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	1.96	ND (0.54)	1.96
SM-203	2 - 4 (ft)	5/30/2014	N	-	-	-	ND (0.181)	ND (0.181)	ND (0.181)	ND (0.181)	ND (0.181)	4.91	ND (0.181)	4.97	ND (0.181)	9.88
SM-203	4 - 6 (ft)	11/20/2014	N	-	-	-	ND (0.577)	ND (0.577)	ND (0.577)	ND (0.577)	ND (0.577)	5.14	ND (0.577)	2.1	ND (0.577)	7.24
SM-203	6 - 8 (ft)	11/20/2014	N	-	-	-	ND (1.43)	ND (1.43)	ND (1.43)	ND (1.43)	ND (1.43)	12.7	ND (1.43)	10	ND (1.43)	22.7
SM-204	6 - 8 (ft)	11/20/2014	N	-	-	-	ND (0.652)	ND (0.652)	ND (0.652)	ND (0.652)	ND (0.652)	10.9	ND (0.652)	4.55 P	ND (0.652)	15.45
SM-204	8 - 10 (ft)	11/20/2014	N	-	-	-	ND (0.314)	ND (0.314)	ND (0.314)	ND (0.314)	ND (0.314)	4.26	ND (0.314)	3.45	ND (0.314)	7.71
SN-001	6 - 8 (ft)	11/8/2013	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.619	ND (0.111)	1.88	ND (0.111)	2.499
SN-101	2 - 4 (ft)	11/11/2013	N	-	-	-	ND (0.279)	ND (0.279)	ND (0.279)	ND (0.279)	ND (0.279)	0.911	ND (0.279)	3.02	ND (0.279)	3.931
SN-101	4 - 6 (ft)	11/11/2013	N	-	-	-	ND (0.0622)	ND (0.0622)	ND (0.0622)	ND (0.0622)	ND (0.0622)	0.158 P	ND (0.0622)	1.41	ND (0.0622)	1.568
SN-102	2 - 4 (ft)	11/21/2013	FD	-	-	-	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)
SN-102	2 - 4 (ft)	11/21/2013	N	-	-	-	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)
SN-102	4 - 6 (ft)	11/21/2013	N	-	-	-	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	0.201	ND (0.0587)	0.201
SO-101	0 - 2 (ft)	10/4/2013	N	-	-	-	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	ND (0.057)	0.23	ND (0.057)	0.23
SO-102	0 - 2 (ft)	10/4/2013	N	-	-	-	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	0.753	ND (0.056)	0.753
SO-103	0 - 2 (ft)	10/4/2013	FD	-	-	-	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)	ND (0.0549)
SO-103	0 - 2 (ft)	10/4/2013	N	-	-	-	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)
SP-001	0 - 2 (ft)	6/11/2014	N	-	-	-	ND (0.539)	ND (0.539)	ND (0.539)	ND (0.539)	ND (0.539)	ND (0.539)	ND (0.539)	9.83	ND (0.539)	9.83
SP-001	2 - 4 (ft)	10/30/2013	N	-	-	-	ND (0.0516)	ND (0.0516)	ND (0.0516)	ND (0.0516)	ND (0.0516)	ND (0.0516)	ND (0.0516)	0.581	ND (0.0516)	0.581
SP-001	4 - 6 (ft)	10/30/2013	N	-	-	-	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)	0.0615	ND (0.0521)	1.07	ND (0.0521)	1.1315
SP-001	6 - 8 (ft)	11/8/2013	N	-	-	-	ND (0.182)	ND (0.182)	ND (0.182)	ND (0.182)	ND (0.182)	0.622	ND (0.182)	3.34	ND (0.182)	3.962

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
SP-101	0 - 2 (ft)	10/3/2013	N	-	-	-	ND (0.0534)	ND (0.0534)	ND (0.0534)	ND (0.0534)	ND (0.0534)	ND (0.0534)	ND (0.0534)	2.08	ND (0.0534)	2.08
SP-101	2 - 4 (ft)	10/31/2013	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	2.46	0.766	3.226
SP-102	0 - 2 (ft)	10/3/2013	N	-	-	-	ND (0.531)	ND (0.531)	ND (0.531)	ND (0.531)	ND (0.531)	ND (0.531)	ND (0.531)	11.3	ND (0.531)	11.3
SP-102	2 - 4 (ft)	11/6/2013	N	-	-	-	ND (0.269)	ND (0.269)	ND (0.269)	ND (0.269)	ND (0.269)	ND (0.269)	ND (0.269)	4.79	ND (0.269)	4.79
SP-103	0 - 2 (ft)	10/3/2013	N	-	-	-	ND (0.158)	ND (0.158)	ND (0.158)	ND (0.158)	ND (0.158)	ND (0.158)	ND (0.158)	2.97	ND (0.158)	2.97
SP-103	2 - 4 (ft)	10/31/2013	N	-	-	-	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	ND (0.056)	0.218	ND (0.056)	0.218
SP-104	0 - 2 (ft)	10/3/2013	N	-	-	-	ND (0.425)	ND (0.425)	ND (0.425)	ND (0.425)	ND (0.425)	ND (0.425)	ND (0.425)	7.51	ND (0.425)	7.51
SP-105	0 - 2 (ft)	10/3/2013	N	-	-	-	ND (0.319)	ND (0.319)	ND (0.319)	ND (0.319)	ND (0.319)	ND (0.319)	ND (0.319)	5.4	ND (0.319)	5.4
SP-105	2 - 4 (ft)	11/8/2013	N	-	-	-	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)
SP-106	0 - 2 (ft)	10/3/2013	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	1.4	ND (0.109)	1.4
SP-201	0 - 2 (ft)	10/27/2014	N	-	-	-	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	5.54	ND (0.166)	5.54
SQ-001	2 - 4 (ft)	10/30/2013	N	-	-	-	ND (0.217)	ND (0.217)	ND (0.217)	ND (0.217)	ND (0.217)	ND (0.217)	ND (0.217)	3.29	ND (0.217)	3.29
SQ-101	0 - 2 (ft)	11/5/2013	N	-	-	-	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	2.95	0.745	3.695
SQ-101	2 - 4 (ft)	11/5/2013	N	-	-	-	ND (0.382)	ND (0.382)	ND (0.382)	ND (0.382)	ND (0.382)	ND (0.382)	ND (0.382)	5.88	1.57	7.45
SQ-102	0 - 2 (ft)	11/9/2013	FD	-	-	-	ND (5.37)	ND (5.37)	ND (5.37)	ND (5.37)	ND (5.37)	ND (5.37)	ND (5.37)	135	40.9	175.9
SQ-102	0 - 2 (ft)	11/9/2013	N	-	-	-	ND (5.54)	ND (5.54)	ND (5.54)	ND (5.54)	ND (5.54)	ND (5.54)	ND (5.54)	245	71.5	316.5
SQ-102	2 - 4 (ft)	11/9/2013	N	-	-	-	ND (0.519)	ND (0.519)	ND (0.519)	ND (0.519)	ND (0.519)	ND (0.519)	ND (0.519)	20.7	ND (0.519)	20.7
SQ-102	4 - 6 (ft)	11/9/2013	N	-	-	-	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	0.913	ND (0.0554)	0.913
SQ-103	0 - 2 (ft)	11/5/2013	N	-	-	-	ND (0.167)	ND (0.167)	ND (0.167)	ND (0.167)	ND (0.167)	ND (0.167)	ND (0.167)	3.37	0.95	4.32
SQ-103	2 - 4 (ft)	11/5/2013	N	-	-	-	ND (1.11)	ND (1.11)	ND (1.11)	ND (1.11)	ND (1.11)	ND (1.11)	ND (1.11)	25.7	7.49	33.19
SQ-103	4 - 6 (ft)	11/5/2013	N	-	-	-	ND (0.559)	ND (0.559)	ND (0.559)	ND (0.559)	ND (0.559)	ND (0.559)	ND (0.559)	24.6	ND (0.559)	24.6
SQ-103	6 - 8 (ft)	6/6/2014	N	-	-	-	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	0.744	ND (0.0595)	0.744
SQ-104	0 - 2 (ft)	11/6/2013	N	-	-	-	ND (1.58)	ND (1.58)	ND (1.58)	ND (1.58)	ND (1.58)	ND (1.58)	ND (1.58)	38.2	ND (1.58)	38.2
SQ-104	2 - 4 (ft)	11/6/2013	N	-	-	-	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	2.11	ND (0.107)	2.11
SQ-104	4 - 6 (ft)	11/6/2013	N	-	-	-	ND (0.162)	ND (0.162)	ND (0.162)	ND (0.162)	ND (0.162)	ND (0.162)	ND (0.162)	3.14	ND (0.162)	3.14
SQ-105	0 - 2 (ft)	11/4/2013	N	-	-	-	ND (1.07)	ND (1.07)	ND (1.07)	ND (1.07)	ND (1.07)	ND (1.07)	ND (1.07)	20.6	4.8	25.4
SQ-105	2 - 4 (ft)	11/4/2013	N	-	-	-	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	1.64 P	ND (0.54)	23.3	6.13	31.07
SQ-105	4 - 6 (ft)	11/4/2013	N	-	-	-	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	ND (0.0552)	0.288	ND (0.0552)	0.288
SQ-106	0 - 2 (ft)	11/4/2013	N	-	-	-	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	1.2	0.366 P	1.566
SQ-106	2 - 4 (ft)	11/4/2013	N	-	-	-	ND (0.369)	ND (0.369)	ND (0.369)	ND (0.369)	ND (0.369)	ND (0.369)	ND (0.369)	8.05	2.35	10.4
SQ-201	4 - 6 (ft)	6/12/2014	N	-	-	-	ND (0.0597)	ND (0.0597)	ND (0.0597)	ND (0.0597)	ND (0.0597)	ND (0.0597)	ND (0.0597)	0.498	ND (0.0597)	0.498
SQ-202	0 - 2 (ft)	6/12/2014	FD	-	-	-	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	25.7	ND (1.1)	25.7
SQ-202	0 - 2 (ft)	6/12/2014	N	-	-	-	ND (1.64)	ND (1.64)	ND (1.64)	ND (1.64)	ND (1.64)	ND (1.64)	ND (1.64)	33.3	ND (1.64)	33.3
SQ-202	4 - 6 (ft)	6/12/2014	N	-	-	-	ND (2.92)	ND (2.92)	ND (2.92)	ND (2.92)	ND (2.92)	ND (2.92)	ND (2.92)	24.5	ND (2.92)	24.5
SQ-202	6 - 8 (ft)	6/12/2014	N	-	-	-	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	ND (0.0563)	0.0375 J	ND (0.0563)	0.0375 J
SQ-203	0 - 2 (ft)	5/16/2014	N	-	-	-	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	6.16	ND (0.228)	6.16
SQ-203	2 - 4 (ft)	5/16/2014	N	-	-	-	ND (0.171)	ND (0.171)	ND (0.171)	ND (0.171)	ND (0.171)	ND (0.171)	ND (0.171)	4.31	ND (0.171)	4.31
SQ-204	0 - 2 (ft)	6/11/2014	N	-	-	-	ND (0.32)	ND (0.32)	ND (0.32)	ND (0.32)	ND (0.32)	ND (0.32)	ND (0.32)	3.46	ND (0.32)	3.46
SQ-204	2 - 4 (ft)	6/11/2014	N	-	-	-	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)
SQ-301	4 - 6 (ft)	6/27/2014	N	-	-	-	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	ND (0.0527)	0.381	ND (0.0527)	0.381
SQ-303	2 - 4 (ft)	10/29/2014	FD	-	-	-	ND (0.212)	ND (0.212)	ND (0.212)	ND (0.212)	ND (0.212)	ND (0.212)	ND (0.212)	5.09	ND (0.212)	5.09

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
SQ-303	2 - 4 (ft)	10/29/2014	N	-	-	-	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	ND (0.165)	3.31	ND (0.165)	3.31
SR-101	0 - 2 (ft)	6/2/2014	N	1100	120	63.2	-	-	-	-	-	-	-	-	-	-
SR-102	0 - 2 (ft)	6/2/2014	FD	-	122	-	-	-	-	-	-	-	-	-	-	-
SR-102	0 - 2 (ft)	6/2/2014	N	1160	95.2	61.4	-	-	-	-	-	-	-	-	-	-
SR-103	0 - 2 (ft)	6/2/2014	N	-	1960	-	-	-	-	-	-	-	-	-	-	-
SR-104	0 - 2 (ft)	6/2/2014	N	-	4930	-	-	-	-	-	-	-	-	-	-	-
SR-201	0 - 2 (ft)	7/1/2014	N	7650	121	87.3	-	-	-	-	-	-	-	-	-	-
SR-202	0 - 2 (ft)	7/1/2014	N	-	43100	-	-	-	-	-	-	-	-	-	-	-
SR-203	0 - 2 (ft)	7/1/2014	FD	-	2020	-	-	-	-	-	-	-	-	-	-	-
SR-203	0 - 2 (ft)	7/1/2014	N	-	1600	-	-	-	-	-	-	-	-	-	-	-
SR-204	0 - 2 (ft)	7/1/2014	N	1160	181	316	-	-	-	-	-	-	-	-	-	-
SR-205	0 - 2 (ft)	7/1/2014	N	3070	60.8	402	-	-	-	-	-	-	-	-	-	-
SR-301	0 - 2 (ft)	7/10/2014	N	4250	382	468	-	-	-	-	-	-	-	-	-	-
SS-101	10 - 12 (ft)	7/17/2014	N	-	-	-	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	25.2	ND (1.17)	25.2
SS-101	12 - 14 (ft)	7/17/2014	N	-	-	-	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	2.62	ND (0.0584)	2.62
SS-101	4 - 6 (ft)	7/17/2014	N	-	-	-	ND (15.9)	ND (15.9)	ND (15.9)	ND (15.9)	ND (15.9)	ND (15.9)	ND (15.9)	276	ND (15.9)	276
SS-101	8 - 10 (ft)	7/17/2014	N	-	-	-	ND (5.78)	ND (5.78)	ND (5.78)	ND (5.78)	ND (5.78)	ND (5.78)	ND (5.78)	178	ND (5.78)	178
SS-102	10 - 12 (ft)	7/17/2014	N	-	-	-	ND (3.24)	ND (3.24)	ND (3.24)	ND (3.24)	ND (3.24)	ND (3.24)	ND (3.24)	66.8	ND (3.24)	66.8
SS-102	12 - 14 (ft)	7/17/2014	N	-	-	-	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)
SS-102	4 - 6 (ft)	7/17/2014	N	-	-	-	ND (6.62)	ND (6.62)	ND (6.62)	ND (6.62)	ND (6.62)	29.4	ND (6.62)	124	ND (6.62)	153.4
SS-102	6 - 8 (ft)	7/17/2014	N	-	-	-	ND (6.85)	ND (6.85)	ND (6.85)	ND (6.85)	ND (6.85)	27.6	ND (6.85)	161	ND (6.85)	188.6
SS-102	8 - 10 (ft)	7/17/2014	N	-	-	-	ND (12.4)	ND (12.4)	ND (12.4)	ND (12.4)	ND (12.4)	ND (12.4)	ND (12.4)	201	ND (12.4)	201
SS-103	10 - 12 (ft)	7/17/2014	N	-	-	-	ND (2.3)	ND (2.3)	ND (2.3)	ND (2.3)	ND (2.3)	ND (2.3)	ND (2.3)	49	ND (2.3)	49
SS-103	12 - 14 (ft)	7/17/2014	N	-	-	-	ND (11.9)	ND (11.9)	ND (11.9)	ND (11.9)	ND (11.9)	ND (11.9)	ND (11.9)	238	ND (11.9)	238
SS-103	4 - 6 (ft)	7/17/2014	N	-	-	-	ND (27.9)	ND (27.9)	ND (27.9)	ND (27.9)	ND (27.9)	ND (27.9)	ND (27.9)	555	ND (27.9)	555
SS-103	8 - 10 (ft)	7/17/2014	N	-	-	-	ND (17.2)	ND (17.2)	ND (17.2)	ND (17.2)	ND (17.2)	ND (17.2)	ND (17.2)	338	ND (17.2)	338
SS-104	10 - 12 (ft)	7/17/2014	N	-	-	-	ND (22.1)	ND (22.1)	ND (22.1)	ND (22.1)	ND (22.1)	ND (22.1)	ND (22.1)	535	ND (22.1)	535
SS-104	12 - 14 (ft)	7/17/2014	N	-	-	-	ND (5.93)	ND (5.93)	ND (5.93)	ND (5.93)	ND (5.93)	ND (5.93)	ND (5.93)	132	ND (5.93)	132
SS-104	4 - 6 (ft)	7/17/2014	N	-	-	-	ND (28.2)	ND (28.2)	ND (28.2)	ND (28.2)	ND (28.2)	ND (28.2)	ND (28.2)	535	ND (28.2)	535
SS-104	6 - 8 (ft)	7/17/2014	N	-	-	-	ND (24.7)	ND (24.7)	ND (24.7)	ND (24.7)	ND (24.7)	ND (24.7)	ND (24.7)	450	ND (24.7)	450
SS-104	8 - 10 (ft)	7/17/2014	N	-	-	-	ND (6.14)	ND (6.14)	ND (6.14)	ND (6.14)	ND (6.14)	ND (6.14)	ND (6.14)	142	ND (6.14)	142
SS-105	10 - 12 (ft)	7/17/2014	N	-	-	-	ND (0.28)	ND (0.28)	ND (0.28)	ND (0.28)	ND (0.28)	ND (0.28)	ND (0.28)	2	ND (0.28)	2
SS-105	4 - 6 (ft)	7/17/2014	N	-	-	-	ND (4.3)	ND (4.3)	ND (4.3)	ND (4.3)	ND (4.3)	ND (4.3)	ND (4.3)	53.3	ND (4.3)	53.3
SS-105	6 - 8 (ft)	7/17/2014	N	-	-	-	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	0.0554 J	ND (0.0593)	0.0554 J
SS-105	8 - 10 (ft)	7/17/2014	N	-	-	-	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	5.71	ND (0.299)	5.71
SS-106	4 - 6 (ft)	7/17/2014	N	-	-	-	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	1.75	ND (0.166)	1.75
SS-106	6 - 8 (ft)	7/17/2014	N	-	-	-	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	46.3	ND (1.2)	46.3
SS-106	8 - 10 (ft)	7/17/2014	N	-	-	-	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	2.16	ND (0.166)	2.16
SS-107	10 - 12 (ft)	7/17/2014	N	-	-	-	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	0.195	ND (0.0583)	0.195
SS-107	4 - 6 (ft)	7/17/2014	N	-	-	-	ND (0.551)	ND (0.551)	ND (0.551)	ND (0.551)	ND (0.551)	ND (0.551)	ND (0.551)	12.7	ND (0.551)	12.7
SS-107	6 - 8 (ft)	7/17/2014	N	-	-	-	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	ND (0.0584)	0.173	ND (0.0584)	0.173

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
SS-107	8 - 10 (ft)	7/17/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	1.04	ND (0.119)	1.04
SS-201	10 - 12 (ft)	10/27/2014	N	-	-	-	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	ND (0.0598)	0.758	ND (0.0598)	0.758
SS-201	4 - 6 (ft)	10/27/2014	FD	-	-	-	ND (0.563)	ND (0.563)	ND (0.563)	ND (0.563)	ND (0.563)	ND (0.563)	ND (0.563)	14.6	ND (0.563)	14.6
SS-201	4 - 6 (ft)	10/27/2014	N	-	-	-	ND (0.55)	ND (0.55)	ND (0.55)	ND (0.55)	ND (0.55)	ND (0.55)	ND (0.55)	12.9	ND (0.55)	12.9
SS-201	6 - 8 (ft)	10/27/2014	N	-	-	-	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	2.16	ND (0.0544)	0.954	ND (0.0544)	3.114
SS-202	4 - 6 (ft)	10/27/2014	N	-	-	-	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	5.18	ND (0.177)	5.18
SS-203	4 - 6 (ft)	10/27/2014	FD	-	-	-	ND (2.77)	ND (2.77)	ND (2.77)	ND (2.77)	ND (2.77)	ND (2.77)	ND (2.77)	71.9	ND (2.77)	71.9
SS-203	4 - 6 (ft)	10/27/2014	N	-	-	-	ND (3.45)	ND (3.45)	ND (3.45)	ND (3.45)	ND (3.45)	ND (3.45)	ND (3.45)	101	ND (3.45)	101
SS-203	6 - 8 (ft)	10/27/2014	N	-	-	-	ND (1.55)	ND (1.55)	ND (1.55)	ND (1.55)	ND (1.55)	ND (1.55)	ND (1.55)	36.6	ND (1.55)	36.6
SS-203	8 - 10 (ft)	10/27/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	2.39	ND (0.112)	2.39
SS-204	10 - 12 (ft)	10/24/2014	N	-	-	-	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	0.81	ND (0.0585)	0.81
SS-204	4 - 6 (ft)	10/24/2014	FD	-	-	-	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	22.4	ND (1.09)	22.4
SS-204	4 - 6 (ft)	10/24/2014	N	-	-	-	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	23.5	ND (1.09)	23.5
SS-204	6 - 8 (ft)	10/24/2014	N	-	-	-	ND (0.607)	ND (0.607)	ND (0.607)	ND (0.607)	ND (0.607)	ND (0.607)	ND (0.607)	15.9	ND (0.607)	15.9
SS-204	8 - 10 (ft)	10/24/2014	N	-	-	-	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	ND (0.058)	1.28	ND (0.058)	1.28
SS-205	10 - 12 (ft)	10/24/2014	N	-	-	-	ND (0.176)	ND (0.176)	ND (0.176)	ND (0.176)	ND (0.176)	2.47	ND (0.176)	3.12	ND (0.176)	5.59
SS-205	4 - 6 (ft)	10/24/2014	N	-	-	-	ND (0.542)	ND (0.542)	ND (0.542)	ND (0.542)	6.89	ND (0.542)	ND (0.542)	15.1	ND (0.542)	21.99
SS-205	6 - 8 (ft)	10/24/2014	N	-	-	-	ND (4.69)	ND (4.69)	ND (4.69)	ND (4.69)	ND (4.69)	110	ND (4.69)	78.6	ND (4.69)	188.6
SS-205	8 - 10 (ft)	10/24/2014	N	-	-	-	ND (0.477)	ND (0.477)	ND (0.477)	ND (0.477)	ND (0.477)	ND (0.477)	ND (0.477)	6.1	ND (0.477)	6.1
SS-206	10 - 12 (ft)	10/24/2014	N	-	-	-	ND (1.86)	ND (1.86)	ND (1.86)	ND (1.86)	ND (1.86)	ND (1.86)	ND (1.86)	90.2	ND (1.86)	90.2
SS-206	12 - 14 (ft)	10/24/2014	N	-	-	-	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	2.62	ND (0.0621)	2.62
SS-206	4 - 6 (ft)	10/24/2014	N	-	-	-	ND (12)	ND (12)	ND (12)	ND (12)	ND (12)	ND (12)	ND (12)	238	ND (12)	238
SS-207	10 - 12 (ft)	10/27/2014	N	-	-	-	ND (2.76)	ND (2.76)	ND (2.76)	ND (2.76)	ND (2.76)	ND (2.76)	ND (2.76)	58.4	ND (2.76)	58.4
SS-207	12 - 14 (ft)	10/27/2014	N	-	-	-	ND (0.298)	ND (0.298)	ND (0.298)	ND (0.298)	ND (0.298)	ND (0.298)	ND (0.298)	4.72	ND (0.298)	4.72
SS-207	4 - 6 (ft)	10/27/2014	FD	-	-	-	ND (4.81)	ND (4.81)	ND (4.81)	ND (4.81)	ND (4.81)	ND (4.81)	ND (4.81)	101	ND (4.81)	101
SS-207	4 - 6 (ft)	10/27/2014	N	-	-	-	ND (4.16)	ND (4.16)	ND (4.16)	ND (4.16)	ND (4.16)	ND (4.16)	ND (4.16)	102	ND (4.16)	102
SS-208	10 - 12 (ft)	11/3/2014	N	-	-	-	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)	ND (0.0594)
SS-208	4 - 6 (ft)	11/3/2014	N	-	-	-	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	ND (0.56)	19.4	ND (0.56)	19.4
SS-208	6 - 8 (ft)	11/3/2014	N	-	-	-	ND (0.569)	ND (0.569)	ND (0.569)	ND (0.569)	ND (0.569)	0.891	ND (0.569)	26.2	ND (0.569)	27.091
SS-208	8 - 10 (ft)	11/3/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	1.74	ND (0.115)	1.74
SS-209	10 - 12 (ft)	11/3/2014	N	-	-	-	ND (3.25)	ND (3.25)	ND (3.25)	ND (3.25)	ND (3.25)	ND (3.25)	ND (3.25)	83.8	ND (3.25)	83.8
SS-209	12 - 14 (ft)	11/3/2014	N	-	-	-	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	0.317	ND (0.0639)	0.317
SS-209	4 - 6 (ft)	11/3/2014	N	-	-	-	ND (52.5)	ND (52.5)	ND (52.5)	ND (52.5)	ND (52.5)	ND (52.5)	ND (52.5)	1030	ND (52.5)	1030
SS-209	6 - 8 (ft)	11/3/2014	N	-	-	-	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	ND (0.0554)	0.138	ND (0.0554)	0.138
SS-209	8 - 10 (ft)	11/3/2014	N	-	-	-	ND (23.1)	ND (23.1)	ND (23.1)	ND (23.1)	ND (23.1)	ND (23.1)	ND (23.1)	172	ND (23.1)	172
SS-210	10 - 12 (ft)	10/31/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	1.39	ND (0.114)	1.39
SS-210	4 - 6 (ft)	10/31/2014	N	-	-	-	ND (0.372)	ND (0.372)	ND (0.372)	ND (0.372)	ND (0.372)	ND (0.372)	ND (0.372)	12	ND (0.372)	12
SS-210	6 - 8 (ft)	10/31/2014	N	-	-	-	ND (5.61)	ND (5.61)	ND (5.61)	ND (5.61)	ND (5.61)	8.67	ND (5.61)	202	ND (5.61)	210.67
SS-210	8 - 10 (ft)	10/31/2014	N	-	-	-	ND (0.241)	ND (0.241)	ND (0.241)	ND (0.241)	ND (0.241)	ND (0.241)	ND (0.241)	3.1	ND (0.241)	3.1
SS-211	10 - 12 (ft)	10/31/2014	N	-	-	-	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	1.82	ND (0.299)	1.82
SS-211	4 - 6 (ft)	10/31/2014	N	-	-	-	ND (0.325)	ND (0.325)	ND (0.325)	ND (0.325)	ND (0.325)	ND (0.325)	ND (0.325)	7.03	ND (0.325)	7.03

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
SS-211	6 - 8 (ft)	10/31/2014	N	-	-	-	ND (10.8)	ND (10.8)	ND (10.8)	ND (10.8)	ND (10.8)	ND (10.8)	ND (10.8)	293	ND (10.8)	293
SS-211	8 - 10 (ft)	10/31/2014	N	-	-	-	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	2.85	ND (0.127)	2.85
SS-212	10 - 12 (ft)	10/31/2014	N	-	-	-	ND (5.03)	ND (5.03)	ND (5.03)	ND (5.03)	ND (5.03)	ND (5.03)	ND (5.03)	125	ND (5.03)	125
SS-212	12 - 14 (ft)	10/31/2014	N	-	-	-	ND (0.447)	ND (0.447)	ND (0.447)	ND (0.447)	ND (0.447)	ND (0.447)	ND (0.447)	8.25	ND (0.447)	8.25
SS-212	4 - 6 (ft)	10/31/2014	N	-	-	-	ND (14.3)	ND (14.3)	ND (14.3)	ND (14.3)	58.1	ND (14.3)	ND (14.3)	392	ND (14.3)	450.1
SS-213	10 - 12 (ft)	11/4/2014	N	-	-	-	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	2.06	ND (0.0788)	2.06
SS-213	4 - 6 (ft)	11/4/2014	N	-	-	-	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	2.16	ND (0.544)	8.59	ND (0.544)	10.75
SS-213	6 - 8 (ft)	11/4/2014	N	-	-	-	ND (0.647)	ND (0.647)	ND (0.647)	ND (0.647)	ND (0.647)	4.61	ND (0.647)	20	6.6	31.21
SS-213	8 - 10 (ft)	11/4/2014	N	-	-	-	ND (1.28)	ND (1.28)	ND (1.28)	ND (1.28)	ND (1.28)	ND (1.28)	ND (1.28)	23.4	ND (1.28)	23.4
SS-214	10 - 12 (ft)	11/4/2014	N	-	-	-	ND (2.3)	ND (2.3)	ND (2.3)	ND (2.3)	ND (2.3)	14.1	ND (2.3)	40.9	ND (2.3)	55
SS-214	12 - 14 (ft)	11/4/2014	N	-	-	-	ND (0.0735)	ND (0.0735)	ND (0.0735)	ND (0.0735)	ND (0.0735)	0.203	ND (0.0735)	0.327	ND (0.0735)	0.53
SS-214	4 - 6 (ft)	11/4/2014	N	-	-	-	ND (4.41)	ND (4.41)	ND (4.41)	ND (4.41)	ND (4.41)	28.6	ND (4.41)	111	ND (4.41)	139.6
SS-215	10 - 12 (ft)	11/4/2014	N	-	-	-	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	4.14	ND (0.34)	4.14
SS-215	4 - 6 (ft)	11/4/2014	N	-	-	-	ND (4.42)	ND (4.42)	ND (4.42)	ND (4.42)	ND (4.42)	ND (4.42)	ND (4.42)	119	ND (4.42)	119
SS-215	6 - 8 (ft)	11/4/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.68	ND (0.114)	4.34	ND (0.114)	5.02
SS-216	4 - 6 (ft)	11/4/2014	N	-	-	-	ND (0.574)	ND (0.574)	ND (0.574)	ND (0.574)	ND (0.574)	3.73	ND (0.574)	11.7	ND (0.574)	15.43
SS-216	6 - 8 (ft)	11/4/2014	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	2.4	ND (0.11)	2.4
SS-217	4 - 6 (ft)	11/4/2014	N	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	1.96	ND (0.105)	1.96
SS-217	6 - 8 (ft)	11/4/2014	N	-	-	-	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	1.57	ND (0.108)	1.57
SS-218	10 - 12 (ft)	11/10/2014	N	-	-	-	ND (0.0592)	ND (0.0592)	ND (0.0592)	ND (0.0592)	0.166	ND (0.0592)	ND (0.0592)	0.0976	ND (0.0592)	0.2636
SS-218	4 - 6 (ft)	11/10/2014	N	-	-	-	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	0.355	ND (0.055)	0.355
SS-218	6 - 8 (ft)	11/10/2014	N	-	-	-	ND (0.0569)	ND (0.0569)	ND (0.0569)	ND (0.0569)	ND (0.0569)	0.118	ND (0.0569)	0.688	ND (0.0569)	0.806
SS-219	10 - 12 (ft)	11/7/2014	N	-	-	-	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	0.227	ND (0.0595)	0.227
SS-219	4 - 6 (ft)	11/7/2014	N	-	-	-	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	ND (0.0526)	0.178	ND (0.0526)	0.473	ND (0.0526)	0.651
SS-219	6 - 8 (ft)	11/7/2014	N	-	-	-	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	ND (0.0578)	0.274	ND (0.0578)	0.951	ND (0.0578)	1.225
SS-220	10 - 12 (ft)	11/7/2014	N	-	-	-	ND (0.356)	ND (0.356)	ND (0.356)	ND (0.356)	ND (0.356)	ND (0.356)	ND (0.356)	2.66	ND (0.356)	2.66
SS-220	4 - 6 (ft)	11/7/2014	N	-	-	-	ND (2.61)	ND (2.61)	ND (2.61)	ND (2.61)	ND (2.61)	9.15	ND (2.61)	38.5	ND (2.61)	47.65
SS-220	6 - 8 (ft)	11/7/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	2.12	ND (0.115)	2.12
SS-220	8 - 10 (ft)	11/7/2014	N	-	-	-	ND (1.69)	ND (1.69)	ND (1.69)	ND (1.69)	1.45 J	ND (1.69)	ND (1.69)	28.4	ND (1.69)	29.85
SS-221	10 - 12 (ft)	11/13/2014	N	-	-	-	ND (0.222)	ND (0.222)	ND (0.222)	ND (0.222)	ND (0.222)	2.66	ND (0.222)	1.02	ND (0.222)	3.68
SS-221	4 - 6 (ft)	11/13/2014	N	-	-	-	ND (0.428)	ND (0.428)	ND (0.428)	ND (0.428)	ND (0.428)	6.99	ND (0.428)	3.88	ND (0.428)	10.87
SS-221	6 - 8 (ft)	11/13/2014	N	-	-	-	ND (0.659)	ND (0.659)	ND (0.659)	ND (0.659)	ND (0.659)	7.07	ND (0.659)	2.66	ND (0.659)	9.73
SS-221	8 - 10 (ft)	11/13/2014	N	-	-	-	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)
SS-222	10 - 12 (ft)	11/13/2014	N	-	-	-	ND (0.18)	ND (0.18)	ND (0.18)	ND (0.18)	ND (0.18)	0.327	ND (0.18)	1.95	ND (0.18)	2.277
SS-222	4 - 6 (ft)	11/13/2014	N	-	-	-	ND (1.99)	ND (1.99)	ND (1.99)	ND (1.99)	17.8	59.1	ND (1.99)	25.4	ND (1.99)	102.3
SS-222	6 - 8 (ft)	11/13/2014	N	-	-	-	ND (0.197)	ND (0.197)	ND (0.197)	ND (0.197)	ND (0.197)	0.445	ND (0.197)	2.78	ND (0.197)	3.225
SS-222	8 - 10 (ft)	11/13/2014	N	-	-	-	ND (0.579)	ND (0.579)	ND (0.579)	ND (0.579)	ND (0.579)	ND (0.579)	ND (0.579)	9.11	ND (0.579)	9.11
SS-223	4 - 6 (ft)	11/13/2014	N	-	-	-	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	16.4	ND (1.71)	36.1	ND (1.71)	52.5
SS-223	6 - 8 (ft)	11/13/2014	N	-	-	-	ND (0.0648)	ND (0.0648)	ND (0.0648)	ND (0.0648)	ND (0.0648)	0.556	ND (0.0648)	0.995	ND (0.0648)	1.551
SS-223	8 - 10 (ft)	11/13/2014	N	-	-	-	ND (0.184)	ND (0.184)	ND (0.184)	ND (0.184)	ND (0.184)	ND (0.184)	ND (0.184)	1.7	ND (0.184)	1.7
SS-224	4 - 6 (ft)	11/12/2014	N	-	-	-	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	1.24	ND (0.113)	1.9	ND (0.113)	3.14

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
SS-225	4 - 6 (ft)	11/17/2014	N	-	-	-	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	ND (0.0575)	0.441	ND (0.0575)	0.441
SS-225	6 - 8 (ft)	11/17/2014	FD	-	-	-	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)	ND (0.0583)
SS-226	4 - 6 (ft)	11/17/2014	N	-	-	-	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)	ND (0.055)
SS-226	6 - 8 (ft)	11/17/2014	N	-	-	-	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	10.1	3.73	13.83
SS-226	8 - 10 (ft)	11/17/2014	N	-	-	-	ND (0.447)	ND (0.447)	ND (0.447)	ND (0.447)	ND (0.447)	ND (0.447)	ND (0.447)	6.26	ND (0.447)	6.26
SS-227	4 - 6 (ft)	11/14/2014	N	-	-	-	ND (0.61)	ND (0.61)	ND (0.61)	ND (0.61)	ND (0.61)	ND (0.61)	ND (0.61)	8.79	ND (0.61)	8.79
SS-227	8 - 10 (ft)	11/14/2014	N	-	-	-	ND (0.0803)	ND (0.0803)	ND (0.0803)	ND (0.0803)	0.326	ND (0.0803)	ND (0.0803)	2.88	ND (0.0803)	3.206
SS-228	10 - 12 (ft)	11/14/2014	N	-	-	-	ND (0.295)	ND (0.295)	ND (0.295)	ND (0.295)	ND (0.295)	3.93	ND (0.295)	1.55	ND (0.295)	5.48
SS-228	6 - 8 (ft)	11/14/2014	N	-	-	-	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	13.7	ND (0.658)	6.01 P	ND (0.658)	19.71
SS-228	8 - 10 (ft)	11/14/2014	N	-	-	-	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	ND (0.544)	8.04	ND (0.544)	ND (0.544)	ND (0.544)	8.04
SS-229	4 - 6 (ft)	11/20/2014	N	-	-	-	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.674	ND (0.132)	0.922 P	ND (0.132)	1.596
SS-229	6 - 8 (ft)	11/20/2014	N	-	-	-	ND (0.382)	ND (0.382)	ND (0.382)	ND (0.382)	ND (0.382)	7.03	ND (0.382)	2.68	ND (0.382)	9.71
SS-229	8 - 10 (ft)	11/20/2014	N	-	-	-	ND (0.161)	ND (0.161)	ND (0.161)	ND (0.161)	ND (0.161)	2.19	ND (0.161)	ND (0.161)	ND (0.161)	2.19
SS-230	10 - 12 (ft)	11/20/2014	N	-	-	-	ND (0.772)	ND (0.772)	ND (0.772)	ND (0.772)	ND (0.772)	5.17	ND (0.772)	3.6	ND (0.772)	8.77
SS-230	4 - 6 (ft)	11/20/2014	N	-	-	-	ND (0.602)	ND (0.602)	ND (0.602)	ND (0.602)	ND (0.602)	10.5	ND (0.602)	17.1	ND (0.602)	27.6
SS-230	6 - 8 (ft)	11/20/2014	N	-	-	-	ND (3.9)	ND (3.9)	ND (3.9)	ND (3.9)	ND (3.9)	133	ND (3.9)	ND (3.9)	ND (3.9)	133
SS-230	8 - 10 (ft)	11/20/2014	N	-	-	-	ND (0.0977)	ND (0.0977)	ND (0.0977)	ND (0.0977)	ND (0.0977)	0.866	ND (0.0977)	0.735	ND (0.0977)	1.601
SS-231	4 - 6 (ft)	11/20/2014	N	-	-	-	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	20.2	ND (1.17)	7.41	ND (1.17)	27.61
SS-231	6 - 8 (ft)	11/20/2014	N	-	-	-	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	ND (0.0581)	0.359	ND (0.0581)	0.359
SS-231	8 - 10 (ft)	11/20/2014	N	-	-	-	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	0.248	ND (0.0799)	0.248
WA-001	6 - 8 (ft)	11/9/2013	N	-	-	-	ND (1.25)	ND (1.25)	ND (1.25)	ND (1.25)	ND (1.25)	5.72	ND (1.25)	26.2	ND (1.25)	31.92
WA-001	8 - 10 (ft)	11/9/2013	N	-	-	-	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	ND (0.658)	13	4.68	17.68
WA-002	2 - 4 (ft)	11/11/2013	N	-	-	-	ND (1.24)	ND (1.24)	ND (1.24)	ND (1.24)	ND (1.24)	5.94 P	ND (1.24)	28.4	ND (1.24)	34.34
WA-002	4 - 6 (ft)	11/11/2013	N	-	-	-	ND (0.173)	ND (0.173)	ND (0.173)	ND (0.173)	ND (0.173)	ND (0.173)	ND (0.173)	1.31	ND (0.173)	1.31
WA-101	8 - 10 (ft)	11/21/2013	N	-	-	-	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	ND (0.0589)	0.119	ND (0.0589)	0.119
WA-102	8 - 10 (ft)	10/29/2013	N	-	-	-	ND (0.0636)	ND (0.0636)	ND (0.0636)	ND (0.0636)	ND (0.0636)	ND (0.0636)	ND (0.0636)	ND (0.0636)	ND (0.0636)	ND (0.0636)
WA-103	8 - 10 (ft)	10/29/2013	N	-	-	-	ND (0.0749)	ND (0.0749)	ND (0.0749)	ND (0.0749)	ND (0.0749)	ND (0.0749)	ND (0.0749)	0.448	0.126	0.574
WA-104	8 - 10 (ft)	10/29/2013	N	-	-	-	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)
WA-105	8 - 10 (ft)	10/29/2013	N	-	-	-	ND (0.379)	ND (0.379)	ND (0.379)	ND (0.379)	ND (0.379)	ND (0.379)	ND (0.379)	1.26	0.566	1.826
WA-106	8 - 10 (ft)	10/29/2013	N	-	-	-	ND (6.64)	ND (6.64)	ND (6.64)	ND (6.64)	ND (6.64)	27.8 P	ND (6.64)	184	83	294.8
WA-106A	8 - 10 (ft)	10/29/2013	FD	-	-	-	ND (7.17)	ND (7.17)	ND (7.17)	ND (7.17)	ND (7.17)	ND (7.17)	ND (7.17)	132	47.7	179.7
WA-106A	8 - 10 (ft)	10/29/2013	N	-	-	-	ND (7.26)	ND (7.26)	ND (7.26)	ND (7.26)	ND (7.26)	ND (7.26)	ND (7.26)	239	83.1	322.1
WA-107	8 - 10 (ft)	10/22/2013	N	-	-	-	ND (4.21)	ND (4.21)	ND (4.21)	ND (4.21)	ND (4.21)	13.4 P	ND (4.21)	95.6	ND (4.21)	109
WA-108	8 - 10 (ft)	10/22/2013	N	-	-	-	ND (0.872)	ND (0.872)	ND (0.872)	ND (0.872)	ND (0.872)	2.54 P	ND (0.872)	16.9	ND (0.872)	19.44
WA-110	8 - 10 (ft)	10/29/2013	N	-	-	-	ND (0.17)	ND (0.17)	ND (0.17)	ND (0.17)	ND (0.17)	ND (0.17)	ND (0.17)	0.695	0.175 P	0.87
WA-112	8 - 10 (ft)	11/11/2013	N	-	-	-	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	0.244	ND (0.086)	0.244
WA-113	0 - 2 (ft)	10/15/2013	N	-	-	-	ND (2.77)	ND (2.77)	ND (2.77)	ND (2.77)	21.8	28.5 P	ND (2.77)	63.5	ND (2.77)	113.8
WA-113	8 - 10 (ft)	10/30/2013	N	-	-	-	ND (0.0671)	ND (0.0671)	ND (0.0671)	ND (0.0671)	ND (0.0671)	0.107	ND (0.0671)	0.166	ND (0.0671)	0.273
WA-114	0 - 2 (ft)	10/15/2013	N	-	-	-	ND (16.2)	ND (16.2)	ND (16.2)	ND (16.2)	96.6	156 P	ND (16.2)	441	ND (16.2)	693.6
WA-114	8 - 10 (ft)	10/30/2013	N	-	-	-	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)
WA-115	0 - 2 (ft)	10/15/2013	N	-	-	-	ND (5.94)	ND (5.94)	ND (5.94)	ND (5.94)	ND (5.94)	ND (5.94)	ND (5.94)	139	ND (5.94)	139

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
WA-115	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)	ND (0.0628)
WA-115	8 - 10 (ft)	10/30/2013	N	-	-	-	ND (0.0727)	ND (0.0727)	ND (0.0727)	ND (0.0727)	ND (0.0727)	ND (0.0727)	ND (0.0727)	0.0865	ND (0.0727)	0.0865
WA-116	0 - 2 (ft)	10/15/2013	N	-	-	-	ND (17.8)	ND (17.8)	ND (17.8)	ND (17.8)	ND (17.8)	ND (17.8)	ND (17.8)	481	ND (17.8)	481
WA-116	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (1.19)	ND (1.19)	ND (1.19)	ND (1.19)	ND (1.19)	5.2	ND (1.19)	23.8	ND (1.19)	29
WA-116	4 - 6 (ft)	6/4/2014	N	-	-	-	ND (0.0644)	ND (0.0644)	ND (0.0644)	ND (0.0644)	ND (0.0644)	ND (0.0644)	ND (0.0644)	0.131	ND (0.0644)	0.131
WA-116	8 - 10 (ft)	10/30/2013	N	-	-	-	ND (0.0699)	ND (0.0699)	ND (0.0699)	ND (0.0699)	ND (0.0699)	ND (0.0699)	ND (0.0699)	0.208	ND (0.0699)	0.208
WA-117	0 - 2 (ft)	10/10/2013	N	-	-	-	ND (11)	ND (11)	ND (11)	ND (11)	ND (11)	42.2 P	ND (11)	213	ND (11)	255.2
WA-117	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (0.243)	ND (0.243)	ND (0.243)	ND (0.243)	ND (0.243)	ND (0.243)	ND (0.243)	3.38	ND (0.243)	3.38
WA-117	4 - 6 (ft)	10/17/2013	N	-	-	-	ND (0.186)	ND (0.186)	ND (0.186)	ND (0.186)	ND (0.186)	0.489 P	ND (0.186)	2.51	ND (0.186)	2.999
WA-117	8 - 10 (ft)	10/30/2013	N	-	-	-	ND (0.0876)	ND (0.0876)	ND (0.0876)	ND (0.0876)	ND (0.0876)	ND (0.0876)	ND (0.0876)	ND (0.0876)	ND (0.0876)	ND (0.0876)
WA-118	0 - 2 (ft)	10/16/2013	FD	-	-	-	ND (57.2)	ND (57.2)	ND (57.2)	ND (57.2)	703	1210	ND (57.2)	2650	ND (57.2)	4563
WA-118	0 - 2 (ft)	10/16/2013	N	-	-	-	ND (55.1)	ND (55.1)	ND (55.1)	ND (55.1)	482	891	ND (55.1)	1860	ND (55.1)	3233
WA-118	2 - 4 (ft)	6/13/2014	N	-	-	-	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.352	ND (0.113)	1.26	ND (0.113)	1.612
WA-118	4 - 6 (ft)	6/13/2014	N	-	-	-	ND (0.0521)	ND (0.0521)	ND (0.0521)	ND (0.0521)	0.0306 J	ND (0.0521)	ND (0.0521)	0.179	ND (0.0521)	0.2096
WA-118	8 - 10 (ft)	10/30/2013	N	-	-	-	ND (0.08)	ND (0.08)	ND (0.08)	ND (0.08)	ND (0.08)	ND (0.08)	ND (0.08)	ND (0.08)	ND (0.08)	ND (0.08)
WA-119	0 - 2 (ft)	10/16/2013	N	-	-	-	ND (332)	ND (332)	ND (332)	ND (332)	ND (332)	ND (332)	ND (332)	10300	ND (332)	10300
WA-119	2 - 4 (ft)	6/12/2014	N	-	-	-	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	ND (0.0544)	0.112	ND (0.0544)	1.37	ND (0.0544)	1.482
WA-119	8 - 10 (ft)	10/30/2013	N	-	-	-	ND (0.0875)	ND (0.0875)	ND (0.0875)	ND (0.0875)	ND (0.0875)	ND (0.0875)	ND (0.0875)	0.148	ND (0.0875)	0.148
WA-120	0 - 2 (ft)	10/16/2013	N	-	-	-	ND (177)	ND (177)	ND (177)	ND (177)	ND (177)	ND (177)	ND (177)	7860	ND (177)	7860
WA-120	2 - 4 (ft)	6/12/2014	N	-	-	-	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	33.6	14.4	48
WA-120	4 - 6 (ft)	6/12/2014	N	-	-	-	ND (0.662)	ND (0.662)	ND (0.662)	ND (0.662)	ND (0.662)	ND (0.662)	ND (0.662)	17.7	ND (0.662)	17.7
WA-120	6 - 8 (ft)	6/12/2014	N	-	-	-	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	3.35	ND (0.192)	3.35
WA-120	8 - 10 (ft)	10/30/2013	N	-	-	-	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)
WA-121	0 - 2 (ft)	10/16/2013	N	-	-	-	ND (32.7)	ND (32.7)	ND (32.7)	ND (32.7)	ND (32.7)	336 P	ND (32.7)	796	ND (32.7)	1132
WA-121	8 - 10 (ft)	10/31/2013	N	-	-	-	ND (3.03)	ND (3.03)	ND (3.03)	ND (3.03)	ND (3.03)	35.6	ND (3.03)	52.7	14.6	102.9
WA-122	0 - 2 (ft)	10/16/2013	N	-	-	-	ND (54.1)	ND (54.1)	ND (54.1)	ND (54.1)	185	639	ND (54.1)	1340	ND (54.1)	2164
WA-122	8 - 10 (ft)	10/31/2013	N	-	-	-	ND (1.69)	ND (1.69)	ND (1.69)	ND (1.69)	ND (1.69)	13.6	ND (1.69)	35.9	11.5	61
WA-123	2 - 4 (ft)	10/10/2013	N	-	-	-	ND (18.1)	ND (18.1)	ND (18.1)	ND (18.1)	ND (18.1)	568	ND (18.1)	384	ND (18.1)	952
WA-123	4 - 6 (ft)	6/13/2014	N	-	-	-	ND (1.92)	ND (1.92)	ND (1.92)	ND (1.92)	ND (1.92)	25.6	ND (1.92)	18.2	ND (1.92)	43.8
WA-123	6 - 8 (ft)	6/13/2014	N	-	-	-	ND (0.0843)	ND (0.0843)	ND (0.0843)	ND (0.0843)	ND (0.0843)	0.472	ND (0.0843)	0.252	ND (0.0843)	0.724
WA-123	8 - 10 (ft)	10/31/2013	N	-	-	-	ND (0.666)	ND (0.666)	ND (0.666)	ND (0.666)	ND (0.666)	1.71	ND (0.666)	1.03	ND (0.666)	2.74
WA-124	2 - 4 (ft)	10/2/2013	N	-	-	-	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	30.4	ND (1.2)	30.4
WA-124	4 - 6 (ft)	6/13/2014	N	-	-	-	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	0.207	ND (0.0586)	0.207
WA-124	8 - 10 (ft)	10/31/2013	FD	-	-	-	ND (0.0897)	ND (0.0897)	ND (0.0897)	ND (0.0897)	ND (0.0897)	ND (0.0897)	ND (0.0897)	ND (0.0897)	ND (0.0897)	ND (0.0897)
WA-124	8 - 10 (ft)	10/31/2013	N	-	-	-	ND (0.204)	ND (0.204)	ND (0.204)	ND (0.204)	ND (0.204)	ND (0.204)	ND (0.204)	0.278	ND (0.204)	0.278
WA-125	2 - 4 (ft)	10/2/2013	N	-	-	-	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	0.327	ND (0.0626)	0.327
WA-125	8 - 10 (ft)	10/31/2013	N	-	-	-	ND (0.0738)	ND (0.0738)	ND (0.0738)	ND (0.0738)	ND (0.0738)	ND (0.0738)	ND (0.0738)	ND (0.0738)	ND (0.0738)	ND (0.0738)
WA-126	2 - 4 (ft)	11/4/2013	N	-	-	-	ND (0.0555)	ND (0.0555)	ND (0.0555)	ND (0.0555)	ND (0.0555)	ND (0.0555)	ND (0.0555)	0.0814	ND (0.0555)	0.0814
WA-126	8 - 10 (ft)	11/4/2013	N	-	-	-	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	0.798	0.26	1.058
WA-127	2 - 4 (ft)	10/2/2013	N	-	-	-	ND (4.81)	ND (4.81)	ND (4.81)	ND (4.81)	ND (4.81)	ND (4.81)	ND (4.81)	137	ND (4.81)	137
WA-127	4 - 6 (ft)	6/13/2014	N	-	-	-	ND (0.0528)	ND (0.0528)	ND (0.0528)	ND (0.0528)	ND (0.0528)	0.0982	ND (0.0528)	0.301	ND (0.0528)	0.3992

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
WA-127	8 - 10 (ft)	11/4/2013	N	-	-	-	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	0.178	ND (0.072)	0.178
WA-128	2 - 4 (ft)	11/6/2013	N	-	-	-	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)
WA-128	6 - 8 (ft)	11/6/2013	N	-	-	-	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)	ND (0.0588)
WA-128	8 - 10 (ft)	11/6/2013	FD	-	-	-	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)
WA-128	8 - 10 (ft)	11/6/2013	N	-	-	-	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)	ND (0.0701)
WA-129	0 - 2 (ft)	11/6/2013	N	-	-	-	ND (564)	ND (564)	ND (564)	ND (564)	2470	4430	ND (564)	2540	ND (564)	9440
WA-129	4 - 6 (ft)	5/22/2014	FD	-	-	-	ND (5.14)	ND (5.14)	ND (5.14)	ND (5.14)	ND (5.14)	96.5	ND (5.14)	50.6	ND (5.14)	147.1
WA-129	4 - 6 (ft)	5/22/2014	N	-	-	-	ND (6.84)	ND (6.84)	ND (6.84)	ND (6.84)	ND (6.84)	196	ND (6.84)	104	ND (6.84)	300
WA-129	6 - 8 (ft)	5/22/2014	N	-	-	-	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	0.0443 J	ND (0.0726)	ND (0.0726)	ND (0.0726)	0.0443 J
WA-129	8 - 10 (ft)	11/6/2013	N	-	-	-	ND (0.0733)	ND (0.0733)	ND (0.0733)	ND (0.0733)	0.482	0.911	ND (0.0733)	0.567	ND (0.0733)	1.96
WA-130	2 - 4 (ft)	10/1/2013	N	-	-	-	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	ND (0.0674)	0.0993	ND (0.0674)	0.0993
WA-130	8 - 10 (ft)	11/4/2013	N	-	-	-	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)	ND (0.0771)
WA-131	2 - 4 (ft)	10/1/2013	N	-	-	-	ND (0.0641)	ND (0.0641)	ND (0.0641)	ND (0.0641)	ND (0.0641)	ND (0.0641)	ND (0.0641)	0.27	ND (0.0641)	0.27
WA-131	8 - 10 (ft)	10/18/2013	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)
WA-132	2 - 4 (ft)	11/17/2014	N	-	-	-	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	2.04	ND (0.124)	2.04
WA-132	4 - 6 (ft)	11/17/2014	N	-	-	-	ND (0.0681)	ND (0.0681)	ND (0.0681)	ND (0.0681)	ND (0.0681)	ND (0.0681)	ND (0.0681)	0.262	ND (0.0681)	0.262
WA-132	8 - 10 (ft)	10/18/2013	N	-	-	-	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)
WA-133	2 - 4 (ft)	11/6/2013	N	-	-	-	ND (0.227)	ND (0.227)	ND (0.227)	ND (0.227)	ND (0.227)	ND (0.227)	ND (0.227)	2.81	ND (0.227)	2.81
WA-133	8 - 10 (ft)	11/6/2013	N	-	-	-	ND (7.14)	ND (7.14)	ND (7.14)	ND (7.14)	ND (7.14)	14.7 P	ND (7.14)	181	ND (7.14)	195.7
WA-134	2 - 4 (ft)	10/1/2013	N	-	-	-	ND (0.0564)	ND (0.0564)	ND (0.0564)	ND (0.0564)	ND (0.0564)	ND (0.0564)	ND (0.0564)	0.204	ND (0.0564)	0.204
WA-134	8 - 10 (ft)	10/18/2013	FD	-	-	-	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)
WA-134	8 - 10 (ft)	10/18/2013	N	-	-	-	ND (0.0787)	ND (0.0787)	ND (0.0787)	ND (0.0787)	ND (0.0787)	ND (0.0787)	ND (0.0787)	ND (0.0787)	ND (0.0787)	ND (0.0787)
WA-135	2 - 4 (ft)	10/1/2013	N	-	-	-	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	ND (0.0547)	0.188	0.806	ND (0.0547)	0.618	1.612
WA-135	8 - 10 (ft)	10/18/2013	N	-	-	-	ND (0.0807)	ND (0.0807)	ND (0.0807)	ND (0.0807)	ND (0.0807)	ND (0.0807)	ND (0.0807)	ND (0.0807)	ND (0.0807)	ND (0.0807)
WA-136	8 - 10 (ft)	10/18/2013	N	-	-	-	ND (0.0913)	ND (0.0913)	ND (0.0913)	ND (0.0913)	ND (0.0913)	ND (0.0913)	ND (0.0913)	ND (0.0913)	ND (0.0913)	ND (0.0913)
WA-137	8 - 10 (ft)	10/18/2013	N	-	-	-	ND (0.205)	ND (0.205)	ND (0.205)	ND (0.205)	ND (0.205)	ND (0.205)	ND (0.205)	7.02	ND (0.205)	7.02
WA-138	8 - 10 (ft)	10/17/2013	N	-	-	-	ND (0.0755)	ND (0.0755)	ND (0.0755)	ND (0.0755)	ND (0.0755)	ND (0.0755)	ND (0.0755)	1.05	ND (0.0755)	1.05
WA-139	8 - 10 (ft)	10/17/2013	N	-	-	-	ND (0.0761)	ND (0.0761)	ND (0.0761)	ND (0.0761)	ND (0.0761)	ND (0.0761)	ND (0.0761)	1.15	ND (0.0761)	1.15
WA-140	8 - 10 (ft)	10/17/2013	N	-	-	-	ND (0.0818)	ND (0.0818)	ND (0.0818)	ND (0.0818)	ND (0.0818)	ND (0.0818)	ND (0.0818)	ND (0.0818)	ND (0.0818)	ND (0.0818)
WA-141	2 - 4 (ft)	11/6/2013	N	-	-	-	ND (16.9)	ND (16.9)	ND (16.9)	ND (16.9)	ND (16.9)	ND (16.9)	ND (16.9)	615	256	871
WA-141	4 - 6 (ft)	5/21/2014	N	-	-	-	ND (0.0643)	ND (0.0643)	ND (0.0643)	ND (0.0643)	ND (0.0643)	ND (0.0643)	ND (0.0643)	0.263	ND (0.0643)	0.263
WA-141	8 - 10 (ft)	11/6/2013	N	-	-	-	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	ND (0.0726)	0.124 P	ND (0.0726)	1.14	ND (0.0726)	1.264
WA-142	4 - 6 (ft)	10/17/2013	N	-	-	-	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	ND (0.0599)	0.169	ND (0.0599)	0.169
WA-142	8 - 10 (ft)	10/17/2013	N	-	-	-	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	0.0973	ND (0.0863)	0.0973
WA-143	4 - 6 (ft)	10/7/2013	N	-	-	-	ND (0.0667)	ND (0.0667)	ND (0.0667)	ND (0.0667)	ND (0.0667)	ND (0.0667)	ND (0.0667)	0.275	ND (0.0667)	0.275
WA-143	8 - 10 (ft)	10/7/2013	N	-	-	-	ND (0.0637)	ND (0.0637)	ND (0.0637)	ND (0.0637)	ND (0.0637)	ND (0.0637)	ND (0.0637)	0.17	ND (0.0637)	0.17
WA-144	4 - 6 (ft)	10/7/2013	N	-	-	-	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	0.104	ND (0.064)	0.104
WA-144	8 - 10 (ft)	10/7/2013	N	-	-	-	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	3	ND (0.128)	3
WA-145	8 - 10 (ft)	11/6/2013	N	-	-	-	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	1.34	ND (0.0925)	1.34
WA-146	2 - 4 (ft)	10/1/2013	N	-	-	-	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	0.187	ND (0.0604)	0.187
WA-146	8 - 10 (ft)	10/1/2013	N	-	-	-	ND (0.0693)	ND (0.0693)	ND (0.0693)	ND (0.0693)	ND (0.0693)	0.99	ND (0.0693)	1.32	ND (0.0693)	2.31

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
WA-147	2 - 4 (ft)	10/1/2013	N	-	-	-	ND (0.0559)	ND (0.0559)	ND (0.0559)	ND (0.0559)	ND (0.0559)	0.155	ND (0.0559)	0.187	ND (0.0559)	0.342
WA-147	8 - 10 (ft)	10/1/2013	FD	-	-	-	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)	ND (0.0799)
WA-147	8 - 10 (ft)	10/1/2013	N	-	-	-	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	0.0414 J	ND (0.0694)	0.0732	ND (0.0694)	0.1146 J
WA-148	2 - 4 (ft)	10/1/2013	N	-	-	-	ND (55.7)	ND (55.7)	ND (55.7)	ND (55.7)	ND (55.7)	ND (55.7)	ND (55.7)	1020	ND (55.7)	1020
WA-148	8 - 10 (ft)	10/1/2013	N	-	-	-	ND (0.73)	ND (0.73)	ND (0.73)	ND (0.73)	ND (0.73)	ND (0.73)	23	ND (0.73)	15.4	38.4
WA-149	6 - 8 (ft)	10/1/2013	FD	-	-	-	ND (1.33)	ND (1.33)	ND (1.33)	ND (1.33)	12	ND (1.33)	37.6	ND (1.33)	47.9	97.5
WA-149	6 - 8 (ft)	10/1/2013	N	-	-	-	ND (7.6)	ND (7.6)	ND (7.6)	ND (7.6)	ND (7.6)	ND (7.6)	107	ND (7.6)	102	209
WA-149	8 - 10 (ft)	10/1/2013	N	-	-	-	ND (1.73)	ND (1.73)	ND (1.73)	ND (1.73)	ND (1.73)	ND (1.73)	ND (1.73)	13.3	ND (1.73)	13.3
WA-152	4 - 6 (ft)	10/3/2013	N	-	-	-	ND (6.16)	ND (6.16)	ND (6.16)	ND (6.16)	ND (6.16)	27.5 P	ND (6.16)	174	ND (6.16)	201.5
WA-152	8 - 10 (ft)	10/3/2013	N	-	-	-	ND (52.6)	ND (52.6)	ND (52.6)	ND (52.6)	264	ND (52.6)	ND (52.6)	1210	ND (52.6)	1474
WA-153	6 - 8 (ft)	10/3/2013	N	-	-	-	ND (1.92)	ND (1.92)	ND (1.92)	ND (1.92)	ND (1.92)	ND (1.92)	ND (1.92)	33.7	12.1	45.8
WA-153	8 - 10 (ft)	10/3/2013	N	-	-	-	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	ND (0.0716)	0.0815	ND (0.0716)	0.0815
WA-154	4 - 6 (ft)	10/3/2013	N	-	-	-	ND (3.72)	ND (3.72)	ND (3.72)	ND (3.72)	ND (3.72)	16.4 P	ND (3.72)	69	ND (3.72)	85.4
WA-154	6 - 8 (ft)	10/3/2013	N	-	-	-	ND (0.778)	ND (0.778)	ND (0.778)	ND (0.778)	ND (0.778)	ND (0.778)	ND (0.778)	15.7	6.09	21.79
WA-154	8 - 10 (ft)	10/3/2013	N	-	-	-	ND (0.522)	ND (0.522)	ND (0.522)	ND (0.522)	2.73	1.17 P	ND (0.522)	5.96	ND (0.522)	9.86
WA-157	2 - 4 (ft)	11/6/2013	N	-	-	-	ND (0.0572)	ND (0.0572)	ND (0.0572)	ND (0.0572)	ND (0.0572)	ND (0.0572)	ND (0.0572)	ND (0.0572)	ND (0.0572)	ND (0.0572)
WA-157	8 - 10 (ft)	11/6/2013	N	-	-	-	ND (0.0814)	ND (0.0814)	ND (0.0814)	ND (0.0814)	ND (0.0814)	ND (0.0814)	ND (0.0814)	0.093	ND (0.0814)	0.093
WA-158	2 - 4 (ft)	11/6/2013	FD	-	-	-	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)	ND (0.0582)
WA-158	8 - 10 (ft)	11/6/2013	N	-	-	-	ND (0.0762)	ND (0.0762)	ND (0.0762)	ND (0.0762)	ND (0.0762)	ND (0.0762)	ND (0.0762)	0.122	ND (0.0762)	0.122
WA-159	8 - 10 (ft)	11/4/2013	N	-	-	-	ND (0.206)	ND (0.206)	ND (0.206)	ND (0.206)	ND (0.206)	ND (0.206)	ND (0.206)	4.02	1.35	5.37
WA-160	4 - 6 (ft)	11/4/2013	FD	-	-	-	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)
WA-160	4 - 6 (ft)	11/4/2013	N	-	-	-	ND (0.0725)	ND (0.0725)	ND (0.0725)	ND (0.0725)	ND (0.0725)	ND (0.0725)	ND (0.0725)	0.115	ND (0.0725)	0.115
WA-160	8 - 10 (ft)	11/4/2013	N	-	-	-	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	0.126	ND (0.0731)	0.126
WA-161	4 - 6 (ft)	11/5/2013	N	-	-	-	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	2.51	0.72	3.23
WA-161	8 - 10 (ft)	11/5/2013	N	-	-	-	ND (0.0849)	ND (0.0849)	ND (0.0849)	ND (0.0849)	ND (0.0849)	ND (0.0849)	ND (0.0849)	0.75	0.227	0.977
WA-162	4 - 6 (ft)	11/5/2013	N	-	-	-	ND (0.211)	ND (0.211)	ND (0.211)	ND (0.211)	ND (0.211)	ND (0.211)	ND (0.211)	4.36	1.38	5.74
WA-162	8 - 10 (ft)	11/5/2013	N	-	-	-	ND (0.377)	ND (0.377)	ND (0.377)	ND (0.377)	ND (0.377)	ND (0.377)	ND (0.377)	6.55	2.13	8.68
WA-163	4 - 6 (ft)	11/5/2013	N	-	-	-	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	ND (0.0632)	0.403	0.403
WA-163	6 - 8 (ft)	11/5/2013	N	-	-	-	ND (0.499)	ND (0.499)	ND (0.499)	ND (0.499)	ND (0.499)	ND (0.499)	ND (0.499)	9.2	ND (0.499)	9.2
WA-163	8 - 10 (ft)	11/5/2013	N	-	-	-	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	2.44	0.681	3.121
WA-201	8 - 10 (ft)	6/3/2014	FD	-	-	-	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)	ND (0.0626)
WA-201	8 - 10 (ft)	6/3/2014	N	-	-	-	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)
WA-202	0 - 2 (ft)	6/4/2014	N	-	-	-	ND (11.5)	ND (11.5)	ND (11.5)	ND (11.5)	171	88.4	ND (11.5)	117	ND (11.5)	376.4
WA-202	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (1.91)	ND (1.91)	ND (1.91)	ND (1.91)	ND (1.91)	43.4	ND (1.91)	14	ND (1.91)	57.4
WA-202	4 - 6 (ft)	6/4/2014	N	-	-	-	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	5.31	ND (0.34)	2.43	ND (0.34)	7.74
WA-202	8 - 10 (ft)	6/4/2014	N	-	-	-	ND (0.225)	ND (0.225)	ND (0.225)	ND (0.225)	ND (0.225)	3.83	ND (0.225)	1.32	ND (0.225)	5.15
WA-203	0 - 2 (ft)	6/4/2014	N	-	-	-	ND (5.76)	ND (5.76)	ND (5.76)	ND (5.76)	ND (5.76)	21.2	ND (5.76)	96.7	ND (5.76)	117.9
WA-203	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (0.0619)	ND (0.0619)	ND (0.0619)	ND (0.0619)	ND (0.0619)	ND (0.0619)	ND (0.0619)	0.0491 J	ND (0.0619)	0.0491 J
WA-204	0 - 2 (ft)	6/4/2014	N	-	-	-	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	31	ND (1.68)	31
WA-204	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)
WA-205	2 - 4 (ft)	5/20/2014	N	-	-	-	ND (0.181)	ND (0.181)	ND (0.181)	ND (0.181)	ND (0.181)	0.235	ND (0.181)	1.95	ND (0.181)	2.185

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AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
WA-206	6 - 8 (ft)	6/13/2014	N	-	-	-	ND (0.0781)	ND (0.0781)	ND (0.0781)	ND (0.0781)	ND (0.0781)	ND (0.0781)	ND (0.0781)	ND (0.0781)	ND (0.0781)	ND (0.0781)
WA-206	8 - 10 (ft)	6/13/2014	FD	-	-	-	ND (0.0769)	ND (0.0769)	ND (0.0769)	ND (0.0769)	ND (0.0769)	0.0854	ND (0.0769)	0.327	ND (0.0769)	0.4124
WA-206	8 - 10 (ft)	6/13/2014	N	-	-	-	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)	0.137	ND (0.0809)	0.675	ND (0.0809)	0.812
WA-207	4 - 6 (ft)	6/12/2014	FD	-	-	-	ND (0.0715)	ND (0.0715)	ND (0.0715)	ND (0.0715)	ND (0.0715)	ND (0.0715)	ND (0.0715)	ND (0.0715)	ND (0.0715)	ND (0.0715)
WA-207	4 - 6 (ft)	6/12/2014	N	-	-	-	ND (0.0676)	ND (0.0676)	ND (0.0676)	ND (0.0676)	ND (0.0676)	ND (0.0676)	ND (0.0676)	ND (0.0676)	ND (0.0676)	ND (0.0676)
WA-207	8 - 10 (ft)	6/12/2014	N	-	-	-	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)	ND (0.0788)
WA-208	2 - 4 (ft)	5/22/2014	N	-	-	-	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)
WA-209	2 - 4 (ft)	5/22/2014	FD	-	-	-	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	0.772	ND (0.0621)	0.772
WA-209	2 - 4 (ft)	5/22/2014	N	-	-	-	ND (0.131)	ND (0.131)	ND (0.131)	ND (0.131)	ND (0.131)	ND (0.131)	ND (0.131)	2.51	ND (0.131)	2.51
WA-209	8 - 10 (ft)	5/22/2014	N	-	-	-	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)
WA-210	2 - 4 (ft)	5/22/2014	N	-	-	-	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)
WA-210	8 - 10 (ft)	5/22/2014	N	-	-	-	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)
WA-211	2 - 4 (ft)	5/21/2014	N	-	-	-	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)	ND (0.0596)
WB-101	0 - 2 (ft)	10/31/2013	N	-	-	-	ND (16.3)	ND (16.3)	ND (16.3)	ND (16.3)	ND (16.3)	96.9 P	ND (16.3)	481	114	691.9
WB-101	2 - 4 (ft)	10/31/2013	N	-	-	-	ND (10.9)	ND (10.9)	ND (10.9)	ND (10.9)	ND (10.9)	38.6 P	ND (10.9)	264	87.4	390
WB-101	4 - 6 (ft)	10/31/2013	N	-	-	-	ND (0.198)	ND (0.198)	ND (0.198)	ND (0.198)	ND (0.198)	ND (0.198)	ND (0.198)	2.91	ND (0.198)	2.91
WB-102	0 - 2 (ft)	10/31/2013	N	-	-	-	ND (59)	ND (59)	ND (59)	ND (59)	ND (59)	451	ND (59)	1230	484	2165
WB-102	2 - 4 (ft)	10/31/2013	N	-	-	-	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	ND (0.0604)	0.32 P	ND (0.0604)	1.53	0.509	2.359
WB-102	4 - 6 (ft)	10/31/2013	N	-	-	-	ND (0.0712)	ND (0.0712)	ND (0.0712)	ND (0.0712)	ND (0.0712)	ND (0.0712)	ND (0.0712)	ND (0.0712)	ND (0.0712)	ND (0.0712)
WB-103	0 - 2 (ft)	10/31/2013	N	-	-	-	ND (16.7)	ND (16.7)	ND (16.7)	ND (16.7)	ND (16.7)	59.5 P	ND (16.7)	332	89.8	481.3
WB-103	2 - 4 (ft)	10/31/2013	N	-	-	-	ND (5.74)	ND (5.74)	ND (5.74)	ND (5.74)	ND (5.74)	66 P	ND (5.74)	236	77	379
WB-103	4 - 6 (ft)	10/31/2013	N	-	-	-	ND (0.0619)	ND (0.0619)	ND (0.0619)	ND (0.0619)	ND (0.0619)	ND (0.0619)	ND (0.0619)	0.293	ND (0.0619)	0.293
WB-104	0 - 2 (ft)	10/31/2013	N	-	-	-	ND (2.32)	ND (2.32)	ND (2.32)	ND (2.32)	ND (2.32)	5.75 P	ND (2.32)	28.4	9.19	43.34
WB-104	2 - 4 (ft)	10/31/2013	N	-	-	-	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)	ND (0.0562)
WB-201	0 - 2 (ft)	6/4/2014	FD	-	-	-	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	ND (1.17)	4.88	ND (1.17)	15.6	ND (1.17)	20.48
WB-201	0 - 2 (ft)	6/4/2014	N	-	-	-	ND (0.554)	ND (0.554)	ND (0.554)	ND (0.554)	ND (0.554)	3.76	ND (0.554)	14.7	ND (0.554)	18.46
WB-201	2 - 4 (ft)	6/4/2014	N	-	-	-	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	ND (0.063)	0.344	ND (0.063)	0.344
WB-201	6 - 8 (ft)	6/4/2014	N	-	-	-	ND (0.0767)	ND (0.0767)	ND (0.0767)	ND (0.0767)	ND (0.0767)	ND (0.0767)	ND (0.0767)	ND (0.0767)	ND (0.0767)	ND (0.0767)
WB-202	0 - 2 (ft)	6/3/2014	N	-	-	-	ND (2.31)	ND (2.31)	ND (2.31)	ND (2.31)	ND (2.31)	ND (2.31)	ND (2.31)	56.5	ND (2.31)	56.5
WB-202	2 - 4 (ft)	6/3/2014	N	-	-	-	ND (0.0579)	ND (0.0579)	ND (0.0579)	ND (0.0579)	ND (0.0579)	ND (0.0579)	ND (0.0579)	1.19	ND (0.0579)	1.19
WB-203	2 - 4 (ft)	6/13/2014	N	-	-	-	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	ND (0.0586)	0.276	ND (0.0586)	0.276
WB-204	4 - 6 (ft)	6/13/2014	N	-	-	-	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)	ND (0.0731)
WB-205	4 - 6 (ft)	6/27/2014	N	-	-	-	ND (13.6)	ND (13.6)	ND (13.6)	ND (13.6)	ND (13.6)	ND (13.6)	ND (13.6)	179	ND (13.6)	179
WB-205	6 - 8 (ft)	6/27/2014	N	-	-	-	ND (0.0677)	ND (0.0677)	ND (0.0677)	ND (0.0677)	ND (0.0677)	0.109	ND (0.0677)	1.01	ND (0.0677)	1.119
WB-206	0 - 2 (ft)	6/3/2014	FD	-	-	-	ND (0.336)	ND (0.336)	ND (0.336)	ND (0.336)	ND (0.336)	0.757	ND (0.336)	5.64	ND (0.336)	6.397
WB-206	0 - 2 (ft)	6/3/2014	N	-	-	-	ND (0.384)	ND (0.384)	ND (0.384)	ND (0.384)	ND (0.384)	0.999	ND (0.384)	6.98	ND (0.384)	7.979
WB-206	6 - 8 (ft)	6/3/2014	N	-	-	-	ND (0.066)	ND (0.066)	ND (0.066)	ND (0.066)	ND (0.066)	ND (0.066)	ND (0.066)	ND (0.066)	ND (0.066)	ND (0.066)
WB-301	0 - 2 (ft)	6/25/2014	N	-	-	-	ND (2.65)	ND (2.65)	ND (2.65)	ND (2.65)	ND (2.65)	ND (2.65)	ND (2.65)	62.2	ND (2.65)	62.2
WB-301	10 - 12 (ft)	11/3/2014	N	-	-	-	ND (31.6)	ND (31.6)	ND (31.6)	ND (31.6)	ND (31.6)	58	ND (31.6)	645	ND (31.6)	703
WB-301	12 - 14 (ft)	11/3/2014	N	-	-	-	ND (0.0706)	ND (0.0706)	ND (0.0706)	ND (0.0706)	ND (0.0706)	ND (0.0706)	ND (0.0706)	1.88	ND (0.0706)	1.88
WB-301	2 - 4 (ft)	6/25/2014	N	-	-	-	ND (224)	ND (224)	ND (224)	ND (224)	ND (224)	ND (224)	ND (224)	8100	ND (224)	8100

TABLE - SOIL ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
WB-301	4 - 6 (ft)	6/25/2014	N	-	-	-	ND (19.1)	ND (19.1)	ND (19.1)	ND (19.1)	ND (19.1)	ND (19.1)	ND (19.1)	413	ND (19.1)	413
WB-301	6 - 8 (ft)	6/25/2014	N	-	-	-	ND (2.35)	ND (2.35)	ND (2.35)	ND (2.35)	ND (2.35)	ND (2.35)	ND (2.35)	53.2	ND (2.35)	53.2
WB-301	8 - 10 (ft)	11/3/2014	N	-	-	-	ND (31)	ND (31)	ND (31)	ND (31)	38.5	ND (31)	ND (31)	849	ND (31)	887.5
WB-302	0 - 2 (ft)	6/26/2014	N	-	-	-	ND (0.3)	ND (0.3)	ND (0.3)	ND (0.3)	ND (0.3)	ND (0.3)	ND (0.3)	4.52	ND (0.3)	4.52
WB-303	10 - 12 (ft)	11/3/2014	N	-	-	-	ND (0.0666)	ND (0.0666)	ND (0.0666)	ND (0.0666)	ND (0.0666)	ND (0.0666)	ND (0.0666)	ND (0.0666)	ND (0.0666)	ND (0.0666)
WB-303	2 - 4 (ft)	10/20/2014	FD	-	-	-	ND (0.0555)	ND (0.0555)	ND (0.0555)	ND (0.0555)	ND (0.0555)	ND (0.0555)	ND (0.0555)	0.423	ND (0.0555)	0.423
WB-303	2 - 4 (ft)	10/20/2014	N	-	-	-	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	ND (0.0557)	0.486	ND (0.0557)	0.486
WB-303	6 - 8 (ft)	11/3/2014	N	-	-	-	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	ND (0.0595)	0.0607	ND (0.0595)	0.0607
WB-303	8 - 10 (ft)	11/3/2014	N	-	-	-	ND (135)	ND (135)	ND (135)	ND (135)	ND (135)	ND (135)	ND (135)	2910	ND (135)	2910
WC-001	2 - 4 (ft)	10/2/2013	N	-	-	-	ND (1.33)	ND (1.33)	ND (1.33)	ND (1.33)	ND (1.33)	ND (1.33)	ND (1.33)	28.9	ND (1.33)	28.9
WC-002	4 - 6 (ft)	10/2/2013	N	-	-	-	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	ND (0.064)	0.701	ND (0.064)	0.701
WC-101	2 - 4 (ft)	11/7/2013	N	-	-	-	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)	ND (0.0585)
WC-102	2 - 4 (ft)	11/7/2013	FD	-	-	-	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)	ND (0.0587)
WC-102	2 - 4 (ft)	11/7/2013	N	-	-	-	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)	ND (0.0624)
WC-102	4 - 6 (ft)	11/7/2013	N	-	-	-	ND (0.0661)	ND (0.0661)	ND (0.0661)	ND (0.0661)	ND (0.0661)	ND (0.0661)	ND (0.0661)	ND (0.0661)	ND (0.0661)	ND (0.0661)
WC-103	2 - 4 (ft)	11/7/2013	N	-	-	-	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	ND (0.0631)	0.122	ND (0.0631)	0.122
WC-103	4 - 6 (ft)	11/7/2013	N	-	-	-	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)
WC-104	2 - 4 (ft)	11/7/2013	N	-	-	-	ND (0.0798)	ND (0.0798)	ND (0.0798)	ND (0.0798)	ND (0.0798)	ND (0.0798)	ND (0.0798)	0.63	ND (0.0798)	0.63
WC-105	2 - 4 (ft)	11/7/2013	N	-	-	-	ND (0.208)	ND (0.208)	ND (0.208)	ND (0.208)	ND (0.208)	ND (0.208)	ND (0.208)	0.238	ND (0.208)	0.238
WC-201	0 - 2 (ft)	5/22/2014	N	-	-	-	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	161	ND (11.2)	161
WC-201	2 - 4 (ft)	5/22/2014	N	-	-	-	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)	ND (0.0608)
WC-201	4 - 6 (ft)	5/22/2014	N	-	-	-	ND (0.709)	ND (0.709)	ND (0.709)	ND (0.709)	ND (0.709)	ND (0.709)	ND (0.709)	12.7	ND (0.709)	12.7
WC-201	6 - 8 (ft)	5/22/2014	N	-	-	-	ND (0.0757)	ND (0.0757)	ND (0.0757)	ND (0.0757)	ND (0.0757)	ND (0.0757)	ND (0.0757)	ND (0.0757)	ND (0.0757)	ND (0.0757)
WC-202	0 - 2 (ft)	10/27/2014	FD	-	-	-	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	ND (11.2)	327	ND (11.2)	327
WC-202	0 - 2 (ft)	10/27/2014	N	-	-	-	ND (11.3)	ND (11.3)	ND (11.3)	ND (11.3)	ND (11.3)	ND (11.3)	ND (11.3)	409	ND (11.3)	409
WD-001	0 - 2 (ft)	10/1/2013	N	-	-	-	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	ND (0.0546)	0.144	ND (0.0546)	0.669	ND (0.0546)	0.813
WD-001	2 - 4 (ft)	10/1/2013	N	-	-	-	ND (27.8)	ND (27.8)	ND (27.8)	ND (27.8)	ND (27.8)	71.4	ND (27.8)	614	ND (27.8)	685.4
WD-001	4 - 6 (ft)	10/1/2013	N	-	-	-	ND (196)	ND (196)	ND (196)	ND (196)	ND (196)	3350	ND (196)	3860	ND (196)	7210
WD-001	6 - 8 (ft)	10/1/2013	N	-	-	-	ND (65.4)	ND (65.4)	ND (65.4)	ND (65.4)	ND (65.4)	586	ND (65.4)	1570	ND (65.4)	2156
WD-001	8 - 10 (ft)	10/1/2013	N	-	-	-	ND (7.92)	ND (7.92)	ND (7.92)	ND (7.92)	47.2	40.8	ND (7.92)	118	ND (7.92)	206
WE-001	6 - 8 (ft)	10/10/2013	N	-	-	-	ND (0.642)	ND (0.642)	ND (0.642)	ND (0.642)	ND (0.642)	1.47	ND (0.642)	9.4	ND (0.642)	10.87
WE-001	8 - 10 (ft)	10/10/2013	N	-	-	-	ND (0.709)	ND (0.709)	ND (0.709)	ND (0.709)	ND (0.709)	2.48	ND (0.709)	9.64	ND (0.709)	12.12

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-101	0 - 0.5 (ft)	8/20/2014	N	-	-	-	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.2	ND (0.117)	ND (0.117)	0.26	ND (0.117)	0.46
VC-101	0.5 - 1 (ft)	8/20/2014	N	-	-	-	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	0.187	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	0.187
VC-101	1 - 2 (ft)	8/20/2014	FD	-	-	-	ND (0.0927)	ND (0.0927)	ND (0.0927)	ND (0.0927)	0.338	ND (0.0927)	ND (0.0927)	ND (0.0927)	ND (0.0927)	0.338
VC-101	1 - 2 (ft)	8/20/2014	N	-	-	-	ND (0.0939)	ND (0.0939)	ND (0.0939)	ND (0.0939)	0.272	ND (0.0939)	ND (0.0939)	0.0864 J	ND (0.0939)	0.3584
VC-101	2 - 3 (ft)	8/20/2014	N	-	-	-	ND (0.0914)	ND (0.0914)	ND (0.0914)	ND (0.0914)	0.51	ND (0.0914)	ND (0.0914)	0.0796 J	ND (0.0914)	0.5896
VC-101	3 - 4 (ft)	8/20/2014	N	-	-	-	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	1.19	ND (0.0943)	ND (0.0943)	0.551	ND (0.0943)	1.741
VC-101A	0.5 - 1 (ft)	8/28/2014	FD	-	-	-	ND (0.0996)	ND (0.0996)	ND (0.0996)	ND (0.0996)	0.318	ND (0.0996)	ND (0.0996)	ND (0.0996)	ND (0.0996)	0.318
VC-101A	0.5 - 1 (ft)	8/28/2014	N	-	-	-	ND (0.0971)	ND (0.0971)	ND (0.0971)	ND (0.0971)	0.306	ND (0.0971)	ND (0.0971)	ND (0.0971)	ND (0.0971)	0.306
VC-101A	1 - 2 (ft)	8/28/2014	N	-	-	-	ND (0.0969)	ND (0.0969)	ND (0.0969)	ND (0.0969)	0.468	ND (0.0969)	ND (0.0969)	0.0633 J	ND (0.0969)	0.5313
VC-101A	2 - 3 (ft)	8/28/2014	N	-	-	-	ND (0.0961)	ND (0.0961)	ND (0.0961)	ND (0.0961)	0.632	ND (0.0961)	ND (0.0961)	0.145	ND (0.0961)	0.777
VC-101A	3 - 4 (ft)	8/28/2014	N	-	-	-	ND (0.0895)	ND (0.0895)	ND (0.0895)	ND (0.0895)	2.07	ND (0.0895)	ND (0.0895)	1.65	ND (0.0895)	3.72
VC-101A	4 - 6 (ft)	8/28/2014	N	-	-	-	ND (0.079)	ND (0.079)	ND (0.079)	ND (0.079)	0.559	ND (0.079)	ND (0.079)	0.156	ND (0.079)	0.715
VC-101B	0.5 - 1 (ft)	8/28/2014	N	-	-	-	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	0.311	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	0.311
VC-101B	1 - 2 (ft)	8/28/2014	N	-	-	-	ND (0.0996)	ND (0.0996)	ND (0.0996)	ND (0.0996)	0.447	ND (0.0996)	ND (0.0996)	0.119	ND (0.0996)	0.566
VC-101B	2 - 3 (ft)	8/28/2014	N	-	-	-	ND (0.0926)	ND (0.0926)	ND (0.0926)	ND (0.0926)	0.6	ND (0.0926)	ND (0.0926)	0.119	ND (0.0926)	0.719
VC-101B	3 - 4 (ft)	8/28/2014	N	-	-	-	ND (2.95)	ND (2.95)	ND (2.95)	ND (2.95)	23.2	ND (2.95)	ND (2.95)	46.3	ND (2.95)	69.5
VC-101B	4 - 6 (ft)	8/28/2014	N	-	-	-	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)
VC-101C	0.5 - 1 (ft)	8/28/2014	N	-	-	-	ND (0.0908)	ND (0.0908)	ND (0.0908)	ND (0.0908)	0.265	ND (0.0908)	ND (0.0908)	ND (0.0908)	ND (0.0908)	0.265
VC-101C	1 - 2 (ft)	8/28/2014	N	-	-	-	ND (0.0992)	ND (0.0992)	ND (0.0992)	ND (0.0992)	0.318	ND (0.0992)	ND (0.0992)	0.103	ND (0.0992)	0.421
VC-101C	2 - 3 (ft)	8/28/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.566	ND (0.101)	ND (0.101)	0.0693 J	ND (0.101)	0.6353
VC-101C	3 - 4 (ft)	8/28/2014	N	-	-	-	ND (0.282)	ND (0.282)	ND (0.282)	ND (0.282)	2.13	ND (0.282)	ND (0.282)	2.38	ND (0.282)	4.51
VC-101C	4 - 6 (ft)	8/28/2014	N	-	-	-	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	0.0516 J	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	0.0516 J
VC-102	0 - 0.5 (ft)	8/20/2014	N	-	-	-	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.224	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.224
VC-102	0.5 - 1 (ft)	8/20/2014	N	-	-	-	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	0.22	ND (0.0963)	ND (0.0963)	0.0756 J	ND (0.0963)	0.2956
VC-102	1 - 2 (ft)	8/20/2014	N	-	-	-	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	0.348	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	0.348
VC-102	2 - 3 (ft)	8/20/2014	N	-	-	-	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	2.07	ND (0.194)	ND (0.194)	0.407	ND (0.194)	2.477
VC-102	3 - 4 (ft)	8/20/2014	N	-	-	-	ND (1.66)	ND (1.66)	ND (1.66)	ND (1.66)	ND (1.66)	ND (1.66)	ND (1.66)	23.5	ND (1.66)	23.5
VC-102A	0.5 - 1 (ft)	8/28/2014	FD	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.2	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.2
VC-102A	0.5 - 1 (ft)	8/28/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.231	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.231
VC-102A	1 - 2 (ft)	8/28/2014	N	-	-	-	ND (0.0955)	ND (0.0955)	ND (0.0955)	ND (0.0955)	0.338	ND (0.0955)	ND (0.0955)	ND (0.0955)	ND (0.0955)	0.338
VC-102A	2 - 3 (ft)	8/28/2014	N	-	-	-	ND (0.0991)	ND (0.0991)	ND (0.0991)	ND (0.0991)	0.947	ND (0.0991)	ND (0.0991)	0.11	ND (0.0991)	1.057
VC-102A	3 - 4 (ft)	8/28/2014	N	-	-	-	ND (5.1)	ND (5.1)	ND (5.1)	ND (5.1)	ND (5.1)	ND (5.1)	ND (5.1)	90.7	ND (5.1)	90.7
VC-102A	4 - 6 (ft)	8/28/2014	N	-	-	-	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)
VC-102B	0.5 - 1 (ft)	8/28/2014	N	-	-	-	ND (0.0989)	ND (0.0989)	ND (0.0989)	ND (0.0989)	0.273	ND (0.0989)	ND (0.0989)	0.101	ND (0.0989)	0.374
VC-102B	1 - 2 (ft)	8/28/2014	N	-	-	-	ND (0.0978)	ND (0.0978)	ND (0.0978)	ND (0.0978)	0.564	ND (0.0978)	ND (0.0978)	0.305	ND (0.0978)	0.869
VC-102B	2 - 3 (ft)	8/28/2014	N	-	-	-	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	2.03	ND (0.1)	ND (0.1)	3.09	ND (0.1)	5.12
VC-102B	3 - 4 (ft)	8/28/2014	N	-	-	-	ND (0.436)	ND (0.436)	ND (0.436)	ND (0.436)	3.48	ND (0.436)	ND (0.436)	5.62	ND (0.436)	9.1
VC-102B	4 - 6 (ft)	8/28/2014	N	-	-	-	ND (0.0815)	ND (0.0815)	ND (0.0815)	ND (0.0815)	ND (0.0815)	ND (0.0815)	ND (0.0815)	ND (0.0815)	ND (0.0815)	ND (0.0815)
VC-102C	0.5 - 1 (ft)	8/28/2014	N	-	-	-	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.312	ND (0.1)	ND (0.1)	0.0418 J	ND (0.1)	0.3538
VC-102C	1 - 2 (ft)	8/28/2014	FD	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.712	ND (0.104)	ND (0.104)	1.55	ND (0.104)	2.262
VC-102C	1 - 2 (ft)	8/28/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.64	ND (0.111)	ND (0.111)	0.0617 J	ND (0.111)	0.7017

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-102C	2 - 3 (ft)	8/28/2014	N	-	-	-	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	0.106	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	0.106
VC-102C	3 - 4 (ft)	8/28/2014	N	-	-	-	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)
VC-102C	4 - 6 (ft)	8/28/2014	N	-	-	-	ND (0.0886)	ND (0.0886)	ND (0.0886)	ND (0.0886)	ND (0.0886)	ND (0.0886)	ND (0.0886)	ND (0.0886)	ND (0.0886)	ND (0.0886)
VC-103	0 - 0.5 (ft)	8/20/2014	FD	-	-	-	ND (0.137)	ND (0.137)	ND (0.137)	ND (0.137)	0.234	ND (0.137)	ND (0.137)	ND (0.137)	ND (0.137)	0.234
VC-103	0 - 0.5 (ft)	8/20/2014	N	-	-	-	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	0.264	ND (0.129)	ND (0.129)	0.486	ND (0.129)	0.75
VC-103	0.5 - 1 (ft)	8/20/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.356	ND (0.112)	ND (0.112)	0.441	ND (0.112)	0.797
VC-103	1 - 2 (ft)	8/20/2014	N	-	-	-	ND (0.0982)	ND (0.0982)	ND (0.0982)	ND (0.0982)	0.312	ND (0.0982)	ND (0.0982)	1.41	ND (0.0982)	1.722
VC-103	2 - 3 (ft)	8/20/2014	N	-	-	-	ND (0.0931)	ND (0.0931)	ND (0.0931)	ND (0.0931)	0.809	ND (0.0931)	ND (0.0931)	0.503	ND (0.0931)	1.312
VC-103	3 - 4 (ft)	8/20/2014	N	-	-	-	ND (3.57)	ND (3.57)	ND (3.57)	ND (3.57)	11.9	ND (3.57)	ND (3.57)	58.7	ND (3.57)	70.6
VC-103	4 - 6 (ft)	8/20/2014	N	-	-	-	ND (0.584)	ND (0.584)	ND (0.584)	ND (0.584)	2.1	ND (0.584)	ND (0.584)	7.8	ND (0.584)	9.9
VC-103A	0.5 - 1 (ft)	8/20/2014	N	-	-	-	ND (0.0938)	ND (0.0938)	ND (0.0938)	ND (0.0938)	0.312	ND (0.0938)	ND (0.0938)	0.0945	ND (0.0938)	0.4065
VC-103A	1 - 2 (ft)	8/20/2014	N	-	-	-	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	0.475	ND (0.0941)	ND (0.0941)	0.774	ND (0.0941)	1.249
VC-103A	2 - 3 (ft)	8/20/2014	N	-	-	-	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	16.8	ND (1.75)	16.8
VC-103A	3 - 4 (ft)	8/20/2014	N	-	-	-	ND (0.423)	ND (0.423)	ND (0.423)	ND (0.423)	4.09	ND (0.423)	ND (0.423)	6.2	ND (0.423)	10.29
VC-103A	4 - 6 (ft)	8/20/2014	N	-	-	-	ND (0.89)	ND (0.89)	ND (0.89)	ND (0.89)	5.97	ND (0.89)	ND (0.89)	14.9	ND (0.89)	20.87
VC-103B	0.5 - 1 (ft)	8/20/2014	N	-	-	-	ND (0.0887)	ND (0.0887)	ND (0.0887)	ND (0.0887)	0.308	ND (0.0887)	ND (0.0887)	0.338	ND (0.0887)	0.646
VC-103B	1 - 2 (ft)	8/20/2014	N	-	-	-	ND (0.0861)	ND (0.0861)	ND (0.0861)	ND (0.0861)	0.411	ND (0.0861)	ND (0.0861)	0.139	ND (0.0861)	0.55
VC-103B	2 - 3 (ft)	8/20/2014	N	-	-	-	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	1.12	ND (0.0904)	ND (0.0904)	1.38	ND (0.0904)	2.5
VC-103B	3 - 4 (ft)	8/20/2014	N	-	-	-	ND (5.52)	ND (5.52)	ND (5.52)	ND (5.52)	ND (5.52)	ND (5.52)	ND (5.52)	69.8	ND (5.52)	69.8
VC-103B	4 - 6 (ft)	8/20/2014	N	-	-	-	ND (5.14)	ND (5.14)	ND (5.14)	ND (5.14)	ND (5.14)	ND (5.14)	ND (5.14)	95.2	ND (5.14)	95.2
VC-103C	0.5 - 1 (ft)	8/21/2014	N	-	-	-	ND (0.0989)	ND (0.0989)	ND (0.0989)	ND (0.0989)	0.305	ND (0.0989)	ND (0.0989)	0.0849 J	ND (0.0989)	0.3899
VC-103C	1 - 2 (ft)	8/21/2014	N	-	-	-	ND (0.0906)	ND (0.0906)	ND (0.0906)	ND (0.0906)	0.393	ND (0.0906)	ND (0.0906)	0.186	ND (0.0906)	0.579
VC-103C	2 - 3 (ft)	8/21/2014	N	-	-	-	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	1.85	ND (0.0904)	ND (0.0904)	0.894	ND (0.0904)	2.744
VC-103C	3 - 4 (ft)	8/21/2014	N	-	-	-	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)	0.0825	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)	0.0825
VC-103C	4 - 6 (ft)	8/21/2014	N	-	-	-	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)
VC-104	0 - 0.5 (ft)	8/27/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.149	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.149
VC-104	0.5 - 1 (ft)	8/27/2014	FD	-	-	-	ND (0.351)	ND (0.351)	ND (0.351)	ND (0.351)	ND (0.351)	ND (0.351)	ND (0.351)	2.86	ND (0.351)	2.86
VC-104	0.5 - 1 (ft)	8/27/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.141	ND (0.116)	ND (0.116)	0.318	ND (0.116)	0.459
VC-104	1 - 2 (ft)	8/27/2014	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.233	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.233
VC-104	2 - 3 (ft)	8/27/2014	N	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.822	ND (0.102)	ND (0.102)	0.0801 J	ND (0.102)	0.9021
VC-104	3 - 4 (ft)	8/27/2014	N	-	-	-	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	0.171	ND (0.086)	ND (0.086)	1.04	ND (0.086)	1.211
VC-105	0 - 0.5 (ft)	8/26/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.19	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.19
VC-105	0.5 - 1 (ft)	8/26/2014	FD	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.156	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.156
VC-105	0.5 - 1 (ft)	8/26/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.168	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.168
VC-105	1 - 2 (ft)	8/26/2014	N	-	-	-	ND (0.0987)	ND (0.0987)	ND (0.0987)	ND (0.0987)	0.154	ND (0.0987)	ND (0.0987)	ND (0.0987)	ND (0.0987)	0.154
VC-105	2 - 3 (ft)	8/26/2014	N	-	-	-	ND (0.0985)	ND (0.0985)	ND (0.0985)	ND (0.0985)	0.846	ND (0.0985)	ND (0.0985)	0.284	ND (0.0985)	1.13
VC-105	3 - 4 (ft)	8/26/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	1.39	ND (0.101)	ND (0.101)	0.827	ND (0.101)	2.217
VC-106	0 - 0.5 (ft)	8/27/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.153	ND (0.119)	ND (0.119)	0.338	ND (0.119)	0.491
VC-106	0.5 - 1 (ft)	8/27/2014	N	-	-	-	ND (0.0966)	ND (0.0966)	ND (0.0966)	ND (0.0966)	0.292	ND (0.0966)	ND (0.0966)	0.139	ND (0.0966)	0.431
VC-106	1 - 2 (ft)	8/27/2014	N	-	-	-	ND (0.0967)	ND (0.0967)	ND (0.0967)	ND (0.0967)	0.372	ND (0.0967)	ND (0.0967)	0.0795 J	ND (0.0967)	0.452
VC-106	2 - 3 (ft)	8/27/2014	N	-	-	-	ND (0.0932)	ND (0.0932)	ND (0.0932)	ND (0.0932)	1.22	ND (0.0932)	ND (0.0932)	1.38	ND (0.0932)	2.6

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-106	3 - 4 (ft)	8/27/2014	FD	-	-	-	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	0.441	ND (0.086)	ND (0.086)	0.092	ND (0.086)	0.533
VC-106	3 - 4 (ft)	8/27/2014	N	-	-	-	ND (0.443)	ND (0.443)	ND (0.443)	ND (0.443)	1.43	ND (0.443)	ND (0.443)	4.87	ND (0.443)	6.3
VC-107	0 - 0.5 (ft)	8/27/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.146	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.146
VC-107	0.5 - 1 (ft)	8/27/2014	N	-	-	-	ND (0.281)	ND (0.281)	ND (0.281)	ND (0.281)	0.434	ND (0.281)	ND (0.281)	3.62	ND (0.281)	4.054
VC-107	1 - 2 (ft)	8/27/2014	FD	-	-	-	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.443	ND (0.103)	ND (0.103)	0.076 J	ND (0.103)	0.519
VC-107	1 - 2 (ft)	8/27/2014	N	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.424	ND (0.102)	ND (0.102)	0.586	ND (0.102)	1.01
VC-107	2 - 3 (ft)	8/27/2014	N	-	-	-	ND (0.0979)	ND (0.0979)	ND (0.0979)	ND (0.0979)	0.807	ND (0.0979)	ND (0.0979)	0.172	ND (0.0979)	0.979
VC-107	3 - 4 (ft)	8/27/2014	N	-	-	-	ND (0.958)	ND (0.958)	ND (0.958)	ND (0.958)	4.78	ND (0.958)	ND (0.958)	13.7	ND (0.958)	18.48
VC-108	0 - 0.5 (ft)	8/27/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.153	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.153
VC-108	0.5 - 1 (ft)	8/27/2014	N	-	-	-	ND (0.0972)	ND (0.0972)	ND (0.0972)	ND (0.0972)	0.193	ND (0.0972)	ND (0.0972)	ND (0.0972)	ND (0.0972)	0.193
VC-108	1 - 2 (ft)	8/27/2014	FD	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.407	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.407
VC-108	1 - 2 (ft)	8/27/2014	N	-	-	-	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.396	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.396
VC-108	2 - 3 (ft)	8/27/2014	N	-	-	-	ND (35)	ND (35)	ND (35)	ND (35)	ND (35)	ND (35)	ND (35)	492	ND (35)	492
VC-108	3 - 4 (ft)	8/27/2014	N	-	-	-	ND (0.45)	ND (0.45)	ND (0.45)	ND (0.45)	ND (0.45)	ND (0.45)	ND (0.45)	10.8	ND (0.45)	10.8
VC-109	0 - 0.5 (ft)	8/25/2014	N	-	-	-	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	0.457	ND (0.0816)	ND (0.0816)	1.31	ND (0.0816)	1.767
VC-109	0.5 - 1 (ft)	8/25/2014	FD	-	-	-	ND (0.0928)	ND (0.0928)	ND (0.0928)	ND (0.0928)	0.291	ND (0.0928)	ND (0.0928)	0.344	ND (0.0928)	0.635
VC-109	0.5 - 1 (ft)	8/25/2014	N	-	-	-	ND (0.0903)	ND (0.0903)	ND (0.0903)	ND (0.0903)	0.259	ND (0.0903)	ND (0.0903)	ND (0.0903)	ND (0.0903)	0.259
VC-109	1 - 2 (ft)	8/25/2014	N	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.314	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.314
VC-109	2 - 3 (ft)	8/25/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.593	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.593
VC-109	3 - 4 (ft)	8/25/2014	N	-	-	-	ND (0.0875)	ND (0.0875)	ND (0.0875)	ND (0.0875)	1.47	ND (0.0875)	ND (0.0875)	2.07	ND (0.0875)	3.54
VC-110	0 - 0.5 (ft)	8/25/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.21	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.21
VC-110	0.5 - 1 (ft)	8/25/2014	N	-	-	-	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	0.267	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	0.267
VC-110	1 - 2 (ft)	8/25/2014	N	-	-	-	ND (0.0937)	ND (0.0937)	ND (0.0937)	ND (0.0937)	0.358	ND (0.0937)	ND (0.0937)	ND (0.0937)	ND (0.0937)	0.358
VC-110	2 - 3 (ft)	8/25/2014	N	-	-	-	ND (0.099)	ND (0.099)	ND (0.099)	ND (0.099)	0.565	ND (0.099)	ND (0.099)	ND (0.099)	ND (0.099)	0.565
VC-110	3 - 4 (ft)	8/25/2014	N	-	-	-	ND (6.16)	ND (6.16)	ND (6.16)	ND (6.16)	ND (6.16)	ND (6.16)	ND (6.16)	108	ND (6.16)	108
VC-110	4 - 6 (ft)	8/25/2014	N	-	-	-	ND (0.597)	ND (0.597)	ND (0.597)	ND (0.597)	ND (0.597)	ND (0.597)	ND (0.597)	8.96	ND (0.597)	8.96
VC-111	0 - 0.5 (ft)	8/25/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.2	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.2
VC-111	0.5 - 1 (ft)	8/25/2014	N	-	-	-	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	0.296	ND (0.0904)	ND (0.0904)	0.0927	ND (0.0904)	0.3887
VC-111	1 - 2 (ft)	8/25/2014	N	-	-	-	ND (0.458)	ND (0.458)	ND (0.458)	ND (0.458)	0.485	ND (0.458)	ND (0.458)	5.24	ND (0.458)	5.725
VC-111	2 - 3 (ft)	8/25/2014	FD	-	-	-	ND (0.0978)	ND (0.0978)	ND (0.0978)	ND (0.0978)	1.13	ND (0.0978)	ND (0.0978)	1.21	ND (0.0978)	2.34
VC-111	2 - 3 (ft)	8/25/2014	N	-	-	-	ND (0.0931)	ND (0.0931)	ND (0.0931)	ND (0.0931)	0.825	ND (0.0931)	ND (0.0931)	0.169	ND (0.0931)	0.994
VC-111	3 - 4 (ft)	8/25/2014	N	-	-	-	ND (2.59)	ND (2.59)	ND (2.59)	ND (2.59)	3.35	ND (2.59)	ND (2.59)	38.6	ND (2.59)	41.95
VC-112	0 - 0.5 (ft)	8/26/2014	FD	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.204	ND (0.114)	ND (0.114)	1.24	ND (0.114)	1.444
VC-112	0 - 0.5 (ft)	8/26/2014	N	-	-	-	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.352	ND (0.117)	ND (0.117)	0.804	ND (0.117)	1.156
VC-112	0.5 - 1 (ft)	8/26/2014	N	-	-	-	ND (0.0917)	ND (0.0917)	ND (0.0917)	ND (0.0917)	0.46	ND (0.0917)	ND (0.0917)	0.135	ND (0.0917)	0.595
VC-112	1 - 2 (ft)	8/26/2014	N	-	-	-	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	0.689	ND (0.0904)	ND (0.0904)	0.632	ND (0.0904)	1.321
VC-112	2 - 3 (ft)	8/26/2014	N	-	-	-	ND (1.88)	ND (1.88)	ND (1.88)	ND (1.88)	3.21	ND (1.88)	ND (1.88)	43.8	ND (1.88)	47.01
VC-112	3 - 4 (ft)	8/26/2014	N	-	-	-	ND (0.0981)	ND (0.0981)	ND (0.0981)	ND (0.0981)	0.0674 J	ND (0.0981)	ND (0.0981)	0.536	ND (0.0981)	0.6034
VC-113	0 - 0.5 (ft)	8/26/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.168	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.168
VC-113	0.5 - 1 (ft)	8/26/2014	N	-	-	-	ND (0.0932)	ND (0.0932)	ND (0.0932)	ND (0.0932)	0.334	ND (0.0932)	ND (0.0932)	0.294	ND (0.0932)	0.628
VC-113	1 - 2 (ft)	8/26/2014	N	-	-	-	ND (0.0892)	ND (0.0892)	ND (0.0892)	ND (0.0892)	0.506	ND (0.0892)	ND (0.0892)	0.101	ND (0.0892)	0.607

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-113	2 - 3 (ft)	8/26/2014	N	-	-	-	ND (0.273)	ND (0.273)	ND (0.273)	ND (0.273)	3.12	ND (0.273)	ND (0.273)	3.31	ND (0.273)	6.43
VC-113	3 - 4 (ft)	8/26/2014	N	-	-	-	ND (0.099)	ND (0.099)	ND (0.099)	ND (0.099)	0.44	ND (0.099)	ND (0.099)	0.235	ND (0.099)	0.675
VC-114	0 - 0.5 (ft)	8/25/2014	N	-	-	-	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.119	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.119
VC-114	0.5 - 1 (ft)	8/25/2014	N	-	-	-	ND (0.0937)	ND (0.0937)	ND (0.0937)	ND (0.0937)	0.261	ND (0.0937)	ND (0.0937)	0.0607 J	ND (0.0937)	0.3217
VC-114	1 - 2 (ft)	8/25/2014	N	-	-	-	ND (0.0907)	ND (0.0907)	ND (0.0907)	ND (0.0907)	0.305	ND (0.0907)	ND (0.0907)	0.11	ND (0.0907)	0.415
VC-114	2 - 3 (ft)	8/25/2014	FD	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.633	ND (0.102)	ND (0.102)	0.0694 J	ND (0.102)	0.7024
VC-114	2 - 3 (ft)	8/25/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.707	ND (0.101)	ND (0.101)	0.093 J	ND (0.101)	0.8
VC-114	3 - 4 (ft)	8/25/2014	N	-	-	-	ND (2.26)	ND (2.26)	ND (2.26)	ND (2.26)	ND (2.26)	ND (2.26)	ND (2.26)	38.3	ND (2.26)	38.3
VC-115	0 - 0.5 (ft)	8/22/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.339	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.339
VC-115	0.5 - 1 (ft)	8/22/2014	FD	-	-	-	ND (0.094)	ND (0.094)	ND (0.094)	ND (0.094)	0.264	ND (0.094)	ND (0.094)	ND (0.094)	ND (0.094)	0.264
VC-115	0.5 - 1 (ft)	8/22/2014	N	-	-	-	ND (0.0951)	ND (0.0951)	ND (0.0951)	ND (0.0951)	0.321	ND (0.0951)	ND (0.0951)	ND (0.0951)	ND (0.0951)	0.321
VC-115	1 - 2 (ft)	8/22/2014	N	-	-	-	ND (0.0968)	ND (0.0968)	ND (0.0968)	ND (0.0968)	0.376	ND (0.0968)	ND (0.0968)	0.102	ND (0.0968)	0.478
VC-115	2 - 3 (ft)	8/22/2014	N	-	-	-	ND (0.174)	ND (0.174)	ND (0.174)	ND (0.174)	0.332	ND (0.174)	ND (0.174)	2.88	ND (0.174)	3.212
VC-115	3 - 4 (ft)	8/22/2014	N	-	-	-	ND (0.093)	ND (0.093)	ND (0.093)	ND (0.093)	ND (0.093)	ND (0.093)	ND (0.093)	ND (0.093)	ND (0.093)	ND (0.093)
VC-116	0 - 0.5 (ft)	8/22/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.26	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.26
VC-116	0.5 - 1 (ft)	8/22/2014	N	-	-	-	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)	0.251	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)	0.251
VC-116	1 - 2 (ft)	8/22/2014	N	-	-	-	ND (0.0826)	ND (0.0826)	ND (0.0826)	ND (0.0826)	0.0562 J	ND (0.0826)	ND (0.0826)	ND (0.0826)	ND (0.0826)	0.0562 J
VC-116	2 - 3 (ft)	8/22/2014	N	-	-	-	ND (0.0955)	ND (0.0955)	ND (0.0955)	ND (0.0955)	ND (0.0955)	ND (0.0955)	ND (0.0955)	0.0577 J	ND (0.0955)	0.0577 J
VC-116	3 - 4 (ft)	8/22/2014	N	-	-	-	ND (0.0948)	ND (0.0948)	ND (0.0948)	ND (0.0948)	ND (0.0948)	ND (0.0948)	ND (0.0948)	ND (0.0948)	ND (0.0948)	ND (0.0948)
VC-117	0 - 0.5 (ft)	8/21/2014	FD	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.155	ND (0.11)	ND (0.11)	0.183	ND (0.11)	0.338
VC-117	0 - 0.5 (ft)	8/21/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.154	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.154
VC-117	0.5 - 1 (ft)	8/21/2014	N	-	-	-	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	0.206	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	0.206
VC-117	1 - 2 (ft)	8/21/2014	N	-	-	-	ND (0.0892)	ND (0.0892)	ND (0.0892)	ND (0.0892)	0.311	ND (0.0892)	ND (0.0892)	1.18	ND (0.0892)	1.491
VC-117	2 - 3 (ft)	8/21/2014	N	-	-	-	ND (0.0974)	ND (0.0974)	ND (0.0974)	ND (0.0974)	1.51	ND (0.0974)	ND (0.0974)	0.149	ND (0.0974)	1.659
VC-117	3 - 4 (ft)	8/21/2014	N	-	-	-	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	1.46	ND (0.228)	ND (0.228)	0.473	ND (0.228)	1.933
VC-118	0 - 0.5 (ft)	8/22/2014	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.284	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.284
VC-118	0.5 - 1 (ft)	8/22/2014	N	-	-	-	ND (0.471)	ND (0.471)	ND (0.471)	ND (0.471)	ND (0.471)	ND (0.471)	ND (0.471)	6.39	ND (0.471)	6.39
VC-118	1 - 2 (ft)	8/22/2014	N	-	-	-	ND (0.949)	ND (0.949)	ND (0.949)	ND (0.949)	ND (0.949)	ND (0.949)	ND (0.949)	19.5	ND (0.949)	19.5
VC-118	2 - 3 (ft)	8/22/2014	FD	-	-	-	ND (0.473)	ND (0.473)	ND (0.473)	ND (0.473)	0.693	ND (0.473)	ND (0.473)	4.82	ND (0.473)	5.513
VC-118	2 - 3 (ft)	8/22/2014	N	-	-	-	ND (0.686)	ND (0.686)	ND (0.686)	ND (0.686)	8.84	ND (0.686)	ND (0.686)	7.38	ND (0.686)	16.22
VC-118	3 - 4 (ft)	8/22/2014	N	-	-	-	ND (0.684)	ND (0.684)	ND (0.684)	ND (0.684)	5.8	ND (0.684)	ND (0.684)	3.4	ND (0.684)	9.2
VC-119	0 - 0.5 (ft)	8/22/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.239	ND (0.115)	ND (0.115)	0.548	ND (0.115)	0.787
VC-119	0.5 - 1 (ft)	8/22/2014	N	-	-	-	ND (0.0973)	ND (0.0973)	ND (0.0973)	ND (0.0973)	0.247	ND (0.0973)	ND (0.0973)	ND (0.0973)	ND (0.0973)	0.247
VC-119	1 - 2 (ft)	8/22/2014	N	-	-	-	ND (0.0986)	ND (0.0986)	ND (0.0986)	ND (0.0986)	0.527	ND (0.0986)	ND (0.0986)	0.0684 J	ND (0.0986)	0.5954
VC-119	2 - 3 (ft)	8/22/2014	N	-	-	-	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	1.84	ND (0.288)	ND (0.288)	8.63	ND (0.288)	10.47
VC-119	3 - 4 (ft)	8/22/2014	FD	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	2.58	ND (0.101)	ND (0.101)	0.139	ND (0.101)	2.719
VC-119	3 - 4 (ft)	8/22/2014	N	-	-	-	ND (0.393)	ND (0.393)	ND (0.393)	ND (0.393)	3.92	ND (0.393)	ND (0.393)	1.53	ND (0.393)	5.45
VC-120	0 - 0.5 (ft)	8/22/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.185	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.185
VC-120	0.5 - 1 (ft)	8/22/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.212	ND (0.101)	ND (0.101)	1.75	ND (0.101)	1.962
VC-120	1 - 2 (ft)	8/22/2014	N	-	-	-	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	0.199	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	0.199
VC-120	2 - 3 (ft)	8/22/2014	N	-	-	-	ND (0.0985)	ND (0.0985)	ND (0.0985)	ND (0.0985)	1.14	ND (0.0985)	ND (0.0985)	3.2	ND (0.0985)	4.34

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-120	3 - 4 (ft)	8/22/2014	N	-	-	-	ND (0.0837)	ND (0.0837)	ND (0.0837)	ND (0.0837)	0.548	ND (0.0837)	ND (0.0837)	0.218	ND (0.0837)	0.766
VC-121	0 - 0.5 (ft)	8/21/2014	N	-	-	-	ND (0.121)	ND (0.121)	ND (0.121)	ND (0.121)	0.338	ND (0.121)	ND (0.121)	0.446	ND (0.121)	0.784
VC-121	0.5 - 1 (ft)	8/21/2014	N	-	-	-	ND (0.0955)	ND (0.0955)	ND (0.0955)	ND (0.0955)	0.202	ND (0.0955)	ND (0.0955)	0.103	ND (0.0955)	0.305
VC-121	1 - 2 (ft)	8/21/2014	N	-	-	-	ND (0.0902)	ND (0.0902)	ND (0.0902)	ND (0.0902)	0.403	ND (0.0902)	ND (0.0902)	0.229	ND (0.0902)	0.632
VC-121	2 - 3 (ft)	8/21/2014	N	-	-	-	ND (0.0871)	ND (0.0871)	ND (0.0871)	ND (0.0871)	0.193	ND (0.0871)	ND (0.0871)	0.15	ND (0.0871)	0.343
VC-121	3 - 4 (ft)	8/21/2014	N	-	-	-	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)
VC-122	0 - 0.5 (ft)	8/21/2014	N	-	-	-	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.136	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.136
VC-122	0.5 - 1 (ft)	8/21/2014	N	-	-	-	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.194	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.194
VC-122	1 - 2 (ft)	8/21/2014	N	-	-	-	ND (0.0836)	ND (0.0836)	ND (0.0836)	ND (0.0836)	ND (0.0836)	ND (0.0836)	ND (0.0836)	1.21	ND (0.0836)	1.21
VC-122	2 - 3 (ft)	8/21/2014	N	-	-	-	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)
VC-122	3 - 4 (ft)	8/21/2014	N	-	-	-	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)
VC-123	0 - 0.5 (ft)	8/21/2014	N	-	-	-	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.172	ND (0.117)	ND (0.117)	0.15	ND (0.117)	0.322
VC-123	0.5 - 1 (ft)	8/21/2014	N	-	-	-	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.163	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.163
VC-123	1 - 2 (ft)	8/21/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.293	ND (0.101)	ND (0.101)	0.153	ND (0.101)	0.446
VC-123	2 - 3 (ft)	8/21/2014	N	-	-	-	ND (0.096)	ND (0.096)	ND (0.096)	1.46	ND (0.096)	0.545	ND (0.096)	0.323	ND (0.096)	2.328
VC-123	3 - 4 (ft)	8/21/2014	N	-	-	-	ND (16.3)	ND (16.3)	ND (16.3)	ND (16.3)	ND (16.3)	98.4	ND (16.3)	279	ND (16.3)	377.4
VC-123	4 - 6 (ft)	8/21/2014	N	-	-	-	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)
VC-124	0 - 0.5 (ft)	8/21/2014	N	-	-	-	ND (0.121)	ND (0.121)	ND (0.121)	ND (0.121)	0.212	0.121	ND (0.121)	ND (0.121)	ND (0.121)	0.333
VC-124	0.5 - 1 (ft)	8/21/2014	N	-	-	-	ND (0.106)	ND (0.106)	ND (0.106)	0.372	ND (0.106)	0.14	ND (0.106)	0.064 J	ND (0.106)	0.576
VC-124	1 - 2 (ft)	8/21/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.368	ND (0.104)	ND (0.104)	0.477	ND (0.104)	0.845
VC-124	2 - 3 (ft)	8/21/2014	N	-	-	-	ND (0.489)	ND (0.489)	ND (0.489)	ND (0.489)	0.976	ND (0.489)	ND (0.489)	7.76	ND (0.489)	8.736
VC-124	3 - 4 (ft)	8/21/2014	N	-	-	-	ND (0.482)	ND (0.482)	ND (0.482)	ND (0.482)	5.69	ND (0.482)	ND (0.482)	3.47	ND (0.482)	9.16
VC-125	0 - 0.5 (ft)	8/21/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.186	ND (0.114)	ND (0.114)	0.116	ND (0.114)	0.302
VC-125	0.5 - 1 (ft)	8/21/2014	N	-	-	-	ND (0.094)	ND (0.094)	ND (0.094)	ND (0.094)	0.207	ND (0.094)	ND (0.094)	ND (0.094)	ND (0.094)	0.207
VC-125	1 - 2 (ft)	8/21/2014	N	-	-	-	ND (0.0988)	ND (0.0988)	ND (0.0988)	ND (0.0988)	0.358	ND (0.0988)	ND (0.0988)	0.125	ND (0.0988)	0.483
VC-125	2 - 3 (ft)	8/21/2014	FD	-	-	-	ND (0.901)	ND (0.901)	ND (0.901)	ND (0.901)	5.01	ND (0.901)	ND (0.901)	14.3	ND (0.901)	19.31
VC-125	2 - 3 (ft)	8/21/2014	N	-	-	-	ND (0.0926)	ND (0.0926)	ND (0.0926)	ND (0.0926)	0.744	ND (0.0926)	ND (0.0926)	0.262	ND (0.0926)	1.006
VC-125	3 - 4 (ft)	8/21/2014	N	-	-	-	ND (0.586)	ND (0.586)	ND (0.586)	ND (0.586)	2.69	ND (0.586)	ND (0.586)	6.53	ND (0.586)	9.22
VC-126	0 - 0.5 (ft)	8/21/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.313	ND (0.118)	ND (0.118)	0.415	ND (0.118)	0.728
VC-126	0.5 - 1 (ft)	8/21/2014	FD	-	-	-	ND (0.0934)	ND (0.0934)	ND (0.0934)	ND (0.0934)	0.189	ND (0.0934)	ND (0.0934)	ND (0.0934)	ND (0.0934)	0.189
VC-126	0.5 - 1 (ft)	8/21/2014	N	-	-	-	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	0.177	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	0.177
VC-126	1 - 2 (ft)	8/21/2014	N	-	-	-	ND (0.0908)	ND (0.0908)	ND (0.0908)	ND (0.0908)	0.593	ND (0.0908)	ND (0.0908)	0.119	ND (0.0908)	0.712
VC-126	2 - 3 (ft)	8/21/2014	N	-	-	-	ND (0.277)	ND (0.277)	ND (0.277)	ND (0.277)	2.68	ND (0.277)	ND (0.277)	0.361	ND (0.277)	3.041
VC-126	3 - 4 (ft)	8/21/2014	N	-	-	-	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)
VC-127	0 - 0.5 (ft)	8/27/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.405	ND (0.116)	ND (0.116)	0.948	ND (0.116)	1.353
VC-127	0.5 - 1 (ft)	8/27/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.219	ND (0.104)	ND (0.104)	0.0945 J	ND (0.104)	0.3135
VC-127	1 - 2 (ft)	8/27/2014	N	-	-	-	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.356	ND (0.103)	ND (0.103)	0.214	ND (0.103)	0.57
VC-127	2 - 3 (ft)	8/27/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.677	ND (0.104)	ND (0.104)	0.0659 J	ND (0.104)	0.7429
VC-127	3 - 4 (ft)	8/27/2014	N	-	-	-	ND (0.58)	ND (0.58)	ND (0.58)	ND (0.58)	1.14	ND (0.58)	ND (0.58)	6.41	ND (0.58)	7.55
VC-128	0 - 0.5 (ft)	8/27/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.206	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.206
VC-128	0.5 - 1 (ft)	8/27/2014	N	-	-	-	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	15.5	ND (1.09)	15.5

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-128	1 - 2 (ft)	8/27/2014	N	-	-	-	ND (0.0994)	ND (0.0994)	ND (0.0994)	ND (0.0994)	0.287	ND (0.0994)	ND (0.0994)	0.0904 J	ND (0.0994)	0.3774
VC-128	2 - 3 (ft)	8/27/2014	N	-	-	-	ND (0.0817)	ND (0.0817)	ND (0.0817)	ND (0.0817)	0.449	ND (0.0817)	ND (0.0817)	ND (0.0817)	ND (0.0817)	0.449
VC-128	3 - 4 (ft)	8/27/2014	N	-	-	-	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)
VC-129	0 - 0.5 (ft)	8/27/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.155	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.155
VC-129	0.5 - 1 (ft)	8/27/2014	N	-	-	-	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.341	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.341
VC-129	1 - 2 (ft)	8/27/2014	N	-	-	-	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.511	ND (0.103)	ND (0.103)	0.178	ND (0.103)	0.689
VC-129	2 - 3 (ft)	8/27/2014	N	-	-	-	ND (0.0958)	ND (0.0958)	ND (0.0958)	ND (0.0958)	1.57	ND (0.0958)	ND (0.0958)	0.323	ND (0.0958)	1.893
VC-129	3 - 4 (ft)	8/27/2014	N	-	-	-	ND (0.727)	ND (0.727)	ND (0.727)	ND (0.727)	3.01	ND (0.727)	ND (0.727)	13.8	ND (0.727)	16.81
VC-130	0 - 0.5 (ft)	8/26/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.282	ND (0.114)	ND (0.114)	ND (0.114)	0.513	0.795
VC-130	0.5 - 1 (ft)	8/26/2014	N	-	-	-	ND (0.0987)	ND (0.0987)	ND (0.0987)	ND (0.0987)	0.247	ND (0.0987)	ND (0.0987)	ND (0.0987)	ND (0.0987)	0.247
VC-130	1 - 2 (ft)	8/26/2014	FD	-	-	-	ND (0.0998)	ND (0.0998)	ND (0.0998)	ND (0.0998)	0.268	ND (0.0998)	ND (0.0998)	ND (0.0998)	ND (0.0998)	0.268
VC-130	1 - 2 (ft)	8/26/2014	N	-	-	-	ND (0.0961)	ND (0.0961)	ND (0.0961)	ND (0.0961)	0.362	ND (0.0961)	ND (0.0961)	ND (0.0961)	ND (0.0961)	0.362
VC-130	2 - 3 (ft)	8/26/2014	N	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.853	ND (0.102)	0.121	ND (0.102)	ND (0.102)	0.974
VC-130	3 - 4 (ft)	8/26/2014	N	-	-	-	ND (58.3)	ND (58.3)	ND (58.3)	ND (58.3)	ND (58.3)	ND (58.3)	ND (58.3)	1090	ND (58.3)	1090
VC-130	4 - 6 (ft)	8/26/2014	N	-	-	-	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	31.6	ND (1.75)	31.6
VC-131	0 - 0.5 (ft)	8/26/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.246	ND (0.109)	ND (0.109)	0.155	ND (0.109)	0.401
VC-131	0.5 - 1 (ft)	8/26/2014	N	-	-	-	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.229	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.229
VC-131	1 - 2 (ft)	8/26/2014	N	-	-	-	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	0.232	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	0.232
VC-131	2 - 3 (ft)	8/26/2014	N	-	-	-	ND (0.0962)	ND (0.0962)	ND (0.0962)	ND (0.0962)	1.17	ND (0.0962)	ND (0.0962)	0.0637 J	ND (0.0962)	1.2337
VC-131	3 - 4 (ft)	8/26/2014	N	-	-	-	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	0.146	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	0.146
VC-132	0 - 0.5 (ft)	8/27/2014	N	-	-	-	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	0.274	ND (0.106)	ND (0.106)	0.275	ND (0.106)	0.549
VC-132	0.5 - 1 (ft)	8/27/2014	N	-	-	-	ND (0.0979)	ND (0.0979)	ND (0.0979)	ND (0.0979)	0.23	ND (0.0979)	ND (0.0979)	ND (0.0979)	ND (0.0979)	0.23
VC-132	1 - 2 (ft)	8/27/2014	N	-	-	-	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	0.464	ND (0.106)	ND (0.106)	0.274	ND (0.106)	0.738
VC-132	2 - 3 (ft)	8/27/2014	N	-	-	-	ND (0.0977)	ND (0.0977)	ND (0.0977)	ND (0.0977)	1.4	ND (0.0977)	ND (0.0977)	3.58	ND (0.0977)	4.98
VC-132	3 - 4 (ft)	8/27/2014	N	-	-	-	ND (1.04)	ND (1.04)	ND (1.04)	ND (1.04)	4.05	ND (1.04)	ND (1.04)	10.6	ND (1.04)	14.65
VC-133	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.211	ND (0.113)	ND (0.113)	0.0629 J	ND (0.113)	0.2739
VC-133	0.5 - 1 (ft)	9/30/2014	N	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.241	ND (0.105)	ND (0.105)	0.0951 J	ND (0.105)	0.3361
VC-133	1 - 2 (ft)	9/30/2014	N	-	-	-	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	0.729	ND (0.0904)	ND (0.0904)	0.443	ND (0.0904)	1.172
VC-133	2 - 3 (ft)	9/30/2014	FD	-	-	-	ND (0.193)	ND (0.193)	ND (0.193)	ND (0.193)	ND (0.193)	ND (0.193)	ND (0.193)	1.92	ND (0.193)	1.92
VC-133	2 - 3 (ft)	9/30/2014	N	-	-	-	ND (0.0862)	ND (0.0862)	ND (0.0862)	ND (0.0862)	0.45	ND (0.0862)	ND (0.0862)	1.01	ND (0.0862)	1.46
VC-133	3 - 4 (ft)	9/30/2014	N	-	-	-	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	0.106	ND (0.0936)	0.106
VC-134	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.2	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.2
VC-134	0.5 - 1 (ft)	9/30/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.295	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.295
VC-134	1 - 2 (ft)	9/30/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.56	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.56
VC-134	2 - 3 (ft)	9/30/2014	N	-	-	-	ND (0.225)	ND (0.225)	ND (0.225)	ND (0.225)	0.761	ND (0.225)	ND (0.225)	2.24	ND (0.225)	3.001
VC-134	3 - 4 (ft)	9/30/2014	N	-	-	-	ND (0.531)	ND (0.531)	ND (0.531)	ND (0.531)	4.66	ND (0.531)	ND (0.531)	0.321 J	ND (0.531)	4.981
VC-135	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.121)	ND (0.121)	ND (0.121)	ND (0.121)	0.283	ND (0.121)	ND (0.121)	0.382	ND (0.121)	0.665
VC-135	0.5 - 1 (ft)	9/30/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.577	ND (0.109)	ND (0.109)	0.743	ND (0.109)	1.32
VC-135	1 - 2 (ft)	9/30/2014	FD	-	-	-	ND (0.679)	ND (0.679)	ND (0.679)	ND (0.679)	5.3	ND (0.679)	ND (0.679)	3.62	1.76	10.68
VC-135	1 - 2 (ft)	9/30/2014	N	-	-	-	ND (0.0977)	ND (0.0977)	ND (0.0977)	ND (0.0977)	2.52	ND (0.0977)	ND (0.0977)	2.42	ND (0.0977)	4.94
VC-135	2 - 3 (ft)	9/30/2014	N	-	-	-	ND (1.11)	ND (1.11)	ND (1.11)	ND (1.11)	4.91	ND (1.11)	ND (1.11)	22.2	8.44	35.55

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-135	3 - 4 (ft)	9/30/2014	N	-	-	-	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)
VC-136	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.251	ND (0.114)	ND (0.114)	1.28	ND (0.114)	1.531
VC-136	0.5 - 1 (ft)	9/30/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.168	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.168
VC-136	1 - 2 (ft)	9/30/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.268	ND (0.101)	ND (0.101)	3.1	ND (0.101)	3.368
VC-136	2 - 3 (ft)	9/30/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.507	ND (0.101)	ND (0.101)	0.167	ND (0.101)	0.674
VC-136	3 - 4 (ft)	9/30/2014	N	-	-	-	ND (0.0867)	ND (0.0867)	ND (0.0867)	ND (0.0867)	ND (0.0867)	ND (0.0867)	ND (0.0867)	ND (0.0867)	ND (0.0867)	ND (0.0867)
VC-137	0 - 0.5 (ft)	9/12/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.261	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.261
VC-137	0.5 - 1 (ft)	9/12/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.219	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.219
VC-137	1 - 2 (ft)	9/12/2014	FD	-	-	-	ND (0.094)	ND (0.094)	ND (0.094)	ND (0.094)	0.339	ND (0.094)	ND (0.094)	0.092 J	ND (0.094)	0.431
VC-137	1 - 2 (ft)	9/12/2014	N	-	-	-	ND (0.0949)	ND (0.0949)	ND (0.0949)	ND (0.0949)	0.275	ND (0.0949)	ND (0.0949)	0.139	ND (0.0949)	0.414
VC-137	2 - 3 (ft)	9/12/2014	N	-	-	-	ND (0.0995)	ND (0.0995)	ND (0.0995)	ND (0.0995)	0.512	ND (0.0995)	ND (0.0995)	2.27	ND (0.0995)	2.782
VC-137	3 - 4 (ft)	9/12/2014	N	-	-	-	ND (0.0919)	ND (0.0919)	ND (0.0919)	ND (0.0919)	1.15	ND (0.0919)	ND (0.0919)	0.2	ND (0.0919)	1.35
VC-138	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.169	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.169
VC-138	0.5 - 1 (ft)	9/30/2014	N	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.188	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.188
VC-138	1 - 2 (ft)	9/30/2014	N	-	-	-	ND (0.0998)	ND (0.0998)	ND (0.0998)	ND (0.0998)	0.258	ND (0.0998)	ND (0.0998)	ND (0.0998)	ND (0.0998)	0.258
VC-138	2 - 3 (ft)	9/30/2014	FD	-	-	-	ND (0.0985)	ND (0.0985)	ND (0.0985)	ND (0.0985)	0.544	ND (0.0985)	ND (0.0985)	ND (0.0985)	ND (0.0985)	0.544
VC-138	2 - 3 (ft)	9/30/2014	N	-	-	-	ND (0.0902)	ND (0.0902)	ND (0.0902)	ND (0.0902)	0.771	ND (0.0902)	ND (0.0902)	0.579	ND (0.0902)	1.35
VC-138	3 - 4 (ft)	9/30/2014	N	-	-	-	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)	ND (0.0816)
VC-139	0 - 0.5 (ft)	9/12/2014	N	-	-	-	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	0.172	ND (0.126)	ND (0.126)	ND (0.126)	ND (0.126)	0.172
VC-139	0.5 - 1 (ft)	9/12/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.203	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.203
VC-139	1 - 2 (ft)	9/12/2014	FD	-	-	-	ND (0.0999)	ND (0.0999)	ND (0.0999)	ND (0.0999)	0.308	ND (0.0999)	ND (0.0999)	0.0737 J	ND (0.0999)	0.3817
VC-139	1 - 2 (ft)	9/12/2014	N	-	-	-	ND (0.0976)	ND (0.0976)	ND (0.0976)	ND (0.0976)	0.261	ND (0.0976)	ND (0.0976)	0.0661 J	ND (0.0976)	0.3271
VC-139	2 - 3 (ft)	9/12/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.728	ND (0.104)	ND (0.104)	0.727	ND (0.104)	1.455
VC-139	3 - 4 (ft)	9/12/2014	N	-	-	-	ND (60.5)	ND (60.5)	ND (60.5)	ND (60.5)	ND (60.5)	ND (60.5)	ND (60.5)	857	ND (60.5)	857
VC-139	4 - 6 (ft)	9/12/2014	N	-	-	-	ND (0.0908)	ND (0.0908)	ND (0.0908)	0.0521 J	ND (0.0908)	ND (0.0908)	0.0585 J	ND (0.0908)	ND (0.0908)	0.1106
VC-140	0 - 0.5 (ft)	9/12/2014	FD	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.191	ND (0.11)	ND (0.11)	0.0905 J	ND (0.11)	0.2815
VC-140	0 - 0.5 (ft)	9/12/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.221	ND (0.111)	ND (0.111)	0.188	ND (0.111)	0.409
VC-140	0.5 - 1 (ft)	9/12/2014	N	-	-	-	ND (0.0989)	ND (0.0989)	ND (0.0989)	ND (0.0989)	0.263	ND (0.0989)	ND (0.0989)	0.122	ND (0.0989)	0.385
VC-140	1 - 2 (ft)	9/12/2014	N	-	-	-	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	0.383	ND (0.0943)	ND (0.0943)	0.433	ND (0.0943)	0.816
VC-140	2 - 3 (ft)	9/12/2014	N	-	-	-	ND (0.0914)	ND (0.0914)	ND (0.0914)	ND (0.0914)	0.654	ND (0.0914)	ND (0.0914)	1.65	ND (0.0914)	2.304
VC-140	3 - 4 (ft)	9/12/2014	N	-	-	-	ND (0.449)	ND (0.449)	ND (0.449)	ND (0.449)	1.37	ND (0.449)	ND (0.449)	6.79	ND (0.449)	8.16
VC-141	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.182	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.182
VC-141	0.5 - 1 (ft)	9/30/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.246	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.246
VC-141	1 - 2 (ft)	9/30/2014	FD	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.196	ND (0.105)	ND (0.105)	0.129	ND (0.105)	0.325
VC-141	1 - 2 (ft)	9/30/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.226	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.226
VC-141	2 - 3 (ft)	9/30/2014	N	-	-	-	ND (0.0811)	ND (0.0811)	ND (0.0811)	ND (0.0811)	0.301	ND (0.0811)	ND (0.0811)	0.0798 J	ND (0.0811)	0.3808
VC-141	3 - 4 (ft)	9/30/2014	N	-	-	-	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)	ND (0.0893)
VC-301	0 - 0.5 (ft)	9/10/2014	N	-	-	-	ND (0.425)	ND (0.425)	ND (0.425)	ND (0.425)	0.571	ND (0.425)	ND (0.425)	5.37	2.31	8.251
VC-301	0.5 - 1 (ft)	9/10/2014	N	-	-	-	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.248	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.248
VC-301	1 - 2 (ft)	9/10/2014	FD	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.431	ND (0.118)	ND (0.118)	0.124	ND (0.118)	0.555
VC-301	1 - 2 (ft)	9/10/2014	N	-	-	-	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.466	ND (0.113)	ND (0.113)	0.117	ND (0.113)	0.583

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-301	2 - 3 (ft)	9/10/2014	N	-	-	-	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.635	ND (0.123)	ND (0.123)	0.0917 J	ND (0.123)	0.7267
VC-302	0 - 0.5 (ft)	9/8/2014	N	-	-	-	ND (0.141)	ND (0.141)	ND (0.141)	ND (0.141)	0.214	ND (0.141)	ND (0.141)	ND (0.141)	ND (0.141)	0.214
VC-302	0.5 - 1 (ft)	9/8/2014	N	-	-	-	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.288	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.288
VC-302	1 - 2 (ft)	9/8/2014	FD	-	-	-	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.789	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.789
VC-302	1 - 2 (ft)	9/8/2014	N	-	-	-	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.701	ND (0.124)	ND (0.124)	0.0739 J	ND (0.124)	0.7749
VC-302	2 - 3 (ft)	9/8/2014	N	-	-	-	ND (2.21)	ND (2.21)	ND (2.21)	ND (2.21)	7.4	ND (2.21)	ND (2.21)	50.7	ND (2.21)	58.1
VC-302	3 - 4 (ft)	9/8/2014	N	-	-	-	ND (8.79)	ND (8.79)	ND (8.79)	ND (8.79)	32.8	ND (8.79)	ND (8.79)	95.9	ND (8.79)	128.7
VC-302	4 - 5 (ft)	9/8/2014	N	-	-	-	ND (0.642)	ND (0.642)	ND (0.642)	ND (0.642)	4.72	ND (0.642)	ND (0.642)	12.7	5.63	23.05
VC-303	0 - 0.5 (ft)	9/8/2014	N	-	-	-	ND (0.136)	ND (0.136)	ND (0.136)	ND (0.136)	0.274	ND (0.136)	ND (0.136)	ND (0.136)	ND (0.136)	0.274
VC-303	0.5 - 1 (ft)	9/8/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.706	ND (0.115)	ND (0.115)	4.02	ND (0.115)	4.726
VC-303	1 - 2 (ft)	9/8/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	1.12	ND (0.111)	ND (0.111)	0.609	ND (0.111)	1.729
VC-303	2 - 3 (ft)	9/8/2014	FD	-	-	-	ND (17.8)	ND (17.8)	ND (17.8)	ND (17.8)	93.2	ND (17.8)	ND (17.8)	705	ND (17.8)	798.2
VC-303	2 - 3 (ft)	9/8/2014	N	-	-	-	ND (27.9)	ND (27.9)	ND (27.9)	ND (27.9)	121	ND (27.9)	ND (27.9)	927	ND (27.9)	1048
VC-303	3 - 4 (ft)	9/8/2014	N	-	-	-	ND (3.59)	ND (3.59)	ND (3.59)	ND (3.59)	4.6	ND (3.59)	ND (3.59)	39.2	ND (3.59)	43.8
VC-303	4 - 5 (ft)	9/8/2014	N	-	-	-	ND (17.4)	ND (17.4)	ND (17.4)	ND (17.4)	30	ND (17.4)	ND (17.4)	306	ND (17.4)	336
VC-303	5 - 6 (ft)	9/8/2014	N	-	-	-	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	ND (1.7)	31	ND (1.7)	31
VC-304	0 - 0.5 (ft)	9/8/2014	N	-	-	-	ND (0.258)	ND (0.258)	ND (0.258)	ND (0.258)	0.722	ND (0.258)	ND (0.258)	2.69	ND (0.258)	3.412
VC-304	0.5 - 1 (ft)	9/8/2014	N	-	-	-	ND (0.569)	ND (0.569)	ND (0.569)	ND (0.569)	1.23	ND (0.569)	ND (0.569)	3.22	ND (0.569)	4.45
VC-304	1 - 2 (ft)	9/8/2014	N	-	-	-	ND (0.568)	ND (0.568)	ND (0.568)	ND (0.568)	4.09	ND (0.568)	ND (0.568)	8.26	ND (0.568)	12.35
VC-304	2 - 3 (ft)	9/8/2014	FD	-	-	-	ND (9.24)	ND (9.24)	ND (9.24)	ND (9.24)	81	ND (9.24)	ND (9.24)	204	84.5	369.5
VC-304	2 - 3 (ft)	9/8/2014	N	-	-	-	ND (9.23)	ND (9.23)	ND (9.23)	ND (9.23)	76.8	ND (9.23)	ND (9.23)	178	79.9	334.7
VC-304	3 - 4 (ft)	9/8/2014	N	-	-	-	ND (359)	ND (359)	ND (359)	ND (359)	734	ND (359)	ND (359)	5640	ND (359)	6374
VC-304	4 - 5 (ft)	9/8/2014	N	-	-	-	ND (7.19)	ND (7.19)	ND (7.19)	ND (7.19)	43.1	ND (7.19)	ND (7.19)	208	ND (7.19)	251.1
VC-304	5 - 6 (ft)	9/8/2014	N	-	-	-	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	0.597	ND (0.0824)	ND (0.0824)	2.72	ND (0.0824)	3.317
VC-304	6 - 8 (ft)	9/8/2014	N	-	-	-	ND (0.0792)	ND (0.0792)	ND (0.0792)	ND (0.0792)	0.128	ND (0.0792)	ND (0.0792)	0.934	ND (0.0792)	1.062
VC-305	0 - 0.5 (ft)	9/10/2014	FD	-	-	-	ND (0.14)	ND (0.14)	ND (0.14)	ND (0.14)	0.346	ND (0.14)	ND (0.14)	0.15	0.108 J	0.604
VC-305	0 - 0.5 (ft)	9/10/2014	N	-	-	-	ND (0.135)	ND (0.135)	ND (0.135)	ND (0.135)	0.679	ND (0.135)	ND (0.135)	0.112 J	ND (0.135)	0.791
VC-305	0.5 - 1 (ft)	9/10/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.519	ND (0.115)	ND (0.115)	1.54	ND (0.115)	2.059
VC-305	1 - 2 (ft)	9/10/2014	N	-	-	-	ND (0.967)	ND (0.967)	ND (0.967)	ND (0.967)	8.81	ND (0.967)	ND (0.967)	15.2	ND (0.967)	24.01
VC-305	2 - 3 (ft)	9/10/2014	N	-	-	-	ND (19.2)	ND (19.2)	ND (19.2)	ND (19.2)	138	ND (19.2)	ND (19.2)	420	ND (19.2)	558
VC-305	3 - 4 (ft)	9/10/2014	N	-	-	-	ND (477)	ND (477)	ND (477)	ND (477)	ND (477)	ND (477)	ND (477)	6190	ND (477)	6190
VC-305	4 - 5 (ft)	9/10/2014	N	-	-	-	ND (244)	ND (244)	ND (244)	ND (244)	336	ND (244)	ND (244)	5580	ND (244)	5916
VC-305	5 - 6 (ft)	9/10/2014	N	-	-	-	ND (3.92)	ND (3.92)	ND (3.92)	ND (3.92)	10.8	ND (3.92)	ND (3.92)	38.1	ND (3.92)	48.9
VC-306	0 - 0.5 (ft)	9/9/2014	N	-	-	-	ND (0.133)	ND (0.133)	ND (0.133)	ND (0.133)	0.227	ND (0.133)	ND (0.133)	ND (0.133)	ND (0.133)	0.227
VC-306	0.5 - 1 (ft)	9/9/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.462	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.462
VC-306	1 - 2 (ft)	9/9/2014	FD	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.949	ND (0.105)	ND (0.105)	0.826	ND (0.105)	1.775
VC-306	1 - 2 (ft)	9/9/2014	N	-	-	-	ND (1.01)	ND (1.01)	ND (1.01)	ND (1.01)	1.76	ND (1.01)	ND (1.01)	9.66	ND (1.01)	11.42
VC-306	2 - 3 (ft)	9/9/2014	N	-	-	-	ND (73.9)	ND (73.9)	ND (73.9)	ND (73.9)	137	ND (73.9)	ND (73.9)	1380	ND (73.9)	1517
VC-306	3 - 4 (ft)	9/9/2014	N	-	-	-	ND (18.6)	ND (18.6)	ND (18.6)	ND (18.6)	52.6	ND (18.6)	ND (18.6)	510	ND (18.6)	562.6
VC-306	4 - 5 (ft)	9/9/2014	N	-	-	-	ND (5.33)	ND (5.33)	ND (5.33)	ND (5.33)	8.87	ND (5.33)	ND (5.33)	104	ND (5.33)	112.87
VC-306	5 - 6 (ft)	9/9/2014	N	-	-	-	ND (8.83)	ND (8.83)	ND (8.83)	ND (8.83)	46.8	ND (8.83)	ND (8.83)	158	ND (8.83)	204.8

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-306	6 - 8 (ft)	9/9/2014	N	-	-	-	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	0.178	ND (0.0898)	ND (0.0898)	0.742	ND (0.0898)	0.92
VC-307	0 - 0.5 (ft)	9/9/2014	FD	-	-	-	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	0.364	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	0.364
VC-307	0 - 0.5 (ft)	9/9/2014	N	-	-	-	ND (0.14)	ND (0.14)	ND (0.14)	ND (0.14)	0.404	ND (0.14)	ND (0.14)	0.855	ND (0.14)	1.259
VC-307	0.5 - 1 (ft)	9/9/2014	N	-	-	-	ND (72.6)	ND (72.6)	ND (72.6)	ND (72.6)	71.6 J	ND (72.6)	ND (72.6)	825	ND (72.6)	896.6
VC-307	1 - 2 (ft)	9/9/2014	N	-	-	-	ND (2.5)	ND (2.5)	ND (2.5)	ND (2.5)	9.2	ND (2.5)	ND (2.5)	51.3	ND (2.5)	60.5
VC-307	2 - 3 (ft)	9/9/2014	N	-	-	-	ND (0.083)	ND (0.083)	ND (0.083)	ND (0.083)	0.177	ND (0.083)	ND (0.083)	0.854	ND (0.083)	1.031
VC-308	0 - 0.5 (ft)	9/9/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.378	ND (0.101)	ND (0.101)	0.703	ND (0.101)	1.081
VC-308	0.5 - 1 (ft)	9/9/2014	FD	-	-	-	ND (4.41)	ND (4.41)	ND (4.41)	ND (4.41)	23	ND (4.41)	ND (4.41)	78.9	ND (4.41)	101.9
VC-308	0.5 - 1 (ft)	9/9/2014	N	-	-	-	ND (3.48)	ND (3.48)	ND (3.48)	ND (3.48)	21.7	ND (3.48)	ND (3.48)	61.8	ND (3.48)	83.5
VC-308	1 - 2 (ft)	9/9/2014	N	-	-	-	ND (5.33)	ND (5.33)	ND (5.33)	ND (5.33)	21.8	ND (5.33)	ND (5.33)	106	ND (5.33)	127.8
VC-308	2 - 3 (ft)	9/9/2014	N	-	-	-	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	0.354	ND (0.0879)	0.354
VC-309	0 - 0.5 (ft)	9/10/2014	N	-	-	-	ND (0.333)	ND (0.333)	ND (0.333)	ND (0.333)	1.45	ND (0.333)	ND (0.333)	4.81	ND (0.333)	6.26
VC-309	0.5 - 1 (ft)	9/10/2014	N	-	-	-	ND (0.705)	ND (0.705)	ND (0.705)	ND (0.705)	8.8	ND (0.705)	ND (0.705)	7.03	ND (0.705)	15.83
VC-309	1 - 2 (ft)	9/10/2014	N	-	-	-	ND (1.86)	ND (1.86)	ND (1.86)	ND (1.86)	11.9	ND (1.86)	ND (1.86)	25.8	ND (1.86)	37.7
VC-309	2 - 3 (ft)	9/10/2014	FD	-	-	-	ND (52.8)	ND (52.8)	ND (52.8)	ND (52.8)	139	ND (52.8)	ND (52.8)	1120	ND (52.8)	1259
VC-309	2 - 3 (ft)	9/10/2014	N	-	-	-	ND (20.1)	ND (20.1)	ND (20.1)	ND (20.1)	83.8	ND (20.1)	ND (20.1)	389	ND (20.1)	472.8
VC-309	3 - 4 (ft)	9/10/2014	N	-	-	-	ND (32.9)	ND (32.9)	ND (32.9)	ND (32.9)	150	ND (32.9)	ND (32.9)	654	ND (32.9)	804
VC-309	4 - 5 (ft)	9/10/2014	N	-	-	-	ND (6.19)	ND (6.19)	ND (6.19)	ND (6.19)	109	ND (6.19)	ND (6.19)	215	101	425
VC-309	5 - 6 (ft)	9/10/2014	N	-	-	-	ND (71.5)	ND (71.5)	ND (71.5)	ND (71.5)	346	ND (71.5)	ND (71.5)	1750	ND (71.5)	2096
VC-309	6 - 8 (ft)	9/10/2014	N	-	-	-	ND (3.36)	ND (3.36)	ND (3.36)	ND (3.36)	12.7	ND (3.36)	ND (3.36)	46.4	ND (3.36)	59.1
VC-310	0 - 0.5 (ft)	9/10/2014	FD	-	-	-	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.255	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.255
VC-310	0 - 0.5 (ft)	9/10/2014	N	-	-	-	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.299	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.299
VC-310	0.5 - 1 (ft)	9/10/2014	N	-	-	-	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	0.35	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	0.35
VC-310	1 - 2 (ft)	9/10/2014	N	-	-	-	ND (1.82)	ND (1.82)	ND (1.82)	ND (1.82)	ND (1.82)	6.61	ND (1.82)	31.8	ND (1.82)	38.41
VC-310	2 - 3 (ft)	9/10/2014	N	-	-	-	ND (0.0918)	ND (0.0918)	ND (0.0918)	ND (0.0918)	ND (0.0918)	1.92	ND (0.0918)	ND (0.0918)	ND (0.0918)	1.92
VC-310	3 - 4 (ft)	9/10/2014	N	-	-	-	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)
VC-310	4 - 5 (ft)	9/10/2014	N	-	-	-	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)	ND (0.0878)
VC-310	5 - 6 (ft)	9/10/2014	N	-	-	-	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)
VC-311	0 - 0.5 (ft)	9/10/2014	N	-	-	-	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.332	ND (0.132)	ND (0.132)	0.198	ND (0.132)	0.53
VC-311	0.5 - 1 (ft)	9/10/2014	N	-	-	-	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.437	ND (0.1)	ND (0.1)	1.68	ND (0.1)	2.117
VC-311	1 - 2 (ft)	9/10/2014	N	-	-	-	ND (0.932)	ND (0.932)	ND (0.932)	ND (0.932)	5.28	ND (0.932)	ND (0.932)	9.38	ND (0.932)	14.66
VC-311	2 - 3 (ft)	9/10/2014	N	-	-	-	ND (0.974)	ND (0.974)	ND (0.974)	ND (0.974)	5.16	ND (0.974)	ND (0.974)	15	ND (0.974)	20.16
VC-311	3 - 4 (ft)	9/10/2014	N	-	-	-	ND (0.258)	ND (0.258)	ND (0.258)	ND (0.258)	0.992	ND (0.258)	ND (0.258)	1.23	ND (0.258)	2.22
VC-311	4 - 5 (ft)	9/10/2014	N	-	-	-	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)
VC-311	5 - 6 (ft)	9/10/2014	N	-	-	-	ND (247)	ND (247)	ND (247)	ND (247)	710	ND (247)	ND (247)	9110	ND (247)	9820
VC-312	0 - 0.5 (ft)	9/9/2014	N	-	-	-	ND (0.144)	ND (0.144)	ND (0.144)	ND (0.144)	0.555	ND (0.144)	ND (0.144)	0.498	ND (0.144)	1.053
VC-312	0.5 - 1 (ft)	9/9/2014	N	-	-	-	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.167	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.167
VC-312	1 - 2 (ft)	9/9/2014	N	-	-	-	ND (0.0919)	ND (0.0919)	ND (0.0919)	ND (0.0919)	ND (0.0919)	ND (0.0919)	ND (0.0919)	0.23	ND (0.0919)	0.23
VC-312	2 - 3 (ft)	9/9/2014	N	-	-	-	ND (5.22)	ND (5.22)	ND (5.22)	ND (5.22)	19.4	ND (5.22)	ND (5.22)	102	ND (5.22)	121.4
VC-312	3 - 4 (ft)	9/9/2014	N	-	-	-	ND (2.66)	ND (2.66)	ND (2.66)	ND (2.66)	15.5	ND (2.66)	ND (2.66)	ND (2.66)	23.1	38.6
VC-313	0 - 0.5 (ft)	9/10/2014	N	-	-	-	ND (0.138)	ND (0.138)	ND (0.138)	ND (0.138)	ND (0.138)	ND (0.138)	ND (0.138)	0.135 J	ND (0.138)	0.135 J

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-313	0.5 - 1 (ft)	9/10/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.36	ND (0.119)	ND (0.119)	0.209	ND (0.119)	0.569
VC-313	1 - 2 (ft)	9/10/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.668	ND (0.116)	ND (0.116)	0.412	ND (0.116)	1.08
VC-313	2 - 3 (ft)	9/10/2014	N	-	-	-	ND (0.439)	ND (0.439)	ND (0.439)	ND (0.439)	1.47	ND (0.439)	ND (0.439)	3.71	ND (0.439)	5.18
VC-313	3 - 4 (ft)	9/10/2014	N	-	-	-	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)
VC-313	5 - 6 (ft)	9/10/2014	N	-	-	-	ND (0.0862)	ND (0.0862)	ND (0.0862)	ND (0.0862)	ND (0.0862)	ND (0.0862)	ND (0.0862)	ND (0.0862)	ND (0.0862)	ND (0.0862)
VC-314	0 - 0.5 (ft)	9/4/2014	N	-	-	-	ND (1.25)	ND (1.25)	ND (1.25)	ND (1.25)	2.43	ND (1.25)	ND (1.25)	17.6	ND (1.25)	20.03
VC-314	0.5 - 1 (ft)	9/4/2014	N	-	-	-	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	0.343	ND (0.129)	ND (0.129)	0.158	ND (0.129)	0.501
VC-314	1 - 2 (ft)	9/4/2014	FD	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	1.1	ND (0.105)	ND (0.105)	1.12	ND (0.105)	2.22
VC-314	1 - 2 (ft)	9/4/2014	N	-	-	-	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	1.12	ND (0.107)	ND (0.107)	0.605	ND (0.107)	1.725
VC-314	2 - 3 (ft)	9/4/2014	N	-	-	-	ND (0.0861)	ND (0.0861)	ND (0.0861)	ND (0.0861)	0.228	ND (0.0861)	ND (0.0861)	0.0761 J	ND (0.0861)	0.3041
VC-314	4 - 5 (ft)	9/4/2014	N	-	-	-	ND (0.0876)	ND (0.0876)	ND (0.0876)	ND (0.0876)	0.546	ND (0.0876)	ND (0.0876)	0.737	ND (0.0876)	1.283
VC-314	5 - 6 (ft)	9/4/2014	N	-	-	-	ND (0.855)	ND (0.855)	ND (0.855)	ND (0.855)	2.78	ND (0.855)	ND (0.855)	10	ND (0.855)	12.78
VC-315	0 - 0.5 (ft)	9/4/2014	N	-	-	-	ND (0.288)	ND (0.288)	ND (0.288)	ND (0.288)	0.618	ND (0.288)	ND (0.288)	3.67	ND (0.288)	4.288
VC-315	0.5 - 1 (ft)	9/4/2014	N	-	-	-	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.647	ND (0.127)	ND (0.127)	0.473	ND (0.127)	1.12
VC-315	1 - 2 (ft)	9/4/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.971	ND (0.12)	ND (0.12)	0.167	ND (0.12)	1.138
VC-315	2 - 3 (ft)	9/4/2014	N	-	-	-	ND (0.35)	ND (0.35)	ND (0.35)	ND (0.35)	2.85	ND (0.35)	ND (0.35)	0.308 J	ND (0.35)	3.158
VC-315	3 - 4 (ft)	9/4/2014	N	-	-	-	ND (2.99)	ND (2.99)	ND (2.99)	ND (2.99)	22.7	ND (2.99)	ND (2.99)	26.7	11.7	61.1
VC-315	4 - 5 (ft)	9/4/2014	N	-	-	-	ND (4.86)	ND (4.86)	ND (4.86)	ND (4.86)	26.3	ND (4.86)	ND (4.86)	58.8	ND (4.86)	85.1
VC-315	5 - 6 (ft)	9/4/2014	N	-	-	-	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	0.107	ND (0.0845)	0.107
VC-315	6 - 8 (ft)	9/4/2014	N	-	-	-	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)	ND (0.0941)
VC-316	0 - 0.5 (ft)	9/4/2014	N	-	-	-	ND (0.133)	ND (0.133)	ND (0.133)	ND (0.133)	0.388	ND (0.133)	ND (0.133)	0.442	ND (0.133)	0.83
VC-316	0.5 - 1 (ft)	9/4/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.796	ND (0.12)	ND (0.12)	0.633	ND (0.12)	1.429
VC-316	1 - 2 (ft)	9/4/2014	N	-	-	-	ND (0.491)	ND (0.491)	ND (0.491)	ND (0.491)	5.13	ND (0.491)	ND (0.491)	4.24	ND (0.491)	9.37
VC-316	2 - 3 (ft)	9/4/2014	N	-	-	-	ND (29.9)	ND (29.9)	ND (29.9)	ND (29.9)	76.2	ND (29.9)	ND (29.9)	695	ND (29.9)	771.2
VC-316	3 - 4 (ft)	9/4/2014	N	-	-	-	ND (0.389)	ND (0.389)	ND (0.389)	ND (0.389)	4.87	ND (0.389)	ND (0.389)	7.56	ND (0.389)	12.43
VC-316	4 - 5 (ft)	9/4/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	1.08	ND (0.118)	ND (0.118)	2.05	ND (0.118)	3.13
VC-316	5 - 6 (ft)	9/4/2014	N	-	-	-	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	0.619	ND (0.106)	ND (0.106)	0.29	ND (0.106)	0.909
VC-316	6 - 8 (ft)	9/4/2014	N	-	-	-	ND (1.92)	ND (1.92)	ND (1.92)	ND (1.92)	14.2	ND (1.92)	ND (1.92)	31.9	ND (1.92)	46.1
VC-317	0 - 0.5 (ft)	9/10/2014	N	-	-	-	ND (0.137)	ND (0.137)	ND (0.137)	ND (0.137)	0.532	ND (0.137)	ND (0.137)	0.558	ND (0.137)	1.09
VC-317	0.5 - 1 (ft)	9/10/2014	N	-	-	-	ND (0.121)	ND (0.121)	ND (0.121)	ND (0.121)	0.35	ND (0.121)	ND (0.121)	0.112 J	ND (0.121)	0.462
VC-317	1 - 2 (ft)	9/10/2014	FD	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.541	ND (0.115)	ND (0.115)	0.245	ND (0.115)	0.786
VC-317	1 - 2 (ft)	9/10/2014	N	-	-	-	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	ND (0.228)	3.65	ND (0.228)	3.65
VC-317	2 - 3 (ft)	9/10/2014	N	-	-	-	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.789	ND (0.117)	ND (0.117)	0.245	ND (0.117)	1.034
VC-317	3 - 4 (ft)	9/10/2014	N	-	-	-	ND (0.72)	ND (0.72)	ND (0.72)	ND (0.72)	10.1	ND (0.72)	ND (0.72)	9.82	ND (0.72)	19.92
VC-317	4 - 5 (ft)	9/10/2014	N	-	-	-	ND (22.5)	ND (22.5)	ND (22.5)	ND (22.5)	ND (22.5)	ND (22.5)	ND (22.5)	527	ND (22.5)	527
VC-317	5 - 6 (ft)	9/10/2014	N	-	-	-	ND (0.0869)	ND (0.0869)	ND (0.0869)	ND (0.0869)	0.0679 J	ND (0.0869)	ND (0.0869)	ND (0.0869)	ND (0.0869)	0.0679 J
VC-317	6 - 8 (ft)	9/10/2014	N	-	-	-	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)	ND (0.0873)
VC-318	0 - 0.5 (ft)	9/10/2014	N	-	-	-	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.698	ND (0.132)	ND (0.132)	1.41	ND (0.132)	2.108
VC-318	0.5 - 1 (ft)	9/10/2014	N	-	-	-	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.263	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.263
VC-318	1 - 2 (ft)	9/10/2014	FD	-	-	-	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.36	ND (0.113)	ND (0.113)	0.108 J	ND (0.113)	0.468
VC-318	1 - 2 (ft)	9/10/2014	N	-	-	-	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	0.368	ND (0.108)	ND (0.108)	0.0708 J	ND (0.108)	0.4388

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-318	2 - 3 (ft)	9/10/2014	N	-	-	-	ND (37.7)	ND (37.7)	ND (37.7)	ND (37.7)	93.6	ND (37.7)	ND (37.7)	630	ND (37.7)	723.6
VC-318	3 - 4 (ft)	9/10/2014	N	-	-	-	ND (0.391)	ND (0.391)	ND (0.391)	ND (0.391)	1.67	ND (0.391)	ND (0.391)	11.1	ND (0.391)	12.77
VC-318	4 - 5 (ft)	9/10/2014	N	-	-	-	ND (0.087)	ND (0.087)	ND (0.087)	0.198	ND (0.087)	ND (0.087)	ND (0.087)	ND (0.087)	ND (0.087)	0.198
VC-318	5 - 6 (ft)	9/10/2014	N	-	-	-	ND (6.25)	ND (6.25)	ND (6.25)	ND (6.25)	ND (6.25)	ND (6.25)	ND (6.25)	110	ND (6.25)	110
VC-318	6 - 8 (ft)	9/10/2014	N	-	-	-	ND (39.9)	ND (39.9)	ND (39.9)	ND (39.9)	84.6	ND (39.9)	ND (39.9)	911	ND (39.9)	995.6
VC-319	0 - 0.5 (ft)	9/3/2014	N	-	-	-	ND (0.144)	ND (0.144)	ND (0.144)	ND (0.144)	0.264	ND (0.144)	ND (0.144)	ND (0.144)	ND (0.144)	0.264
VC-319	0.5 - 1 (ft)	9/3/2014	FD	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.396	ND (0.101)	ND (0.101)	0.549	ND (0.101)	0.945
VC-319	0.5 - 1 (ft)	9/3/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.348	ND (0.104)	ND (0.104)	0.247	ND (0.104)	0.595
VC-319	1 - 2 (ft)	9/3/2014	N	-	-	-	ND (0.0874)	ND (0.0874)	ND (0.0874)	ND (0.0874)	0.0901	ND (0.0874)	ND (0.0874)	0.384	ND (0.0874)	0.4741
VC-319	2 - 3 (ft)	9/3/2014	N	-	-	-	ND (0.09)	ND (0.09)	ND (0.09)	ND (0.09)	ND (0.09)	ND (0.09)	ND (0.09)	ND (0.09)	ND (0.09)	ND (0.09)
VC-320	0 - 0.5 (ft)	9/3/2014	N	-	-	-	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	0.296	ND (0.142)	ND (0.142)	0.235	ND (0.142)	0.531
VC-320	0.5 - 1 (ft)	9/3/2014	N	-	-	-	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	ND (1.2)	22.3	ND (1.2)	22.3
VC-320	1 - 2 (ft)	9/3/2014	FD	-	-	-	ND (0.0871)	ND (0.0871)	ND (0.0871)	ND (0.0871)	0.364	ND (0.0871)	ND (0.0871)	0.211	ND (0.0871)	0.575
VC-320	1 - 2 (ft)	9/3/2014	N	-	-	-	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	5.14	ND (0.261)	5.14
VC-320	2 - 3 (ft)	9/3/2014	N	-	-	-	ND (0.0929)	ND (0.0929)	ND (0.0929)	ND (0.0929)	ND (0.0929)	ND (0.0929)	ND (0.0929)	ND (0.0929)	ND (0.0929)	ND (0.0929)
VC-321	0 - 0.5 (ft)	9/3/2014	N	-	-	-	ND (0.134)	ND (0.134)	ND (0.134)	ND (0.134)	0.288	ND (0.134)	ND (0.134)	ND (0.134)	ND (0.134)	0.288
VC-321	0.5 - 1 (ft)	9/3/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.266	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.266
VC-321	1 - 2 (ft)	9/3/2014	N	-	-	-	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	ND (5.63)	126	ND (5.63)	126
VC-321	2 - 3 (ft)	9/3/2014	FD	-	-	-	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)	ND (0.072)
VC-321	2 - 3 (ft)	9/3/2014	N	-	-	-	ND (0.689)	ND (0.689)	ND (0.689)	ND (0.689)	ND (0.689)	ND (0.689)	ND (0.689)	12.8	ND (0.689)	12.8
VC-322	0 - 0.5 (ft)	9/3/2014	FD	-	-	-	ND (3.65)	ND (3.65)	ND (3.65)	ND (3.65)	ND (3.65)	ND (3.65)	ND (3.65)	61.5	ND (3.65)	61.5
VC-322	0 - 0.5 (ft)	9/3/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.334	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.334
VC-322	0.5 - 1 (ft)	9/3/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.349	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.349
VC-322	1 - 2 (ft)	9/3/2014	N	-	-	-	ND (3.08)	ND (3.08)	ND (3.08)	ND (3.08)	ND (3.08)	ND (3.08)	ND (3.08)	57.1	ND (3.08)	57.1
VC-322	2 - 3 (ft)	9/3/2014	N	-	-	-	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)
VC-323	0 - 0.5 (ft)	9/3/2014	N	-	-	-	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.296	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.296
VC-323	0.5 - 1 (ft)	9/3/2014	FD	-	-	-	ND (17.6)	ND (17.6)	ND (17.6)	ND (17.6)	ND (17.6)	ND (17.6)	ND (17.6)	435	259	694
VC-323	0.5 - 1 (ft)	9/3/2014	N	-	-	-	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	24.5	ND (1.68)	24.5
VC-323	1 - 2 (ft)	9/3/2014	N	-	-	-	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	0.52	ND (0.0884)	0.52
VC-323	2 - 3 (ft)	9/3/2014	N	-	-	-	ND (0.0723)	ND (0.0723)	ND (0.0723)	ND (0.0723)	ND (0.0723)	ND (0.0723)	ND (0.0723)	ND (0.0723)	ND (0.0723)	ND (0.0723)
VC-324	0 - 0.5 (ft)	9/3/2014	N	-	-	-	ND (0.275)	ND (0.275)	ND (0.275)	ND (0.275)	0.351	ND (0.275)	ND (0.275)	ND (0.275)	ND (0.275)	0.351
VC-324	0.5 - 1 (ft)	9/3/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.257	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.257
VC-324	1 - 2 (ft)	9/3/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.518	ND (0.104)	ND (0.104)	0.211	ND (0.104)	0.729
VC-324	2 - 3 (ft)	9/3/2014	FD	-	-	-	ND (0.0974)	ND (0.0974)	ND (0.0974)	ND (0.0974)	ND (0.0974)	ND (0.0974)	ND (0.0974)	2.44	ND (0.0974)	2.44
VC-324	2 - 3 (ft)	9/3/2014	N	-	-	-	ND (0.0935)	ND (0.0935)	ND (0.0935)	ND (0.0935)	0.218	ND (0.0935)	ND (0.0935)	0.132	ND (0.0935)	0.35
VC-325	0 - 0.5 (ft)	9/3/2014	N	-	-	-	ND (0.136)	ND (0.136)	ND (0.136)	ND (0.136)	0.713	1.21	ND (0.136)	0.446	ND (0.136)	2.369
VC-325	0.5 - 1 (ft)	9/3/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.375	ND (0.116)	ND (0.116)	1.86	ND (0.116)	2.235
VC-325	1 - 2 (ft)	9/3/2014	N	-	-	-	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	ND (1.68)	31.9	ND (1.68)	31.9
VC-325	2 - 3 (ft)	9/3/2014	N	-	-	-	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)	ND (0.0909)
VC-326	0 - 0.5 (ft)	9/4/2014	FD	-	-	-	ND (0.13)	ND (0.13)	ND (0.13)	ND (0.13)	0.291	ND (0.13)	ND (0.13)	0.106 J	ND (0.13)	0.397
VC-326	0 - 0.5 (ft)	9/4/2014	N	-	-	-	ND (0.258)	ND (0.258)	ND (0.258)	ND (0.258)	1.34	ND (0.258)	ND (0.258)	3.7	2.04	7.08

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-326	0.5 - 1 (ft)	9/4/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.602	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.602
VC-326	1 - 2 (ft)	9/4/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.426	ND (0.116)	ND (0.116)	0.094 J	ND (0.116)	0.52
VC-326	2 - 3 (ft)	9/4/2014	N	-	-	-	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.725	ND (0.117)	ND (0.117)	0.106 J	ND (0.117)	0.831
VC-326	3 - 4 (ft)	9/4/2014	N	-	-	-	ND (0.607)	ND (0.607)	ND (0.607)	ND (0.607)	4.9	ND (0.607)	ND (0.607)	8.28	2.94	16.12
VC-326	4 - 5 (ft)	9/4/2014	N	-	-	-	ND (0.347)	ND (0.347)	ND (0.347)	ND (0.347)	1.11	ND (0.347)	ND (0.347)	3.02	1.44	5.57
VC-326	5 - 6 (ft)	9/4/2014	N	-	-	-	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)
VC-326	6 - 8 (ft)	9/4/2014	N	-	-	-	ND (0.0877)	ND (0.0877)	ND (0.0877)	ND (0.0877)	0.391	ND (0.0877)	ND (0.0877)	0.0688 J	ND (0.0877)	0.4598
VC-327	0 - 0.5 (ft)	9/4/2014	N	-	-	-	ND (0.134)	ND (0.134)	ND (0.134)	ND (0.134)	0.334	ND (0.134)	ND (0.134)	0.895	ND (0.134)	1.229
VC-327	0.5 - 1 (ft)	9/4/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.458	ND (0.114)	ND (0.114)	0.0818 J	ND (0.114)	0.5398
VC-327	1 - 2 (ft)	9/4/2014	FD	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	3.14	ND (0.115)	ND (0.115)	1.35	ND (0.115)	4.49
VC-327	1 - 2 (ft)	9/4/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	2.85	ND (0.114)	ND (0.114)	0.884	ND (0.114)	3.734
VC-327	2 - 3 (ft)	9/4/2014	N	-	-	-	ND (19.7)	ND (19.7)	ND (19.7)	ND (19.7)	38.6	ND (19.7)	ND (19.7)	272	ND (19.7)	310.6
VC-327	3 - 4 (ft)	9/4/2014	N	-	-	-	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	0.376	ND (0.088)	0.376
VC-327	4 - 5 (ft)	9/4/2014	N	-	-	-	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	1.82	ND (0.0846)	1.82
VC-327	5 - 6 (ft)	9/4/2014	N	-	-	-	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)
VC-327	6 - 8 (ft)	9/4/2014	N	-	-	-	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	ND (0.142)	1.29	ND (0.142)	1.29
VC-328	0 - 0.5 (ft)	9/4/2014	N	-	-	-	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	0.277	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	0.277
VC-328	0.5 - 1 (ft)	9/4/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.33	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.33
VC-328	1 - 2 (ft)	9/4/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.393	ND (0.116)	ND (0.116)	0.797	ND (0.116)	1.19
VC-328	2 - 3 (ft)	9/4/2014	FD	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)
VC-328	2 - 3 (ft)	9/4/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.636	ND (0.118)	ND (0.118)	0.0812 J	ND (0.118)	0.7172
VC-328	3 - 4 (ft)	9/4/2014	N	-	-	-	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	1.31	ND (0.107)	ND (0.107)	0.504	ND (0.107)	1.814
VC-328	4 - 5 (ft)	9/4/2014	N	-	-	-	ND (0.503)	ND (0.503)	ND (0.503)	ND (0.503)	5.12	ND (0.503)	ND (0.503)	5.43	2.56	13.11
VC-328	5 - 6 (ft)	9/4/2014	N	-	-	-	ND (202)	ND (202)	ND (202)	ND (202)	1010	ND (202)	ND (202)	3930	1960	6900
VC-328	6 - 8 (ft)	9/4/2014	N	-	-	-	ND (0.0901)	ND (0.0901)	ND (0.0901)	ND (0.0901)	0.15	ND (0.0901)	ND (0.0901)	0.457	ND (0.0901)	0.607
VC-329	0 - 0.5 (ft)	9/4/2014	N	-	-	-	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	0.149	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	0.149
VC-329	0.5 - 1 (ft)	9/4/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.203	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.203
VC-329	1 - 2 (ft)	9/4/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.294	ND (0.112)	ND (0.112)	0.103 J	ND (0.112)	0.397
VC-329	2 - 3 (ft)	9/4/2014	FD	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.425	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.425
VC-329	2 - 3 (ft)	9/4/2014	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.385	ND (0.11)	ND (0.11)	0.0809 J	ND (0.11)	0.4659
VC-329	3 - 4 (ft)	9/4/2014	N	-	-	-	ND (2.82)	ND (2.82)	ND (2.82)	ND (2.82)	8.77	ND (2.82)	ND (2.82)	44.3	ND (2.82)	53.07
VC-329	4 - 5 (ft)	9/4/2014	N	-	-	-	ND (0.492)	ND (0.492)	ND (0.492)	ND (0.492)	0.907	ND (0.492)	ND (0.492)	4.71	ND (0.492)	5.617
VC-329	5 - 6 (ft)	9/4/2014	N	-	-	-	ND (0.0906)	ND (0.0906)	ND (0.0906)	ND (0.0906)	ND (0.0906)	ND (0.0906)	ND (0.0906)	0.274	ND (0.0906)	0.274
VC-329	6 - 8 (ft)	9/4/2014	N	-	-	-	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)
VC-330	0 - 0.5 (ft)	9/5/2014	N	-	-	-	ND (1.45)	ND (1.45)	ND (1.45)	ND (1.45)	3.78	ND (1.45)	ND (1.45)	21.2	ND (1.45)	24.98
VC-330	0.5 - 1 (ft)	9/5/2014	N	-	-	-	ND (58.3)	ND (58.3)	ND (58.3)	ND (58.3)	152	ND (58.3)	ND (58.3)	744	ND (58.3)	896
VC-330	1 - 2 (ft)	9/5/2014	FD	-	-	-	ND (32)	ND (32)	ND (32)	ND (32)	109	ND (32)	ND (32)	387	ND (32)	496
VC-330	1 - 2 (ft)	9/5/2014	N	-	-	-	ND (18.2)	ND (18.2)	ND (18.2)	ND (18.2)	74.7	ND (18.2)	ND (18.2)	178	ND (18.2)	252.7
VC-330	2 - 3 (ft)	9/5/2014	N	-	-	-	ND (1.88)	ND (1.88)	ND (1.88)	ND (1.88)	18.9	ND (1.88)	ND (1.88)	52.7	ND (1.88)	71.6
VC-330	3 - 4 (ft)	9/5/2014	N	-	-	-	ND (8.33)	ND (8.33)	ND (8.33)	ND (8.33)	32.9	ND (8.33)	ND (8.33)	121	ND (8.33)	153.9
VC-330	4 - 5 (ft)	9/5/2014	N	-	-	-	ND (1.81)	ND (1.81)	ND (1.81)	ND (1.81)	10.9	ND (1.81)	ND (1.81)	19.9	ND (1.81)	30.8

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-331	0 - 0.5 (ft)	9/5/2014	N	-	-	-	ND (1.85)	ND (1.85)	ND (1.85)	ND (1.85)	4.53	ND (1.85)	ND (1.85)	26	ND (1.85)	30.53
VC-331	0.5 - 1 (ft)	9/5/2014	N	-	-	-	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	1	ND (0.103)	ND (0.103)	0.85	ND (0.103)	1.85
VC-331	1 - 2 (ft)	9/5/2014	FD	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)
VC-331	1 - 2 (ft)	9/5/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)
VC-331	2 - 3 (ft)	9/5/2014	N	-	-	-	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)	ND (0.097)
VC-331	3 - 4 (ft)	9/5/2014	N	-	-	-	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)
VC-332	0 - 0.5 (ft)	9/5/2014	FD	-	-	-	ND (0.265)	ND (0.265)	ND (0.265)	ND (0.265)	0.268	ND (0.265)	ND (0.265)	ND (0.265)	ND (0.265)	0.268
VC-332	0 - 0.5 (ft)	9/5/2014	N	-	-	-	ND (0.138)	ND (0.138)	ND (0.138)	ND (0.138)	0.309	ND (0.138)	ND (0.138)	0.165	ND (0.138)	0.474
VC-332	0.5 - 1 (ft)	9/5/2014	N	-	-	-	ND (0.961)	ND (0.961)	ND (0.961)	ND (0.961)	5.85	ND (0.961)	ND (0.961)	15	ND (0.961)	20.85
VC-332	1 - 2 (ft)	9/5/2014	N	-	-	-	ND (0.725)	ND (0.725)	ND (0.725)	ND (0.725)	11.6	ND (0.725)	ND (0.725)	13.2	ND (0.725)	24.8
VC-332	2 - 3 (ft)	9/5/2014	N	-	-	-	ND (3.12)	ND (3.12)	ND (3.12)	ND (3.12)	20.8	ND (3.12)	ND (3.12)	37.3	ND (3.12)	58.1
VC-332	3 - 4 (ft)	9/5/2014	N	-	-	-	ND (9.02)	ND (9.02)	ND (9.02)	ND (9.02)	66.8	ND (9.02)	ND (9.02)	208	ND (9.02)	274.8
VC-332	4 - 5 (ft)	9/5/2014	N	-	-	-	ND (2.03)	ND (2.03)	ND (2.03)	ND (2.03)	12.1	ND (2.03)	ND (2.03)	16.5	ND (2.03)	28.6
VC-334	0 - 0.5 (ft)	10/1/2014	N	-	-	-	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.637	ND (0.132)	ND (0.132)	1.1	0.529	2.266
VC-334	0.5 - 1 (ft)	10/1/2014	N	-	-	-	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	0.321	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	0.321
VC-334	1 - 2 (ft)	10/1/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.41	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.41
VC-334	2 - 3 (ft)	10/1/2014	FD	-	-	-	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.649	ND (0.123)	ND (0.123)	0.0835 J	ND (0.123)	0.733
VC-334	2 - 3 (ft)	10/1/2014	N	-	-	-	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	0.655	ND (0.122)	ND (0.122)	0.0816 J	ND (0.122)	0.737
VC-334	3 - 4 (ft)	10/1/2014	N	-	-	-	ND (0.545)	ND (0.545)	ND (0.545)	ND (0.545)	1.34	ND (0.545)	ND (0.545)	9.97	ND (0.545)	11.31
VC-334	4 - 5 (ft)	10/1/2014	N	-	-	-	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)	ND (0.0884)
VC-334	5 - 6 (ft)	10/1/2014	N	-	-	-	ND (0.0885)	ND (0.0885)	ND (0.0885)	ND (0.0885)	ND (0.0885)	ND (0.0885)	ND (0.0885)	ND (0.0885)	ND (0.0885)	ND (0.0885)
VC-335	0 - 0.5 (ft)	10/1/2014	N	-	-	-	ND (0.134)	ND (0.134)	ND (0.134)	ND (0.134)	0.289	ND (0.134)	ND (0.134)	ND (0.134)	ND (0.134)	0.289
VC-335	0.5 - 1 (ft)	10/1/2014	N	-	-	-	ND (0.121)	ND (0.121)	ND (0.121)	ND (0.121)	0.345	ND (0.121)	ND (0.121)	ND (0.121)	ND (0.121)	0.345
VC-335	1 - 2 (ft)	10/1/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.541	ND (0.118)	ND (0.118)	0.0798 J	ND (0.118)	0.621
VC-335	2 - 3 (ft)	10/1/2014	FD	-	-	-	ND (0.905)	ND (0.905)	ND (0.905)	ND (0.905)	3.64	ND (0.905)	ND (0.905)	21.4	ND (0.905)	25.04
VC-335	2 - 3 (ft)	10/1/2014	N	-	-	-	ND (1.8)	ND (1.8)	ND (1.8)	ND (1.8)	4.16	ND (1.8)	ND (1.8)	27.9	ND (1.8)	32.06
VC-335	3 - 4 (ft)	10/1/2014	N	-	-	-	ND (0.0935)	ND (0.0935)	ND (0.0935)	ND (0.0935)	ND (0.0935)	ND (0.0935)	ND (0.0935)	0.0563 J	ND (0.0935)	0.0563 J
VC-335	4 - 5 (ft)	10/1/2014	N	-	-	-	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)	ND (0.0923)
VC-335	5 - 6 (ft)	10/1/2014	N	-	-	-	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)
VC-336	0 - 0.5 (ft)	10/1/2014	N	-	-	-	ND (0.135)	ND (0.135)	ND (0.135)	ND (0.135)	0.187	ND (0.135)	ND (0.135)	0.112 J	ND (0.135)	0.299
VC-336	0.5 - 1 (ft)	10/1/2014	N	-	-	-	ND (0.121)	ND (0.121)	ND (0.121)	ND (0.121)	0.488	1.37	ND (0.121)	ND (0.121)	ND (0.121)	1.858
VC-336	1 - 2 (ft)	10/1/2014	N	-	-	-	ND (68.9)	ND (68.9)	ND (68.9)	ND (68.9)	ND (68.9)	ND (68.9)	ND (68.9)	869	ND (68.9)	869
VC-336	2 - 3 (ft)	10/1/2014	FD	-	-	-	ND (0.0914)	ND (0.0914)	ND (0.0914)	ND (0.0914)	0.357	ND (0.0914)	ND (0.0914)	0.419	ND (0.0914)	0.776
VC-336	2 - 3 (ft)	10/1/2014	N	-	-	-	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	0.104	ND (0.0943)	ND (0.0943)	0.123	ND (0.0943)	0.227
VC-336	3 - 4 (ft)	10/1/2014	N	-	-	-	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)	ND (0.0936)
VC-336	4 - 5 (ft)	10/1/2014	N	-	-	-	ND (0.0779)	ND (0.0779)	ND (0.0779)	ND (0.0779)	ND (0.0779)	ND (0.0779)	ND (0.0779)	ND (0.0779)	ND (0.0779)	ND (0.0779)
VC-336	5 - 6 (ft)	10/1/2014	N	-	-	-	ND (0.089)	ND (0.089)	ND (0.089)	ND (0.089)	ND (0.089)	ND (0.089)	ND (0.089)	ND (0.089)	ND (0.089)	ND (0.089)
VC-337	0 - 0.5 (ft)	10/20/2014	N	-	-	-	ND (10.5)	ND (10.5)	ND (10.5)	ND (10.5)	37.7	ND (10.5)	ND (10.5)	240	ND (10.5)	277.7
VC-337	0.5 - 1 (ft)	10/20/2014	N	-	-	-	ND (56.7)	ND (56.7)	ND (56.7)	ND (56.7)	ND (56.7)	ND (56.7)	ND (56.7)	1360	ND (56.7)	1360
VC-337	1 - 2 (ft)	10/20/2014	N	-	-	-	ND (0.0931)	ND (0.0931)	ND (0.0931)	ND (0.0931)	0.185	ND (0.0931)	ND (0.0931)	0.138	ND (0.0931)	0.323
VC-337	2 - 3 (ft)	10/20/2014	N	-	-	-	ND (0.0895)	ND (0.0895)	ND (0.0895)	ND (0.0895)	ND (0.0895)	ND (0.0895)	ND (0.0895)	ND (0.0895)	ND (0.0895)	ND (0.0895)

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-337	3 - 4 (ft)	10/20/2014	N	-	-	-	ND (5.08)	ND (5.08)	ND (5.08)	ND (5.08)	13.5	ND (5.08)	ND (5.08)	100	ND (5.08)	113.5
VC-337	4 - 5 (ft)	10/20/2014	N	-	-	-	ND (0.259)	ND (0.259)	ND (0.259)	ND (0.259)	0.395	ND (0.259)	ND (0.259)	3.08	ND (0.259)	3.475
VC-337	5 - 6 (ft)	10/20/2014	N	-	-	-	ND (0.0842)	ND (0.0842)	ND (0.0842)	ND (0.0842)	ND (0.0842)	ND (0.0842)	ND (0.0842)	ND (0.0842)	ND (0.0842)	ND (0.0842)
VC-338	0 - 0.5 (ft)	10/20/2014	N	-	-	-	ND (0.14)	ND (0.14)	ND (0.14)	ND (0.14)	0.394	ND (0.14)	ND (0.14)	ND (0.14)	ND (0.14)	0.394
VC-338	0.5 - 1 (ft)	10/20/2014	N	-	-	-	ND (0.0871)	ND (0.0871)	ND (0.0871)	ND (0.0871)	ND (0.0871)	ND (0.0871)	ND (0.0871)	ND (0.0871)	ND (0.0871)	ND (0.0871)
VC-338	1 - 2 (ft)	10/20/2014	N	-	-	-	ND (0.0834)	ND (0.0834)	ND (0.0834)	ND (0.0834)	ND (0.0834)	ND (0.0834)	ND (0.0834)	ND (0.0834)	ND (0.0834)	ND (0.0834)
VC-338	2 - 3 (ft)	10/20/2014	FD	-	-	-	ND (0.172)	ND (0.172)	ND (0.172)	ND (0.172)	1.02	ND (0.172)	ND (0.172)	1.98	ND (0.172)	3
VC-338	2 - 3 (ft)	10/20/2014	N	-	-	-	ND (0.442)	ND (0.442)	ND (0.442)	ND (0.442)	2.21	ND (0.442)	ND (0.442)	7.67	ND (0.442)	9.88
VC-338	3 - 4 (ft)	10/20/2014	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.396	ND (0.11)	ND (0.11)	0.238	ND (0.11)	0.634
VC-338	4 - 5 (ft)	10/20/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.168	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.168
VC-338	5 - 6 (ft)	10/20/2014	N	-	-	-	ND (0.0772)	ND (0.0772)	ND (0.0772)	ND (0.0772)	ND (0.0772)	ND (0.0772)	ND (0.0772)	ND (0.0772)	ND (0.0772)	ND (0.0772)
VC-338	6 - 8 (ft)	10/20/2014	N	-	-	-	ND (25.7)	ND (25.7)	ND (25.7)	ND (25.7)	64.3	ND (25.7)	ND (25.7)	633	ND (25.7)	697.3
VC-339	2 - 3 (ft)	10/2/2014	N	-	-	-	ND (4.29)	ND (4.29)	ND (4.29)	ND (4.29)	4.99	ND (4.29)	ND (4.29)	70.1	ND (4.29)	75.09
VC-339	3 - 4 (ft)	10/2/2014	N	-	-	-	ND (0.0968)	ND (0.0968)	ND (0.0968)	ND (0.0968)	ND (0.0968)	ND (0.0968)	ND (0.0968)	0.415	ND (0.0968)	0.415
VC-339	4 - 5 (ft)	10/2/2014	FD	-	-	-	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)
VC-339	4 - 5 (ft)	10/2/2014	N	-	-	-	ND (0.0916)	ND (0.0916)	ND (0.0916)	ND (0.0916)	ND (0.0916)	ND (0.0916)	ND (0.0916)	ND (0.0916)	ND (0.0916)	ND (0.0916)
VC-339	5 - 6 (ft)	10/2/2014	N	-	-	-	ND (0.0765)	ND (0.0765)	ND (0.0765)	ND (0.0765)	ND (0.0765)	ND (0.0765)	ND (0.0765)	ND (0.0765)	ND (0.0765)	ND (0.0765)
VC-340	4 - 5 (ft)	10/2/2014	FD	-	-	-	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)
VC-340	4 - 5 (ft)	10/2/2014	N	-	-	-	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)	ND (0.0922)
VC-340	5 - 6 (ft)	10/2/2014	N	-	-	-	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)
VC-341	0 - 0.5 (ft)	10/2/2014	N	-	-	-	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	6.49	ND (1.09)	ND (1.09)	26.3	ND (1.09)	32.79
VC-341	0.5 - 1 (ft)	10/2/2014	N	-	-	-	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	0.413	ND (0.129)	ND (0.129)	ND (0.129)	ND (0.129)	0.413
VC-341	1 - 2 (ft)	10/2/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.279	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.279
VC-341	2 - 3 (ft)	10/2/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.644	ND (0.116)	ND (0.116)	0.149	ND (0.116)	0.793
VC-341	3 - 4 (ft)	10/2/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.633	ND (0.111)	ND (0.111)	0.0929 J	ND (0.111)	0.726
VC-341	4 - 5 (ft)	10/2/2014	N	-	-	-	ND (2.01)	ND (2.01)	ND (2.01)	ND (2.01)	8.1	ND (2.01)	ND (2.01)	32.4	ND (2.01)	40.5
VC-341	5 - 6 (ft)	10/2/2014	N	-	-	-	ND (1.88)	ND (1.88)	ND (1.88)	ND (1.88)	7.85	ND (1.88)	ND (1.88)	47.3	ND (1.88)	55.15
VC-342	0 - 0.5 (ft)	10/20/2014	N	-	-	-	ND (0.512)	ND (0.512)	ND (0.512)	ND (0.512)	2.05	ND (0.512)	ND (0.512)	7.58	ND (0.512)	9.63
VC-342	0.5 - 1 (ft)	10/20/2014	N	-	-	-	ND (0.0995)	ND (0.0995)	ND (0.0995)	ND (0.0995)	2.58	ND (0.0995)	ND (0.0995)	3.65	ND (0.0995)	6.23
VC-342	1 - 2 (ft)	10/20/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.622	ND (0.109)	ND (0.109)	0.405	ND (0.109)	1.027
VC-342	2 - 3 (ft)	10/20/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.374	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.374
VC-342	3 - 4 (ft)	10/20/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.271	ND (0.109)	ND (0.109)	0.0696 J	ND (0.109)	0.3406
VC-342	4 - 5 (ft)	10/20/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.328	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.328
VC-342	5 - 6 (ft)	10/20/2014	FD	-	-	-	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)
VC-342	5 - 6 (ft)	10/20/2014	N	-	-	-	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)
VC-342	6 - 8 (ft)	10/20/2014	N	-	-	-	ND (2.57)	ND (2.57)	ND (2.57)	ND (2.57)	16.5	ND (2.57)	ND (2.57)	49.7	ND (2.57)	66.2
VC-343	0 - 0.5 (ft)	10/1/2014	N	-	-	-	ND (1.32)	ND (1.32)	ND (1.32)	ND (1.32)	6.27	ND (1.32)	ND (1.32)	17.9	ND (1.32)	24.17
VC-343	0.5 - 1 (ft)	10/1/2014	N	-	-	-	ND (0.135)	ND (0.135)	ND (0.135)	ND (0.135)	0.315	ND (0.135)	ND (0.135)	ND (0.135)	ND (0.135)	0.315
VC-343	1 - 2 (ft)	10/1/2014	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.372	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.372
VC-343	2 - 3 (ft)	10/1/2014	N	-	-	-	ND (0.0905)	ND (0.0905)	ND (0.0905)	ND (0.0905)	0.684	ND (0.0905)	ND (0.0905)	0.257	ND (0.0905)	0.941
VC-343	3 - 4 (ft)	10/1/2014	N	-	-	-	ND (0.282)	ND (0.282)	ND (0.282)	ND (0.282)	1.4	ND (0.282)	ND (0.282)	2.21	ND (0.282)	3.61

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-343	4 - 5 (ft)	10/1/2014	N	-	-	-	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)
VC-343	5 - 6 (ft)	10/1/2014	N	-	-	-	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)
VC-344	0 - 0.5 (ft)	10/1/2014	N	-	-	-	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	0.164	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	0.164
VC-344	0.5 - 1 (ft)	10/1/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.333	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.333
VC-344	1 - 2 (ft)	10/1/2014	N	-	-	-	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	0.584	ND (0.122)	ND (0.122)	0.456	ND (0.122)	1.04
VC-344	2 - 3 (ft)	10/1/2014	N	-	-	-	ND (0.0968)	ND (0.0968)	ND (0.0968)	ND (0.0968)	1.03	ND (0.0968)	ND (0.0968)	3.09	ND (0.0968)	4.12
VC-344	3 - 4 (ft)	10/1/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	3.11	ND (0.109)	ND (0.109)	2.98	ND (0.109)	6.09
VC-344	4 - 5 (ft)	10/1/2014	N	-	-	-	ND (4.38)	ND (4.38)	ND (4.38)	ND (4.38)	18.9	ND (4.38)	ND (4.38)	82.1	ND (4.38)	101
VC-345	0 - 0.5 (ft)	10/20/2014	N	-	-	-	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.423	ND (0.127)	ND (0.127)	0.367	ND (0.127)	0.79
VC-345	0.5 - 1 (ft)	10/20/2014	N	-	-	-	ND (0.5)	ND (0.5)	ND (0.5)	ND (0.5)	1.11	ND (0.5)	ND (0.5)	8.01	ND (0.5)	9.12
VC-345	1 - 2 (ft)	10/20/2014	N	-	-	-	ND (9.04)	ND (9.04)	ND (9.04)	ND (9.04)	57.4	ND (9.04)	ND (9.04)	158	ND (9.04)	215.4
VC-345	2 - 3 (ft)	10/20/2014	N	-	-	-	ND (1.09)	ND (1.09)	ND (1.09)	ND (1.09)	5.74	ND (1.09)	ND (1.09)	13.8	ND (1.09)	19.54
VC-345	3 - 4 (ft)	10/20/2014	FD	-	-	-	ND (1.15)	ND (1.15)	ND (1.15)	ND (1.15)	4.81	ND (1.15)	ND (1.15)	14.4	ND (1.15)	19.21
VC-345	3 - 4 (ft)	10/20/2014	N	-	-	-	ND (1.14)	ND (1.14)	ND (1.14)	ND (1.14)	5.25	ND (1.14)	ND (1.14)	12.3	ND (1.14)	17.55
VC-345	4 - 5 (ft)	10/20/2014	N	-	-	-	ND (0.68)	ND (0.68)	ND (0.68)	ND (0.68)	2.79	ND (0.68)	ND (0.68)	8.53	ND (0.68)	11.32
VC-346	0 - 0.5 (ft)	10/2/2014	N	-	-	-	ND (0.624)	ND (0.624)	ND (0.624)	ND (0.624)	3.07	ND (0.624)	ND (0.624)	11.1	ND (0.624)	14.17
VC-346	0.5 - 1 (ft)	10/2/2014	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.617	ND (0.11)	ND (0.11)	0.356	ND (0.11)	0.973
VC-346	1 - 2 (ft)	10/2/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.656	ND (0.118)	ND (0.118)	0.265	ND (0.118)	0.921
VC-346	2 - 3 (ft)	10/2/2014	FD	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.579	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.579
VC-346	2 - 3 (ft)	10/2/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.805	ND (0.114)	ND (0.114)	0.12	ND (0.114)	0.925
VC-346	3 - 4 (ft)	10/2/2014	N	-	-	-	ND (0.404)	ND (0.404)	ND (0.404)	ND (0.404)	3.25	ND (0.404)	ND (0.404)	3.44	ND (0.404)	6.69
VC-346	4 - 5 (ft)	10/2/2014	N	-	-	-	ND (1.1)	ND (1.1)	ND (1.1)	ND (1.1)	8.13	ND (1.1)	ND (1.1)	19.1	ND (1.1)	27.23
VC-346	5 - 6 (ft)	10/2/2014	N	-	-	-	ND (215)	ND (215)	ND (215)	ND (215)	1610	ND (215)	ND (215)	6890	ND (215)	8500
VC-346	6 - 8 (ft)	10/2/2014	N	-	-	-	ND (157)	ND (157)	ND (157)	ND (157)	408	ND (157)	ND (157)	4260	1610	6278
VC-347	0 - 0.5 (ft)	10/2/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.585	ND (0.12)	ND (0.12)	0.282	ND (0.12)	0.867
VC-347	0.5 - 1 (ft)	10/2/2014	N	-	-	-	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	0.261	ND (0.106)	ND (0.106)	0.0851 J	ND (0.106)	0.3461
VC-347	1 - 2 (ft)	10/2/2014	N	-	-	-	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	0.452	ND (0.107)	ND (0.107)	0.786	ND (0.107)	1.238
VC-347	2 - 3 (ft)	10/2/2014	N	-	-	-	ND (1.01)	ND (1.01)	ND (1.01)	ND (1.01)	1.67	ND (1.01)	ND (1.01)	21	ND (1.01)	22.67
VC-347	3 - 4 (ft)	10/2/2014	N	-	-	-	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	0.489	ND (0.0964)	ND (0.0964)	0.231	ND (0.0964)	0.72
VC-347	4 - 5 (ft)	10/2/2014	N	-	-	-	ND (34.3)	ND (34.3)	ND (34.3)	ND (34.3)	107	ND (34.3)	ND (34.3)	782	317	1206
VC-347	5 - 6 (ft)	10/2/2014	FD	-	-	-	ND (0.0951)	ND (0.0951)	ND (0.0951)	ND (0.0951)	0.14	ND (0.0951)	ND (0.0951)	0.111	ND (0.0951)	0.251
VC-347	5 - 6 (ft)	10/2/2014	N	-	-	-	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	0.0769 J	ND (0.0964)	ND (0.0964)	0.0624 J	ND (0.0964)	0.1393
VC-348	0 - 0.5 (ft)	10/2/2014	N	-	-	-	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.261	ND (0.127)	ND (0.127)	0.0807 J	ND (0.127)	0.342
VC-348	0.5 - 1 (ft)	10/2/2014	N	-	-	-	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.295	ND (0.124)	ND (0.124)	0.121 J	ND (0.124)	0.416
VC-348	1 - 2 (ft)	10/2/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.43	ND (0.12)	ND (0.12)	0.442	ND (0.12)	0.872
VC-348	2 - 3 (ft)	10/2/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.335	ND (0.12)	ND (0.12)	0.0802 J	ND (0.12)	0.4152
VC-348	3 - 4 (ft)	10/2/2014	FD	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.488	ND (0.112)	ND (0.112)	0.912	ND (0.112)	1.4
VC-348	3 - 4 (ft)	10/2/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.497	ND (0.111)	ND (0.111)	0.0827 J	ND (0.111)	0.5797
VC-349	0.5 - 1 (ft)	10/2/2014	N	-	-	-	ND (0.235)	ND (0.235)	ND (0.235)	ND (0.235)	2.06	ND (0.235)	ND (0.235)	4.53	ND (0.235)	6.59
VC-349	1 - 2 (ft)	10/2/2014	N	-	-	-	ND (0.833)	ND (0.833)	ND (0.833)	ND (0.833)	5.25	ND (0.833)	ND (0.833)	5.89	ND (0.833)	11.14
VC-349	2 - 3 (ft)	10/2/2014	N	-	-	-	ND (0.973)	ND (0.973)	ND (0.973)	ND (0.973)	6.69	ND (0.973)	ND (0.973)	10.1	4.37	21.16

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-349	3 - 4 (ft)	10/2/2014	FD	-	-	-	ND (18.3)	ND (18.3)	ND (18.3)	ND (18.3)	74.3	ND (18.3)	ND (18.3)	315	ND (18.3)	389.3
VC-349	3 - 4 (ft)	10/2/2014	N	-	-	-	ND (18.9)	ND (18.9)	ND (18.9)	ND (18.9)	69	ND (18.9)	ND (18.9)	298	ND (18.9)	367
VC-349	4 - 5 (ft)	10/2/2014	N	-	-	-	ND (0.0938)	ND (0.0938)	ND (0.0938)	ND (0.0938)	0.0965	ND (0.0938)	ND (0.0938)	0.141	ND (0.0938)	0.237
VC-350	0 - 0.5 (ft)	10/2/2014	N	-	-	-	ND (0.296)	ND (0.296)	ND (0.296)	ND (0.296)	1.38	ND (0.296)	ND (0.296)	2.75	ND (0.296)	4.13
VC-350	0.5 - 1 (ft)	10/2/2014	N	-	-	-	ND (0.332)	ND (0.332)	ND (0.332)	ND (0.332)	2.05	ND (0.332)	ND (0.332)	2.31	ND (0.332)	4.36
VC-350	1 - 2 (ft)	10/2/2014	N	-	-	-	ND (0.572)	ND (0.572)	ND (0.572)	ND (0.572)	4.49	ND (0.572)	ND (0.572)	3.06	ND (0.572)	7.55
VC-350	2 - 3 (ft)	10/2/2014	N	-	-	-	ND (1.03)	ND (1.03)	ND (1.03)	ND (1.03)	10	ND (1.03)	ND (1.03)	10.3	ND (1.03)	20.3
VC-350	3 - 4 (ft)	10/2/2014	FD	-	-	-	ND (0.626)	ND (0.626)	ND (0.626)	ND (0.626)	5.53	ND (0.626)	ND (0.626)	5.91	ND (0.626)	11.44
VC-350	3 - 4 (ft)	10/2/2014	N	-	-	-	ND (0.737)	ND (0.737)	ND (0.737)	ND (0.737)	6.38	ND (0.737)	ND (0.737)	17.6	ND (0.737)	23.98
VC-351	0 - 0.5 (ft)	10/1/2014	N	-	-	-	ND (0.139)	ND (0.139)	ND (0.139)	ND (0.139)	0.277	ND (0.139)	ND (0.139)	ND (0.139)	ND (0.139)	0.277
VC-351	0.5 - 1 (ft)	10/1/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.236	ND (0.101)	ND (0.101)	0.136	ND (0.101)	0.372
VC-351	1 - 2 (ft)	10/1/2014	N	-	-	-	ND (0.527)	ND (0.527)	ND (0.527)	ND (0.527)	0.897	ND (0.527)	ND (0.527)	7.04	ND (0.527)	7.937
VC-352	0 - 0.5 (ft)	10/1/2014	N	-	-	-	ND (0.14)	ND (0.14)	ND (0.14)	ND (0.14)	0.245	ND (0.14)	ND (0.14)	ND (0.14)	ND (0.14)	0.245
VC-352	0.5 - 1 (ft)	10/1/2014	N	-	-	-	ND (0.143)	ND (0.143)	ND (0.143)	ND (0.143)	0.247	ND (0.143)	ND (0.143)	ND (0.143)	ND (0.143)	0.247
VC-352	1 - 2 (ft)	10/1/2014	FD	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.0596 J	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.0596 J
VC-352	1 - 2 (ft)	10/1/2014	N	-	-	-	ND (0.0931)	ND (0.0931)	ND (0.0931)	ND (0.0931)	0.119	ND (0.0931)	ND (0.0931)	1.04	ND (0.0931)	1.159
VC-353	0 - 0.5 (ft)	10/1/2014	N	-	-	-	ND (0.138)	ND (0.138)	ND (0.138)	ND (0.138)	0.317	ND (0.138)	ND (0.138)	ND (0.138)	ND (0.138)	0.317
VC-353	0.5 - 1 (ft)	10/1/2014	FD	-	-	-	ND (0.136)	ND (0.136)	ND (0.136)	ND (0.136)	0.291	ND (0.136)	ND (0.136)	ND (0.136)	ND (0.136)	0.291
VC-353	0.5 - 1 (ft)	10/1/2014	N	-	-	-	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.307	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.307
VC-353	1 - 2 (ft)	10/1/2014	FD	-	-	-	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.273	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.273
VC-353	1 - 2 (ft)	10/1/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.252	ND (0.119)	ND (0.119)	0.878	ND (0.119)	1.13
VC-354	0 - 0.5 (ft)	10/1/2014	N	-	-	-	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.292	ND (0.132)	ND (0.132)	ND (0.132)	ND (0.132)	0.292
VC-354	0.5 - 1 (ft)	10/1/2014	FD	-	-	-	ND (0.121)	ND (0.121)	ND (0.121)	ND (0.121)	0.35	ND (0.121)	ND (0.121)	0.214	ND (0.121)	0.564
VC-354	0.5 - 1 (ft)	10/1/2014	N	-	-	-	ND (0.128)	ND (0.128)	ND (0.128)	ND (0.128)	0.258	ND (0.128)	ND (0.128)	0.451	ND (0.128)	0.709
VC-354	1 - 2 (ft)	10/1/2014	N	-	-	-	ND (0.0874)	ND (0.0874)	ND (0.0874)	ND (0.0874)	0.286	ND (0.0874)	ND (0.0874)	0.537	ND (0.0874)	0.823
VC-355	0 - 0.5 (ft)	10/21/2014	FD	-	-	-	ND (0.23)	ND (0.23)	ND (0.23)	ND (0.23)	0.552	ND (0.23)	ND (0.23)	2.2	ND (0.23)	2.752
VC-355	0 - 0.5 (ft)	10/21/2014	N	-	-	-	ND (0.419)	ND (0.419)	ND (0.419)	ND (0.419)	0.428	ND (0.419)	ND (0.419)	3.71	ND (0.419)	4.138
VC-355	0.5 - 1 (ft)	10/21/2014	N	-	-	-	ND (0.272)	ND (0.272)	ND (0.272)	ND (0.272)	1.2	ND (0.272)	ND (0.272)	3.09	ND (0.272)	4.29
VC-355	1 - 2 (ft)	10/21/2014	N	-	-	-	ND (1.82)	ND (1.82)	ND (1.82)	ND (1.82)	12.8	ND (1.82)	ND (1.82)	14.5	ND (1.82)	27.3
VC-355	2 - 3 (ft)	10/21/2014	N	-	-	-	ND (18.4)	ND (18.4)	ND (18.4)	ND (18.4)	89.3	ND (18.4)	ND (18.4)	336	166	591.3
VC-355	3 - 4 (ft)	10/21/2014	N	-	-	-	ND (7.69)	ND (7.69)	ND (7.69)	ND (7.69)	60.1	ND (7.69)	ND (7.69)	82.9	ND (7.69)	143
VC-355	4 - 5 (ft)	10/21/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.595	ND (0.111)	ND (0.111)	0.506	ND (0.111)	1.101
VC-356	0 - 0.5 (ft)	10/22/2014	N	-	-	-	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	0.275	ND (0.122)	ND (0.122)	0.153	ND (0.122)	0.428
VC-356	0.5 - 1 (ft)	10/22/2014	N	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.343	ND (0.102)	ND (0.102)	0.729	ND (0.102)	1.072
VC-356	1 - 2 (ft)	10/22/2014	FD	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.351	ND (0.105)	ND (0.105)	0.541	ND (0.105)	0.892
VC-356	1 - 2 (ft)	10/22/2014	N	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.41	ND (0.105)	ND (0.105)	0.565	ND (0.105)	0.975
VC-356	2 - 3 (ft)	10/22/2014	N	-	-	-	ND (0.876)	ND (0.876)	ND (0.876)	ND (0.876)	5.9	ND (0.876)	ND (0.876)	3.18	ND (0.876)	9.08
VC-356	3 - 4 (ft)	10/22/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.0837 J	ND (0.101)	ND (0.101)	0.0897 J	ND (0.101)	0.1734
VC-357	0 - 0.5 (ft)	10/24/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.259	ND (0.12)	ND (0.12)	0.0996 J	ND (0.12)	0.3586
VC-357	0.5 - 1 (ft)	10/24/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.218	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.218
VC-357	1 - 2 (ft)	10/24/2014	N	-	-	-	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.29	ND (0.113)	ND (0.113)	1.35	ND (0.113)	1.64

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-358	0 - 0.5 (ft)	10/24/2014	N	-	-	-	ND (0.131)	ND (0.131)	ND (0.131)	ND (0.131)	0.219	ND (0.131)	ND (0.131)	0.0861 J	ND (0.131)	0.3051
VC-358	0.5 - 1 (ft)	10/24/2014	N	-	-	-	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.235	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.235
VC-358	1 - 2 (ft)	10/24/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.304	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.304
VC-358	4 - 5 (ft)	10/24/2014	N	-	-	-	ND (2.96)	ND (2.96)	ND (2.96)	ND (2.96)	3.61	ND (2.96)	ND (2.96)	33.5	ND (2.96)	37.11
VC-359	0 - 0.5 (ft)	10/28/2014	N	-	-	-	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	0.272	ND (0.261)	ND (0.261)	ND (0.261)	ND (0.261)	0.272
VC-359	0.5 - 1 (ft)	10/28/2014	N	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.371	ND (0.104)	ND (0.104)	1.18	ND (0.104)	1.551
VC-359	1 - 2 (ft)	10/28/2014	N	-	-	-	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	2.01	ND (0.103)	ND (0.103)	0.917	ND (0.103)	2.927
VC-359	2 - 3 (ft)	10/28/2014	N	-	-	-	ND (3.49)	ND (3.49)	ND (3.49)	ND (3.49)	4.44	ND (3.49)	ND (3.49)	78.2	ND (3.49)	82.64
VC-359	3 - 4 (ft)	10/28/2014	N	-	-	-	ND (1.02)	ND (1.02)	ND (1.02)	ND (1.02)	7.91	ND (1.02)	ND (1.02)	7.64	ND (1.02)	15.55
VC-360	0 - 0.5 (ft)	10/28/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.294	ND (0.112)	ND (0.112)	0.97	ND (0.112)	1.264
VC-360	0.5 - 1 (ft)	10/28/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.5	ND (0.116)	ND (0.116)	0.427	ND (0.116)	0.927
VC-360	1 - 2 (ft)	10/28/2014	N	-	-	-	ND (0.983)	ND (0.983)	ND (0.983)	ND (0.983)	3.16	ND (0.983)	ND (0.983)	12	ND (0.983)	15.16
VC-360	2 - 3 (ft)	10/28/2014	N	-	-	-	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.429	ND (0.102)	ND (0.102)	0.0787 J	ND (0.102)	0.5077
VC-360	3 - 4 (ft)	10/28/2014	FD	-	-	-	ND (0.0999)	ND (0.0999)	ND (0.0999)	ND (0.0999)	0.401	ND (0.0999)	ND (0.0999)	0.114	ND (0.0999)	0.515
VC-360	3 - 4 (ft)	10/28/2014	N	-	-	-	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)	ND (0.0879)
VC-361	0 - 0.5 (ft)	10/28/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.274	ND (0.118)	ND (0.118)	0.234	ND (0.118)	0.508
VC-361	0.5 - 1 (ft)	10/28/2014	N	-	-	-	ND (0.0938)	ND (0.0938)	ND (0.0938)	ND (0.0938)	0.0675 J	ND (0.0938)	ND (0.0938)	0.148	ND (0.0938)	0.2155
VC-361	1 - 2 (ft)	10/28/2014	N	-	-	-	ND (43)	ND (43)	ND (43)	ND (43)	90.3	ND (43)	ND (43)	1080	ND (43)	1170.3
VC-361	2 - 3 (ft)	10/28/2014	N	-	-	-	ND (0.363)	ND (0.363)	ND (0.363)	ND (0.363)	0.415	ND (0.363)	ND (0.363)	2.88	ND (0.363)	3.295
VC-362	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.805	ND (0.118)	ND (0.118)	0.922	ND (0.118)	1.727
VC-362	0.5 - 1 (ft)	10/29/2014	N	-	-	-	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.0795 J	ND (0.127)	ND (0.127)	ND (0.127)	0.0795 J
VC-362	1 - 2 (ft)	10/29/2014	N	-	-	-	ND (0.494)	ND (0.494)	ND (0.494)	ND (0.494)	1	ND (0.494)	ND (0.494)	3.31	ND (0.494)	4.31
VC-362	2 - 3 (ft)	10/29/2014	N	-	-	-	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.306	ND (0.11)	ND (0.11)	0.117	ND (0.11)	0.423
VC-362	3 - 4 (ft)	10/29/2014	N	-	-	-	ND (0.0998)	ND (0.0998)	ND (0.0998)	ND (0.0998)	0.344	ND (0.0998)	ND (0.0998)	0.206	ND (0.0998)	0.55
VC-362	4 - 5 (ft)	10/29/2014	N	-	-	-	ND (0.108)	ND (0.108)	ND (0.108)	0.721	ND (0.108)	0.232	ND (0.108)	ND (0.108)	ND (0.108)	0.953
VC-362	5 - 6 (ft)	10/29/2014	N	-	-	-	ND (0.0963)	ND (0.0963)	ND (0.0963)	ND (0.0963)	0.39	ND (0.0963)	ND (0.0963)	0.0827 J	ND (0.0963)	0.4727
VC-363	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.655	ND (0.123)	ND (0.123)	1.62	0.921	3.196
VC-363	0.5 - 1 (ft)	10/29/2014	N	-	-	-	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.275	ND (0.105)	ND (0.105)	0.703	ND (0.105)	0.978
VC-363	1 - 2 (ft)	10/29/2014	N	-	-	-	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.557	ND (0.109)	ND (0.109)	0.19	ND (0.109)	0.747
VC-363	2 - 3 (ft)	10/29/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.559	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.559
VC-363	3 - 4 (ft)	10/29/2014	FD	-	-	-	ND (0.947)	ND (0.947)	ND (0.947)	ND (0.947)	6.95	ND (0.947)	ND (0.947)	12.6	6.61	26.16
VC-363	3 - 4 (ft)	10/29/2014	N	-	-	-	ND (0.666)	ND (0.666)	ND (0.666)	ND (0.666)	5.32	ND (0.666)	ND (0.666)	5.54	ND (0.666)	10.86
VC-363	4 - 5 (ft)	10/29/2014	N	-	-	-	ND (6.03)	ND (6.03)	ND (6.03)	ND (6.03)	27.7	ND (6.03)	ND (6.03)	113	57.7	198.4
VC-363	5 - 6 (ft)	10/29/2014	N	-	-	-	ND (0.0918)	ND (0.0918)	ND (0.0918)	ND (0.0918)	0.0749 J	ND (0.0918)	ND (0.0918)	0.131	ND (0.0918)	0.2059
VC-364	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.12)	ND (0.12)	ND (0.12)	0.336	ND (0.12)	0.108 J	ND (0.12)	ND (0.12)	ND (0.12)	0.444
VC-364	0.5 - 1 (ft)	10/29/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.0719 J	ND (0.119)	ND (0.119)	ND (0.119)	0.0719 J
VC-364	1 - 2 (ft)	10/29/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	0.417	ND (0.114)	0.118	ND (0.114)	ND (0.114)	ND (0.114)	0.535
VC-364	2 - 3 (ft)	10/29/2014	N	-	-	-	ND (0.117)	ND (0.117)	ND (0.117)	0.518	ND (0.117)	0.216	ND (0.117)	ND (0.117)	ND (0.117)	0.734
VC-364	3 - 4 (ft)	10/29/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.444	ND (0.111)	ND (0.111)	0.125	ND (0.111)	0.569
VC-364	4 - 5 (ft)	10/29/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.85	ND (0.112)	ND (0.112)	0.591	ND (0.112)	1.441
VC-364	5 - 6 (ft)	10/29/2014	N	-	-	-	ND (0.197)	ND (0.197)	ND (0.197)	ND (0.197)	2.17	ND (0.197)	ND (0.197)	1.33	ND (0.197)	3.5

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-365	2 - 3 (ft)	10/28/2014	N	-	-	-	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)
VC-367	0 - 0.5 (ft)	10/29/2014	N	-	-	-	ND (0.133)	ND (0.133)	ND (0.133)	ND (0.133)	0.254	ND (0.133)	ND (0.133)	0.104 J	ND (0.133)	0.358
VC-367	0.5 - 1 (ft)	10/29/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.425	ND (0.116)	ND (0.116)	0.54	ND (0.116)	0.965
VC-367	1 - 2 (ft)	10/29/2014	N	-	-	-	ND (1.83)	ND (1.83)	ND (1.83)	ND (1.83)	6.22	ND (1.83)	ND (1.83)	18	ND (1.83)	24.22
VC-367	2 - 3 (ft)	10/29/2014	N	-	-	-	ND (1.62)	ND (1.62)	ND (1.62)	ND (1.62)	7.88	ND (1.62)	ND (1.62)	19.2	ND (1.62)	27.08
VC-367	3 - 4 (ft)	10/29/2014	FD	-	-	-	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.0921 J	ND (0.104)	0.0921 J
VC-367	3 - 4 (ft)	10/29/2014	N	-	-	-	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.0842 J	ND (0.101)	0.0842 J
VC-368	0 - 0.5 (ft)	10/31/2014	N	-	-	-	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.455	ND (0.116)	ND (0.116)	0.599	ND (0.116)	1.054
VC-368	0.5 - 1 (ft)	11/3/2014	N	-	-	-	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.49	ND (0.111)	ND (0.111)	0.207	ND (0.111)	0.697
VC-368	1 - 2 (ft)	11/3/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.444	ND (0.114)	ND (0.114)	0.192	ND (0.114)	0.636
VC-368	2 - 3 (ft)	11/3/2014	FD	-	-	-	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	0.381	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	0.381
VC-368	2 - 3 (ft)	11/3/2014	N	-	-	-	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	0.318	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	0.318
VC-368	3 - 4 (ft)	11/3/2014	N	-	-	-	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	3.03	ND (0.106)	ND (0.106)	0.241	ND (0.106)	3.271
VC-370	0 - 0.5 (ft)	10/31/2014	N	-	-	-	ND (0.123)	ND (0.123)	ND (0.123)	ND (0.123)	0.277	ND (0.123)	ND (0.123)	0.114 J	ND (0.123)	0.391
VC-370	0.5 - 1 (ft)	11/3/2014	N	-	-	-	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.207	ND (0.124)	ND (0.124)	ND (0.124)	ND (0.124)	0.207
VC-370	1 - 2 (ft)	11/3/2014	N	-	-	-	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.53	ND (0.115)	ND (0.115)	ND (0.115)	ND (0.115)	0.53
VC-370	2 - 3 (ft)	11/3/2014	N	-	-	-	ND (0.119)	ND (0.119)	ND (0.119)	ND (0.119)	0.597	ND (0.119)	ND (0.119)	0.182	ND (0.119)	0.779
VC-370	3 - 4 (ft)	11/3/2014	N	-	-	-	ND (1.08)	ND (1.08)	ND (1.08)	ND (1.08)	14.9	ND (1.08)	ND (1.08)	27.2	15.7	57.8
VC-370	4 - 5 (ft)	11/3/2014	FD	-	-	-	ND (1.04)	ND (1.04)	ND (1.04)	ND (1.04)	7.54	ND (1.04)	ND (1.04)	14.4	ND (1.04)	21.94
VC-370	4 - 5 (ft)	11/3/2014	N	-	-	-	ND (4.5)	ND (4.5)	ND (4.5)	ND (4.5)	12	ND (4.5)	ND (4.5)	80.7	ND (4.5)	92.7
VC-372	3 - 4 (ft)	11/4/2014	FD	-	-	-	ND (0.0952)	ND (0.0952)	ND (0.0952)	ND (0.0952)	0.302	ND (0.0952)	ND (0.0952)	1.03	ND (0.0952)	1.332
VC-372	3 - 4 (ft)	11/4/2014	N	-	-	-	ND (1.86)	ND (1.86)	ND (1.86)	ND (1.86)	ND (1.86)	ND (1.86)	ND (1.86)	34.6	ND (1.86)	34.6
VC-373	0 - 0.5 (ft)	11/4/2014	N	-	-	-	ND (0.143)	ND (0.143)	ND (0.143)	ND (0.143)	0.339	ND (0.143)	ND (0.143)	ND (0.143)	ND (0.143)	0.339
VC-373	0.5 - 1 (ft)	11/4/2014	N	-	-	-	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)
VC-373	1 - 2 (ft)	11/4/2014	N	-	-	-	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)	ND (0.0943)
VC-373	2 - 3 (ft)	11/4/2014	N	-	-	-	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)
VC-373	3 - 4 (ft)	11/4/2014	FD	-	-	-	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)
VC-373	3 - 4 (ft)	11/4/2014	N	-	-	-	ND (0.0949)	ND (0.0949)	ND (0.0949)	ND (0.0949)	ND (0.0949)	ND (0.0949)	ND (0.0949)	ND (0.0949)	ND (0.0949)	ND (0.0949)
VC-375	0 - 0.5 (ft)	10/31/2014	N	-	-	-	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.276	ND (0.114)	ND (0.114)	0.115	ND (0.114)	0.391
VC-375	0.5 - 1 (ft)	11/4/2014	N	-	-	-	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	0.34	ND (0.106)	ND (0.106)	0.165	ND (0.106)	0.505
VC-375	1 - 2 (ft)	11/4/2014	N	-	-	-	ND (0.386)	ND (0.386)	ND (0.386)	ND (0.386)	2.51	ND (0.386)	ND (0.386)	1.73	ND (0.386)	4.24
VC-375	2 - 3 (ft)	11/4/2014	FD	-	-	-	ND (0.254)	ND (0.254)	ND (0.254)	ND (0.254)	2.41	ND (0.254)	ND (0.254)	1.69	ND (0.254)	4.1
VC-375	2 - 3 (ft)	11/4/2014	N	-	-	-	ND (0.592)	ND (0.592)	ND (0.592)	ND (0.592)	3.29	ND (0.592)	ND (0.592)	5.09	ND (0.592)	8.38
VC-375	3 - 4 (ft)	11/4/2014	N	-	-	-	ND (0.517)	ND (0.517)	ND (0.517)	ND (0.517)	2.71	ND (0.517)	ND (0.517)	2.09	ND (0.517)	4.8
VC-401	0 - 0.5 (ft)	8/28/2014	FD	82.1	55.4	146 B	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.442	ND (0.113)	ND (0.113)	1	ND (0.113)	1.442
VC-401	0 - 0.5 (ft)	8/28/2014	N	63.1	48.4	130 B	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.307	ND (0.114)	ND (0.114)	1.08	ND (0.114)	1.387
VC-401	0.5 - 1 (ft)	8/28/2014	N	108	110	163 B	ND (0.175)	ND (0.175)	ND (0.175)	ND (0.175)	1.15	ND (0.175)	ND (0.175)	2.14	ND (0.175)	3.29
VC-401	1 - 2 (ft)	8/28/2014	N	200	125	192 B	ND (0.345)	ND (0.345)	ND (0.345)	ND (0.345)	3.53	ND (0.345)	ND (0.345)	1.41	ND (0.345)	4.94
VC-401	2 - 3 (ft)	8/28/2014	N	343	160	208 B	ND (0.444)	ND (0.444)	ND (0.444)	ND (0.444)	3.73	ND (0.444)	ND (0.444)	1.46	ND (0.444)	5.19
VC-401	3 - 4 (ft)	8/28/2014	N	394	150	198 B	ND (0.416)	ND (0.416)	ND (0.416)	ND (0.416)	4.56	ND (0.416)	ND (0.416)	3.94	ND (0.416)	8.5
VC-401	4 - 5 (ft)	8/28/2014	N	329	132	198 B	ND (0.481)	ND (0.481)	ND (0.481)	ND (0.481)	4.24	ND (0.481)	ND (0.481)	3.92	ND (0.481)	8.16

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AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-401	5 - 6 (ft)	8/28/2014	N	371	168	247 B	ND (0.492)	ND (0.492)	ND (0.492)	ND (0.492)	3.7	ND (0.492)	ND (0.492)	3.56	ND (0.492)	7.26
VC-401	6 - 8 (ft)	8/28/2014	N	364	173	299 B	ND (0.249)	ND (0.249)	ND (0.249)	ND (0.249)	2.56	ND (0.249)	ND (0.249)	1.77	ND (0.249)	4.33
VC-402	0 - 0.5 (ft)	8/29/2014	FD	66.3	42.8	109	ND (0.0951)	ND (0.0951)	ND (0.0951)	ND (0.0951)	0.286	ND (0.0951)	ND (0.0951)	1.19	ND (0.0951)	1.476
VC-402	0 - 0.5 (ft)	8/29/2014	N	212	40.5	109	ND (0.0938)	ND (0.0938)	ND (0.0938)	ND (0.0938)	0.305	ND (0.0938)	ND (0.0938)	0.378	ND (0.0938)	0.683
VC-402	0.5 - 1 (ft)	8/29/2014	N	88.8	129	143	ND (0.0784)	ND (0.0784)	ND (0.0784)	ND (0.0784)	0.756	ND (0.0784)	ND (0.0784)	0.406	ND (0.0784)	1.162
VC-402	1 - 2 (ft)	8/29/2014	N	140	105	144	ND (0.0821)	ND (0.0821)	ND (0.0821)	ND (0.0821)	2.07	ND (0.0821)	ND (0.0821)	0.678	ND (0.0821)	2.748
VC-402	2 - 3 (ft)	8/29/2014	N	236	130	207	ND (0.0907)	ND (0.0907)	ND (0.0907)	ND (0.0907)	2.67	ND (0.0907)	ND (0.0907)	2.28	ND (0.0907)	4.95
VC-402	3 - 4 (ft)	8/29/2014	N	368	142	209	ND (0.173)	ND (0.173)	ND (0.173)	ND (0.173)	2.75	ND (0.173)	ND (0.173)	0.768	ND (0.173)	3.518
VC-402	4 - 5 (ft)	8/29/2014	N	347	121	190	ND (0.0835)	ND (0.0835)	ND (0.0835)	ND (0.0835)	3.1	ND (0.0835)	ND (0.0835)	1.96	ND (0.0835)	5.06
VC-402	5 - 6 (ft)	8/29/2014	N	354	110	187	ND (0.451)	ND (0.451)	ND (0.451)	ND (0.451)	4.12	ND (0.451)	ND (0.451)	1.09	ND (0.451)	5.21
VC-402	6 - 8 (ft)	8/29/2014	N	416	169	468	ND (0.331)	ND (0.331)	ND (0.331)	ND (0.331)	1.51	ND (0.331)	ND (0.331)	1.27	ND (0.331)	2.78
VC-403	0 - 0.5 (ft)	8/29/2014	N	60.9	62	129	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.111	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.111 J
VC-403	0.5 - 1 (ft)	8/29/2014	N	75.3	59.8	132	ND (0.0986)	ND (0.0986)	ND (0.0986)	ND (0.0986)	0.262	ND (0.0986)	ND (0.0986)	0.0978 J	ND (0.0986)	0.3598
VC-403	1 - 2 (ft)	8/29/2014	N	86.3	88.1	141	ND (0.0862)	ND (0.0862)	ND (0.0862)	ND (0.0862)	0.515	ND (0.0862)	ND (0.0862)	1.41	ND (0.0862)	1.925
VC-403	2 - 3 (ft)	8/29/2014	N	128	120	189	ND (0.0891)	ND (0.0891)	ND (0.0891)	ND (0.0891)	1.95	ND (0.0891)	ND (0.0891)	0.447	ND (0.0891)	2.397
VC-403	3 - 4 (ft)	8/29/2014	N	222	151	235	ND (0.278)	ND (0.278)	ND (0.278)	ND (0.278)	3.42	ND (0.278)	ND (0.278)	1.38	ND (0.278)	4.8
VC-403	4 - 5 (ft)	8/29/2014	FD	225	153	251	ND (0.285)	ND (0.285)	ND (0.285)	ND (0.285)	2.86	ND (0.285)	ND (0.285)	0.326	ND (0.285)	3.186
VC-403	4 - 5 (ft)	8/29/2014	N	274	155	257	ND (0.464)	ND (0.464)	ND (0.464)	ND (0.464)	5.73	ND (0.464)	ND (0.464)	1.58	ND (0.464)	7.31
VC-403	5 - 6 (ft)	8/29/2014	N	322	180	290	ND (0.0864)	ND (0.0864)	ND (0.0864)	ND (0.0864)	0.876	ND (0.0864)	ND (0.0864)	0.673	ND (0.0864)	1.549
VC-403	6 - 8 (ft)	8/29/2014	N	430	153	294	ND (0.0853)	ND (0.0853)	ND (0.0853)	ND (0.0853)	0.779	ND (0.0853)	ND (0.0853)	0.706	ND (0.0853)	1.485
VC-404	0 - 0.5 (ft)	8/29/2014	N	64	57.8	136	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.587	ND (0.11)	ND (0.11)	1.12	0.501	2.208
VC-404	0.5 - 1 (ft)	8/29/2014	N	58.6	52.6	121	ND (0.0912)	ND (0.0912)	ND (0.0912)	ND (0.0912)	0.335	ND (0.0912)	ND (0.0912)	0.342	ND (0.0912)	0.677
VC-404	1 - 2 (ft)	8/29/2014	N	83	78.5	162	ND (0.465)	ND (0.465)	ND (0.465)	ND (0.465)	9.34	ND (0.465)	1.59	ND (0.465)	ND (0.465)	10.93
VC-404	2 - 3 (ft)	8/29/2014	FD	108	111	177	ND (0.0851)	ND (0.0851)	ND (0.0851)	ND (0.0851)	0.905	ND (0.0851)	ND (0.0851)	0.322	ND (0.0851)	1.227
VC-404	2 - 3 (ft)	8/29/2014	N	104	129	178	ND (0.0806)	ND (0.0806)	ND (0.0806)	ND (0.0806)	0.985	ND (0.0806)	ND (0.0806)	0.308	ND (0.0806)	1.293
VC-404	3 - 4 (ft)	8/29/2014	N	137	138	214	ND (0.178)	ND (0.178)	ND (0.178)	ND (0.178)	2.35	ND (0.178)	ND (0.178)	0.499	ND (0.178)	2.849
VC-404	4 - 5 (ft)	8/29/2014	N	197	152	222	ND (0.355)	ND (0.355)	ND (0.355)	ND (0.355)	4.12	ND (0.355)	ND (0.355)	0.633	ND (0.355)	4.753
VC-404	5 - 6 (ft)	8/29/2014	N	294	168	264	ND (0.554)	ND (0.554)	ND (0.554)	ND (0.554)	5.54	ND (0.554)	ND (0.554)	1.17	ND (0.554)	6.71
VC-404	6 - 8 (ft)	8/29/2014	N	348	163	284	ND (0.176)	ND (0.176)	ND (0.176)	ND (0.176)	1.11	ND (0.176)	ND (0.176)	1.97	ND (0.176)	3.08
VC-405	0 - 0.5 (ft)	8/29/2014	N	66	47.1	130	ND (0.0975)	ND (0.0975)	ND (0.0975)	ND (0.0975)	0.164	ND (0.0975)	ND (0.0975)	0.307	ND (0.0975)	0.471
VC-405	0.5 - 1 (ft)	8/29/2014	N	62.6	56	149	ND (0.0905)	ND (0.0905)	ND (0.0905)	ND (0.0905)	0.29	ND (0.0905)	ND (0.0905)	0.664	ND (0.0905)	0.954
VC-405	1 - 2 (ft)	8/29/2014	N	85	90.2	152	ND (0.463)	ND (0.463)	ND (0.463)	ND (0.463)	4.36	ND (0.463)	ND (0.463)	1.54	ND (0.463)	5.9
VC-405	2 - 3 (ft)	8/29/2014	FD	123	118	221	ND (0.27)	ND (0.27)	ND (0.27)	ND (0.27)	2.16	ND (0.27)	ND (0.27)	0.452	ND (0.27)	2.612
VC-405	2 - 3 (ft)	8/29/2014	N	112	134	216	ND (0.27)	ND (0.27)	ND (0.27)	ND (0.27)	2.29	ND (0.27)	ND (0.27)	0.421	ND (0.27)	2.711
VC-405	3 - 4 (ft)	8/29/2014	N	126	135	235	ND (0.539)	ND (0.539)	ND (0.539)	ND (0.539)	4.17	ND (0.539)	ND (0.539)	0.915	ND (0.539)	5.085
VC-405	4 - 5 (ft)	8/29/2014	N	150	144	225	ND (0.53)	ND (0.53)	ND (0.53)	ND (0.53)	4.41	ND (0.53)	ND (0.53)	0.993	ND (0.53)	5.403
VC-405	5 - 6 (ft)	8/29/2014	N	219	174	269	ND (0.627)	ND (0.627)	ND (0.627)	ND (0.627)	5.4	ND (0.627)	ND (0.627)	0.846	ND (0.627)	6.246
VC-405	6 - 8 (ft)	8/29/2014	N	453	169	383	ND (0.356)	ND (0.356)	ND (0.356)	ND (0.356)	0.218 J	ND (0.356)	ND (0.356)	0.624	ND (0.356)	0.842
VC-406	0 - 0.5 (ft)	9/9/2014	N	181	51.2	469	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.124	ND (0.116)	ND (0.116)	0.196	ND (0.116)	0.32
VC-406	0.5 - 1 (ft)	9/9/2014	N	1540	186	1190	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	0.132	ND (0.0863)	0.132
VC-406	1 - 2 (ft)	9/9/2014	FD	2160	175	3090	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	ND (0.0776)	0.2	ND (0.0776)	0.2

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-406	1 - 2 (ft)	9/9/2014	N	3570	184	3350	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	0.33	ND (0.081)	0.33
VC-406	2 - 3 (ft)	9/9/2014	N	9770	1510	11800	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)	ND (0.0694)
VC-406	3 - 4 (ft)	9/9/2014	N	8450	1070	15600	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)	ND (0.0621)
VC-406	4 - 5 (ft)	9/9/2014	N	6560	330	11000	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)	ND (0.0567)
VC-406	5 - 6 (ft)	9/9/2014	N	8640	254	15800	ND (0.0685)	ND (0.0685)	ND (0.0685)	ND (0.0685)	ND (0.0685)	ND (0.0685)	ND (0.0685)	ND (0.0685)	ND (0.0685)	ND (0.0685)
VC-406	6 - 8 (ft)	9/9/2014	N	5990	120	6870	ND (0.0678)	ND (0.0678)	ND (0.0678)	ND (0.0678)	ND (0.0678)	ND (0.0678)	ND (0.0678)	ND (0.0678)	ND (0.0678)	ND (0.0678)
VC-407	0 - 0.5 (ft)	9/2/2014	N	86.4	47.7	168	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.107	ND (0.101)	ND (0.101)	ND (0.101)	ND (0.101)	0.107
VC-407	0.5 - 1 (ft)	9/2/2014	N	1320	189	804	ND (0.0942)	ND (0.0942)	ND (0.0942)	ND (0.0942)	ND (0.0942)	ND (0.0942)	ND (0.0942)	ND (0.0942)	ND (0.0942)	ND (0.0942)
VC-407	1 - 2 (ft)	9/2/2014	N	3970	212	3810	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)
VC-407	2 - 3 (ft)	9/2/2014	FD	5140	344	6720	ND (0.0794)	ND (0.0794)	ND (0.0794)	ND (0.0794)	ND (0.0794)	ND (0.0794)	ND (0.0794)	ND (0.0794)	ND (0.0794)	ND (0.0794)
VC-407	2 - 3 (ft)	9/2/2014	N	6410	355	6580	ND (0.0736)	ND (0.0736)	ND (0.0736)	ND (0.0736)	ND (0.0736)	ND (0.0736)	ND (0.0736)	ND (0.0736)	ND (0.0736)	ND (0.0736)
VC-407	3 - 4 (ft)	9/2/2014	N	3570	233	6870	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)
VC-407	4 - 5 (ft)	9/2/2014	N	3240	167	5010	ND (0.0775)	ND (0.0775)	ND (0.0775)	ND (0.0775)	ND (0.0775)	ND (0.0775)	ND (0.0775)	ND (0.0775)	ND (0.0775)	ND (0.0775)
VC-407	5 - 6 (ft)	9/2/2014	N	1930	162	2670	ND (0.0797)	ND (0.0797)	ND (0.0797)	ND (0.0797)	ND (0.0797)	ND (0.0797)	ND (0.0797)	ND (0.0797)	ND (0.0797)	ND (0.0797)
VC-407	6 - 8 (ft)	9/2/2014	N	863	155	1310	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)	ND (0.0824)
VC-408	0 - 0.5 (ft)	9/2/2014	N	72.7	48.8	135	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.137	ND (0.118)	ND (0.118)	0.178	ND (0.118)	0.315
VC-408	0.5 - 1 (ft)	9/2/2014	N	553	95.4	322	ND (4.07)	ND (4.07)	ND (4.07)	ND (4.07)	31	ND (4.07)	ND (4.07)	41.9	41.3	114.2
VC-408	1 - 2 (ft)	9/2/2014	N	1340	152	757	ND (0.603)	ND (0.603)	ND (0.603)	ND (0.603)	2.57	ND (0.603)	ND (0.603)	2.9	2.01	7.48
VC-408	2 - 3 (ft)	9/2/2014	N	1420	188	1450	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)
VC-408	3 - 4 (ft)	9/2/2014	FD	2630	203	3030	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)
VC-408	3 - 4 (ft)	9/2/2014	N	2600	197	2910	ND (0.0843)	ND (0.0843)	ND (0.0843)	ND (0.0843)	ND (0.0843)	ND (0.0843)	ND (0.0843)	ND (0.0843)	ND (0.0843)	ND (0.0843)
VC-408	4 - 5 (ft)	9/2/2014	N	2060	269	3120	ND (0.0831)	ND (0.0831)	ND (0.0831)	ND (0.0831)	ND (0.0831)	ND (0.0831)	ND (0.0831)	ND (0.0831)	ND (0.0831)	ND (0.0831)
VC-408	5 - 6 (ft)	9/2/2014	N	917	160	1560	ND (0.0804)	ND (0.0804)	ND (0.0804)	ND (0.0804)	ND (0.0804)	ND (0.0804)	ND (0.0804)	ND (0.0804)	ND (0.0804)	ND (0.0804)
VC-408	6 - 8 (ft)	9/2/2014	N	293	108	311	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)
VC-409	0 - 0.5 (ft)	9/2/2014	N	79.2	47.6	131	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	0.224	ND (0.122)	ND (0.122)	0.132	ND (0.122)	0.356
VC-409	0.5 - 1 (ft)	9/2/2014	N	1250	171	432	ND (0.224)	ND (0.224)	ND (0.224)	ND (0.224)	2.55	ND (0.224)	ND (0.224)	3.14	ND (0.224)	5.69
VC-409	1 - 2 (ft)	9/2/2014	FD	636	306	349	ND (1.59)	ND (1.59)	ND (1.59)	ND (1.59)	6.64	ND (1.59)	ND (1.59)	25.1	ND (1.59)	31.74
VC-409	1 - 2 (ft)	9/2/2014	N	536	198	404	ND (0.877)	ND (0.877)	ND (0.877)	ND (0.877)	7.01	ND (0.877)	ND (0.877)	13.7	7.46	28.17
VC-409	2 - 3 (ft)	9/2/2014	N	780	139	817	ND (0.174)	ND (0.174)	ND (0.174)	ND (0.174)	0.545	ND (0.174)	ND (0.174)	0.742	0.425	1.712
VC-409	3 - 4 (ft)	9/2/2014	N	1800	179	2000	ND (0.166)	ND (0.166)	ND (0.166)	ND (0.166)	0.647	ND (0.166)	ND (0.166)	1.24	0.97	2.857
VC-409	4 - 5 (ft)	9/2/2014	N	1020	121	1560	ND (0.0802)	ND (0.0802)	ND (0.0802)	ND (0.0802)	ND (0.0802)	ND (0.0802)	ND (0.0802)	0.163	0.0909	0.254
VC-409	5 - 6 (ft)	9/2/2014	N	289	127	311	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)
VC-409	6 - 8 (ft)	9/2/2014	N	163	111	220	ND (0.0841)	ND (0.0841)	ND (0.0841)	ND (0.0841)	ND (0.0841)	ND (0.0841)	ND (0.0841)	0.0811 J	ND (0.0841)	0.0811 J
VC-410	0 - 0.5 (ft)	9/9/2014	N	67.2	49.9	153	ND (0.13)	ND (0.13)	ND (0.13)	ND (0.13)	0.248	ND (0.13)	ND (0.13)	0.152	ND (0.13)	0.4
VC-410	0.5 - 1 (ft)	9/9/2014	FD	247	229	1460	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	0.325	ND (0.194)	ND (0.194)	ND (0.194)	ND (0.194)	0.325
VC-410	0.5 - 1 (ft)	9/9/2014	N	631	67.4	183	ND (0.196)	ND (0.196)	ND (0.196)	ND (0.196)	ND (0.196)	1.56	ND (0.196)	ND (0.196)	ND (0.196)	1.56
VC-410	1 - 2 (ft)	9/9/2014	N	3920	137	210	ND (0.27)	ND (0.27)	ND (0.27)	ND (0.27)	1.87	ND (0.27)	ND (0.27)	1.24	ND (0.27)	3.11
VC-410	2 - 3 (ft)	9/9/2014	N	813	138	265	ND (0.176)	ND (0.176)	ND (0.176)	ND (0.176)	1.8	ND (0.176)	ND (0.176)	1.87	ND (0.176)	3.67
VC-410	3 - 4 (ft)	9/9/2014	N	957	150	280	ND (0.558)	ND (0.558)	ND (0.558)	ND (0.558)	2.94	ND (0.558)	ND (0.558)	ND (0.558)	3.7	6.64
VC-410	4 - 5 (ft)	9/9/2014	N	6300	148	320	ND (0.0809)	ND (0.0809)	ND (0.0809)	ND (0.0809)	0.453	ND (0.0809)	ND (0.0809)	0.718	ND (0.0809)	1.171
VC-410	5 - 6 (ft)	9/9/2014	N	1200	162	1190	ND (0.0805)	ND (0.0805)	ND (0.0805)	ND (0.0805)	0.0806	ND (0.0805)	ND (0.0805)	0.0486 J	ND (0.0805)	0.1292

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-410	6 - 8 (ft)	9/9/2014	N	632	169	1090	ND (0.0837)	ND (0.0837)	ND (0.0837)	ND (0.0837)	ND (0.0837)	ND (0.0837)	ND (0.0837)	ND (0.0837)	ND (0.0837)	ND (0.0837)
VC-411	0 - 0.5 (ft)	10/3/2014	N	59.1	55.5	153 B	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.163	ND (0.12)	ND (0.12)	0.156	ND (0.12)	0.319
VC-411	0.5 - 1 (ft)	10/3/2014	N	85	66.3	158 B	ND (0.0992)	ND (0.0992)	ND (0.0992)	ND (0.0992)	0.448	ND (0.0992)	ND (0.0992)	0.163	ND (0.0992)	0.611
VC-411	1 - 2 (ft)	10/3/2014	N	176	92	155 B	ND (0.179)	ND (0.179)	ND (0.179)	ND (0.179)	0.752	ND (0.179)	ND (0.179)	0.64	ND (0.179)	1.392
VC-411	2 - 3 (ft)	10/3/2014	FD	958	294	233 B	ND (0.253)	ND (0.253)	ND (0.253)	ND (0.253)	2.36	ND (0.253)	ND (0.253)	2.45	ND (0.253)	4.81
VC-411	2 - 3 (ft)	10/3/2014	N	643	132	192 B	ND (0.16)	ND (0.16)	ND (0.16)	ND (0.16)	2.28	ND (0.16)	ND (0.16)	1.18	ND (0.16)	3.46
VC-411	3 - 4 (ft)	10/3/2014	N	437	141	259 B	ND (0.0925)	ND (0.0925)	ND (0.0925)	ND (0.0925)	0.786	ND (0.0925)	ND (0.0925)	0.95	ND (0.0925)	1.736
VC-411	4 - 5 (ft)	10/3/2014	N	452	139	272 B	ND (1.92)	ND (1.92)	ND (1.92)	ND (1.92)	4.93	ND (1.92)	ND (1.92)	53.4	ND (1.92)	58.33
VC-411	5 - 6 (ft)	10/3/2014	N	283	131	301 B	ND (0.0907)	ND (0.0907)	ND (0.0907)	ND (0.0907)	ND (0.0907)	ND (0.0907)	ND (0.0907)	ND (0.0907)	ND (0.0907)	ND (0.0907)
VC-411	6 - 8 (ft)	10/3/2014	N	405	145	386 B	ND (0.0905)	ND (0.0905)	ND (0.0905)	ND (0.0905)	ND (0.0905)	ND (0.0905)	ND (0.0905)	ND (0.0905)	ND (0.0905)	ND (0.0905)
VC-412	0 - 0.5 (ft)	10/3/2014	N	53.4	50.5	134 B	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.207	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.207
VC-412	0.5 - 1 (ft)	10/3/2014	N	153	73.1	150 B	ND (0.099)	ND (0.099)	ND (0.099)	ND (0.099)	0.456	ND (0.099)	ND (0.099)	0.305	ND (0.099)	0.761
VC-412	1 - 2 (ft)	10/3/2014	N	169	104	169 B	ND (0.0842)	ND (0.0842)	ND (0.0842)	ND (0.0842)	0.547	ND (0.0842)	ND (0.0842)	0.484	ND (0.0842)	1.031
VC-412	2 - 3 (ft)	10/3/2014	N	572	133	175 B	ND (0.344)	ND (0.344)	ND (0.344)	ND (0.344)	2.99	ND (0.344)	ND (0.344)	2.59	ND (0.344)	5.58
VC-412	3 - 4 (ft)	10/3/2014	N	262	140	166 B	ND (0.266)	ND (0.266)	ND (0.266)	ND (0.266)	2.3	ND (0.266)	ND (0.266)	1.66	ND (0.266)	3.96
VC-412	4 - 5 (ft)	10/3/2014	FD	549	123	206 B	ND (0.403)	ND (0.403)	ND (0.403)	ND (0.403)	3.89	ND (0.403)	ND (0.403)	3.43	ND (0.403)	7.32
VC-412	4 - 5 (ft)	10/3/2014	N	540	838	202 B	ND (0.341)	ND (0.341)	ND (0.341)	ND (0.341)	3.47	ND (0.341)	ND (0.341)	2.17	ND (0.341)	5.64
VC-412	5 - 6 (ft)	10/3/2014	N	544	143	215 B	ND (0.504)	ND (0.504)	ND (0.504)	ND (0.504)	5.16	ND (0.504)	ND (0.504)	5.42	ND (0.504)	10.58
VC-412	6 - 8 (ft)	10/3/2014	N	523	164	267 B	ND (0.687)	ND (0.687)	ND (0.687)	ND (0.687)	10.1	ND (0.687)	ND (0.687)	3.14	ND (0.687)	13.24
VC-413	0 - 0.5 (ft)	10/3/2014	N	57.6	46.5	124 B	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.24	ND (0.114)	ND (0.114)	ND (0.114)	ND (0.114)	0.24
VC-413	0.5 - 1 (ft)	10/3/2014	N	62.9	61.5	124 B	ND (0.0904)	ND (0.0904)	ND (0.0904)	ND (0.0904)	0.251	ND (0.0904)	ND (0.0904)	0.142	ND (0.0904)	0.393
VC-413	1 - 2 (ft)	10/3/2014	N	90.4	71.7	160 B	ND (0.0978)	ND (0.0978)	ND (0.0978)	ND (0.0978)	0.581	ND (0.0978)	ND (0.0978)	1.25	ND (0.0978)	1.831
VC-413	2 - 3 (ft)	10/3/2014	N	130	82.1	162 B	ND (0.0947)	ND (0.0947)	ND (0.0947)	ND (0.0947)	0.528	ND (0.0947)	ND (0.0947)	0.118	ND (0.0947)	0.646
VC-413	3 - 4 (ft)	10/3/2014	N	138	88.3	157 B	ND (0.0891)	ND (0.0891)	ND (0.0891)	ND (0.0891)	0.462	ND (0.0891)	ND (0.0891)	0.167	ND (0.0891)	0.629
VC-413	4 - 5 (ft)	10/3/2014	N	240	105	177 B	ND (0.081)	ND (0.081)	ND (0.081)	ND (0.081)	1.13	ND (0.081)	ND (0.081)	1.15	ND (0.081)	2.28
VC-413	5 - 6 (ft)	10/3/2014	N	340	120	188 B	ND (0.237)	ND (0.237)	ND (0.237)	ND (0.237)	2.22	ND (0.237)	ND (0.237)	1.84	ND (0.237)	4.06
VC-413	6 - 8 (ft)	10/3/2014	N	943	170	227 B	ND (0.333)	ND (0.333)	ND (0.333)	ND (0.333)	3.02	ND (0.333)	ND (0.333)	1.64	ND (0.333)	4.66
VC-414	0 - 0.5 (ft)	10/3/2014	N	68.1	53.6	135 B	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.281	ND (0.116)	ND (0.116)	0.109 J	ND (0.116)	0.39
VC-414	0.5 - 1 (ft)	10/3/2014	N	84.7	65.2	140 B	ND (0.0939)	ND (0.0939)	ND (0.0939)	ND (0.0939)	0.342	ND (0.0939)	ND (0.0939)	0.178	ND (0.0939)	0.52
VC-414	1 - 2 (ft)	10/3/2014	FD	98.5	74.1	170 B	ND (0.0938)	ND (0.0938)	ND (0.0938)	ND (0.0938)	0.339	ND (0.0938)	ND (0.0938)	0.477	ND (0.0938)	0.816
VC-414	1 - 2 (ft)	10/3/2014	N	89.5	69.7	154 B	ND (0.0908)	ND (0.0908)	ND (0.0908)	ND (0.0908)	0.311	ND (0.0908)	ND (0.0908)	0.189	ND (0.0908)	0.5
VC-414	2 - 3 (ft)	10/3/2014	N	135	75.6	158 B	ND (0.0895)	ND (0.0895)	ND (0.0895)	ND (0.0895)	0.332	ND (0.0895)	ND (0.0895)	0.118	ND (0.0895)	0.45
VC-414	3 - 4 (ft)	10/3/2014	N	108	105	175 B	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	0.406	ND (0.0859)	ND (0.0859)	0.119	ND (0.0859)	0.525
VC-414	4 - 5 (ft)	10/3/2014	N	101	93.1	178 B	ND (0.168)	ND (0.168)	ND (0.168)	ND (0.168)	0.936	ND (0.168)	ND (0.168)	3.37	ND (0.168)	4.306
VC-414	5 - 6 (ft)	10/3/2014	N	124	102	203 B	ND (0.083)	ND (0.083)	ND (0.083)	ND (0.083)	1.12	ND (0.083)	ND (0.083)	0.248	ND (0.083)	1.368
VC-414	6 - 8 (ft)	10/3/2014	N	507	147	246 B	ND (0.265)	ND (0.265)	ND (0.265)	ND (0.265)	3.15	ND (0.265)	ND (0.265)	1.17	ND (0.265)	4.32
VC-415	0 - 0.5 (ft)	10/3/2014	N	72.5	51	135 B	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	0.185	ND (0.107)	ND (0.107)	0.0832 J	ND (0.107)	0.2682
VC-415	0.5 - 1 (ft)	10/3/2014	N	106	60.1	145 B	ND (0.0899)	ND (0.0899)	ND (0.0899)	ND (0.0899)	0.226	ND (0.0899)	ND (0.0899)	0.13	ND (0.0899)	0.356
VC-415	1 - 2 (ft)	10/3/2014	N	86.3	68.5	157 B	ND (0.0911)	ND (0.0911)	ND (0.0911)	ND (0.0911)	0.344	ND (0.0911)	ND (0.0911)	0.162	ND (0.0911)	0.506
VC-415	2 - 3 (ft)	10/3/2014	N	74.1	71	157 B	ND (0.0964)	ND (0.0964)	ND (0.0964)	ND (0.0964)	0.406	ND (0.0964)	ND (0.0964)	0.139	ND (0.0964)	0.545
VC-415	3 - 4 (ft)	10/3/2014	FD	156	111	193 B	ND (0.0946)	ND (0.0946)	ND (0.0946)	ND (0.0946)	0.449	ND (0.0946)	ND (0.0946)	0.164	ND (0.0946)	0.613

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-415	3 - 4 (ft)	10/3/2014	N	160	104	200 B	ND (0.091)	ND (0.091)	ND (0.091)	ND (0.091)	0.576	ND (0.091)	ND (0.091)	0.447	ND (0.091)	1.023
VC-415	4 - 5 (ft)	10/3/2014	N	124	103	182 B	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	0.857	ND (0.086)	ND (0.086)	0.538	ND (0.086)	1.395
VC-415	5 - 6 (ft)	10/3/2014	N	21.9	19.8	107	ND (0.0811)	ND (0.0811)	ND (0.0811)	ND (0.0811)	1.09	ND (0.0811)	ND (0.0811)	0.206	ND (0.0811)	1.296
VC-415	6 - 8 (ft)	10/3/2014	N	123	122	198 B	ND (0.0831)	ND (0.0831)	ND (0.0831)	ND (0.0831)	1.79	0.634	ND (0.0831)	0.179	ND (0.0831)	2.603
VC-416	0 - 0.5 (ft)	10/21/2014	N	67	62	151 B	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.276	ND (0.116)	ND (0.116)	0.189	ND (0.116)	0.465
VC-416	0.5 - 1 (ft)	10/21/2014	N	76.5	73.8	161 B	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.396	ND (0.11)	ND (0.11)	1.19	ND (0.11)	1.586
VC-416	1 - 2 (ft)	10/21/2014	N	81.7	72.2	160 B	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.414	ND (0.102)	ND (0.102)	0.388	ND (0.102)	0.802
VC-416	2 - 3 (ft)	10/21/2014	N	115	80.3	180 B	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	0.604	ND (0.106)	ND (0.106)	0.213	ND (0.106)	0.817
VC-416	3 - 4 (ft)	10/21/2014	N	121	85.8	166 B	ND (0.0868)	ND (0.0868)	ND (0.0868)	ND (0.0868)	0.621	ND (0.0868)	ND (0.0868)	0.893	ND (0.0868)	1.514
VC-416	4 - 5 (ft)	10/21/2014	FD	125	106	176 B	ND (0.0792)	ND (0.0792)	ND (0.0792)	ND (0.0792)	0.653	ND (0.0792)	ND (0.0792)	0.264	ND (0.0792)	0.917
VC-416	4 - 5 (ft)	10/21/2014	N	116	104	173 B	ND (0.159)	ND (0.159)	ND (0.159)	ND (0.159)	1.21	ND (0.159)	ND (0.159)	1.72	ND (0.159)	2.93
VC-416	5 - 6 (ft)	10/21/2014	N	94.1	91.4	193	ND (0.0826)	ND (0.0826)	ND (0.0826)	ND (0.0826)	1.35	ND (0.0826)	ND (0.0826)	0.501	ND (0.0826)	1.851
VC-416	6 - 8 (ft)	10/21/2014	N	206	121	217 B	ND (0.0818)	ND (0.0818)	ND (0.0818)	ND (0.0818)	2.22	0.662	ND (0.0818)	0.684	ND (0.0818)	3.566
VC-417	0 - 0.5 (ft)	10/21/2014	N	101	62.9	149 B	ND (0.111)	ND (0.111)	ND (0.111)	ND (0.111)	0.199	ND (0.111)	ND (0.111)	0.0962 J	ND (0.111)	0.295
VC-417	0.5 - 1 (ft)	10/21/2014	N	131	69.4	150 B	ND (0.0975)	ND (0.0975)	ND (0.0975)	ND (0.0975)	0.295	ND (0.0975)	ND (0.0975)	0.31	ND (0.0975)	0.605
VC-417	1 - 2 (ft)	10/21/2014	N	152	70.2	147 B	ND (0.0892)	ND (0.0892)	ND (0.0892)	ND (0.0892)	0.761	ND (0.0892)	ND (0.0892)	0.742	ND (0.0892)	1.503
VC-417	2 - 3 (ft)	10/21/2014	N	148	86.5	169 B	ND (0.0956)	ND (0.0956)	ND (0.0956)	ND (0.0956)	0.822	ND (0.0956)	ND (0.0956)	1.5	ND (0.0956)	2.322
VC-417	3 - 4 (ft)	10/21/2014	N	124	97.2	179 B	ND (0.0855)	ND (0.0855)	ND (0.0855)	ND (0.0855)	1.1	ND (0.0855)	ND (0.0855)	0.292	ND (0.0855)	1.392
VC-417	4 - 5 (ft)	10/21/2014	FD	767	155	208 B	ND (0.085)	ND (0.085)	ND (0.085)	ND (0.085)	1.4	ND (0.085)	ND (0.085)	0.34	ND (0.085)	1.74
VC-417	4 - 5 (ft)	10/21/2014	N	655	146	210 B	ND (0.0841)	ND (0.0841)	ND (0.0841)	ND (0.0841)	2.29	ND (0.0841)	ND (0.0841)	0.704	ND (0.0841)	2.994
VC-417	5 - 6 (ft)	10/21/2014	N	935	118	162	ND (0.0795)	ND (0.0795)	ND (0.0795)	ND (0.0795)	1.81	ND (0.0795)	ND (0.0795)	0.966	ND (0.0795)	2.776
VC-417	6 - 8 (ft)	10/21/2014	N	1290	198	198 B	ND (0.0789)	ND (0.0789)	ND (0.0789)	ND (0.0789)	1.52	1.39	ND (0.0789)	1.33	ND (0.0789)	4.24
VC-418	0 - 0.5 (ft)	10/21/2014	N	54.3	52.3	137 B	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	0.192	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	0.192
VC-418	0.5 - 1 (ft)	10/21/2014	N	297	76.3	159 B	ND (1.04)	ND (1.04)	ND (1.04)	ND (1.04)	1.92	ND (1.04)	ND (1.04)	7.19	ND (1.04)	9.11
VC-418	1 - 2 (ft)	10/21/2014	N	213	101	185 B	ND (6.01)	ND (6.01)	ND (6.01)	ND (6.01)	ND (6.01)	24.1	ND (6.01)	87.2	ND (6.01)	111.3
VC-418	2 - 3 (ft)	10/21/2014	N	271	103	168 B	ND (0.17)	ND (0.17)	ND (0.17)	ND (0.17)	1.31	ND (0.17)	ND (0.17)	0.942	ND (0.17)	2.25
VC-418	3 - 4 (ft)	10/21/2014	FD	1840	141	202 B	ND (0.352)	ND (0.352)	ND (0.352)	ND (0.352)	3.49	ND (0.352)	ND (0.352)	0.902	ND (0.352)	4.392
VC-418	3 - 4 (ft)	10/21/2014	N	1060	135	186 B	ND (0.235)	ND (0.235)	ND (0.235)	ND (0.235)	1.95	ND (0.235)	ND (0.235)	0.412	ND (0.235)	2.362
VC-418	4 - 5 (ft)	10/21/2014	N	5490	171	189 B	ND (0.322)	ND (0.322)	ND (0.322)	ND (0.322)	2.16	ND (0.322)	ND (0.322)	1.13	ND (0.322)	3.29
VC-418	5 - 6 (ft)	10/21/2014	N	1240	159	212	ND (0.0786)	ND (0.0786)	ND (0.0786)	ND (0.0786)	2.55	ND (0.0786)	ND (0.0786)	1.86	ND (0.0786)	4.41
VC-418	6 - 8 (ft)	10/21/2014	N	879	171	258 B	ND (0.0842)	ND (0.0842)	ND (0.0842)	ND (0.0842)	1.01	0.848	ND (0.0842)	0.324	ND (0.0842)	2.182
VC-419	0 - 0.5 (ft)	10/22/2014	N	174	70.5	230 B	ND (1.22)	ND (1.22)	ND (1.22)	ND (1.22)	ND (1.22)	3.19	ND (1.22)	15.5	ND (1.22)	18.69
VC-419	0.5 - 1 (ft)	10/22/2014	N	1110	153	176 B	ND (0.113)	ND (0.113)	ND (0.113)	ND (0.113)	0.58	ND (0.113)	ND (0.113)	1.25	ND (0.113)	1.83
VC-419	1 - 2 (ft)	10/22/2014	N	210	115	319 B	ND (0.0957)	ND (0.0957)	ND (0.0957)	ND (0.0957)	0.559	ND (0.0957)	ND (0.0957)	0.539	ND (0.0957)	1.098
VC-419	2 - 3 (ft)	10/22/2014	N	403	107	196 B	ND (0.093)	ND (0.093)	ND (0.093)	ND (0.093)	0.661	ND (0.093)	ND (0.093)	0.189	ND (0.093)	0.85
VC-419	3 - 4 (ft)	10/22/2014	FD	4030	137	209 B	ND (0.356)	ND (0.356)	ND (0.356)	ND (0.356)	4.41	ND (0.356)	ND (0.356)	1.48	ND (0.356)	5.89
VC-419	3 - 4 (ft)	10/22/2014	N	525	111	167 B	ND (0.246)	ND (0.246)	ND (0.246)	ND (0.246)	3.17	ND (0.246)	ND (0.246)	0.689	ND (0.246)	3.859
VC-419	4 - 5 (ft)	10/22/2014	N	671	158	223 B	ND (0.439)	ND (0.439)	ND (0.439)	ND (0.439)	4.98	ND (0.439)	ND (0.439)	1.04	ND (0.439)	6.02
VC-419	5 - 6 (ft)	10/22/2014	N	450	177	252	ND (0.0882)	ND (0.0882)	ND (0.0882)	ND (0.0882)	1.82	ND (0.0882)	ND (0.0882)	2.14	ND (0.0882)	3.96
VC-419	6 - 8 (ft)	10/22/2014	N	241	126	217 B	ND (0.0889)	ND (0.0889)	ND (0.0889)	ND (0.0889)	ND (0.0889)	ND (0.0889)	ND (0.0889)	ND (0.0889)	ND (0.0889)	ND (0.0889)
VC-420	0 - 0.5 (ft)	10/21/2014	N	71.5	48.9	130 B	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	ND (0.108)	0.371	ND (0.108)	0.313	ND (0.108)	0.684

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-420	0.5 - 1 (ft)	10/21/2014	N	227	90.9	169 B	ND (0.106)	ND (0.106)	ND (0.106)	ND (0.106)	0.56	ND (0.106)	ND (0.106)	0.798	ND (0.106)	1.358
VC-420	1 - 2 (ft)	10/21/2014	N	397	98.6	178 B	ND (0.0902)	ND (0.0902)	ND (0.0902)	ND (0.0902)	0.537	ND (0.0902)	ND (0.0902)	0.328	ND (0.0902)	0.865
VC-420	2 - 3 (ft)	10/21/2014	N	795	123	185 B	ND (0.249)	ND (0.249)	ND (0.249)	ND (0.249)	2.02	ND (0.249)	ND (0.249)	0.855	ND (0.249)	2.875
VC-420	3 - 4 (ft)	10/21/2014	FD	1630	166	219 B	ND (0.253)	ND (0.253)	ND (0.253)	ND (0.253)	1.92	ND (0.253)	ND (0.253)	2.03	ND (0.253)	3.95
VC-420	3 - 4 (ft)	10/21/2014	N	1490	277	218 B	ND (0.326)	ND (0.326)	ND (0.326)	ND (0.326)	1.69	ND (0.326)	ND (0.326)	2.46	ND (0.326)	4.15
VC-420	4 - 5 (ft)	10/21/2014	N	850	368	250 B	ND (1.75)	ND (1.75)	ND (1.75)	ND (1.75)	8.38	ND (1.75)	ND (1.75)	13.2	ND (1.75)	21.58
VC-420	5 - 6 (ft)	10/21/2014	N	560	166	226	ND (0.0881)	ND (0.0881)	ND (0.0881)	ND (0.0881)	0.069 J	ND (0.0881)	ND (0.0881)	0.106	ND (0.0881)	0.175
VC-420	6 - 8 (ft)	10/21/2014	N	291	196	224 B	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	0.0813 J	0.0813 J
VC-421	0 - 0.5 (ft)	10/21/2014	N	81.1	65.5	149 B	ND (0.127)	ND (0.127)	ND (0.127)	ND (0.127)	0.326	ND (0.127)	ND (0.127)	0.562	ND (0.127)	0.888
VC-421	0.5 - 1 (ft)	10/21/2014	N	763	107	215 B	ND (0.189)	ND (0.189)	ND (0.189)	ND (0.189)	1.15	ND (0.189)	ND (0.189)	0.853	ND (0.189)	2.003
VC-421	1 - 2 (ft)	10/21/2014	N	734	132	213 B	ND (0.566)	ND (0.566)	ND (0.566)	ND (0.566)	3.87	ND (0.566)	ND (0.566)	0.996 P	ND (0.566)	4.866
VC-421	2 - 3 (ft)	10/21/2014	N	1910	137	213 B	ND (0.278)	ND (0.278)	ND (0.278)	ND (0.278)	2.24	ND (0.278)	ND (0.278)	ND (0.278)	11.1	13.34
VC-421	3 - 4 (ft)	10/21/2014	N	4360	228	230 B	ND (0.426)	ND (0.426)	ND (0.426)	ND (0.426)	1.62	ND (0.426)	ND (0.426)	3.11	ND (0.426)	4.73
VC-421	4 - 5 (ft)	10/21/2014	FD	1550	351	260 B	ND (1.71)	ND (1.71)	ND (1.71)	ND (1.71)	6.14	ND (1.71)	ND (1.71)	10.6	ND (1.71)	16.74
VC-421	4 - 5 (ft)	10/21/2014	N	1600	359	296 B	ND (1.79)	ND (1.79)	ND (1.79)	ND (1.79)	8.61	ND (1.79)	ND (1.79)	14.3	ND (1.79)	22.91
VC-421	5 - 6 (ft)	10/21/2014	N	548	208	226	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	0.103	ND (0.0846)	0.103
VC-421	6 - 8 (ft)	10/21/2014	N	220	117	205 B	ND (0.0832)	ND (0.0832)	ND (0.0832)	ND (0.0832)	ND (0.0832)	ND (0.0832)	ND (0.0832)	ND (0.0832)	ND (0.0832)	ND (0.0832)
VC-422	0 - 0.5 (ft)	10/22/2014	N	67	60.6	149 B	ND (0.12)	ND (0.12)	ND (0.12)	ND (0.12)	0.329	ND (0.12)	ND (0.12)	0.396	ND (0.12)	0.725
VC-422	0.5 - 1 (ft)	10/22/2014	N	362	126	191 B	ND (0.443)	ND (0.443)	ND (0.443)	ND (0.443)	2.05	ND (0.443)	ND (0.443)	0.823	ND (0.443)	2.873
VC-422	1 - 2 (ft)	10/22/2014	FD	237	110	178 B	ND (0.407)	ND (0.407)	ND (0.407)	ND (0.407)	2.81	ND (0.407)	ND (0.407)	ND (0.407)	ND (0.407)	2.81
VC-422	1 - 2 (ft)	10/22/2014	N	336	127	187 B	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	3.01	ND (0.34)	ND (0.34)	ND (0.34)	ND (0.34)	3.01
VC-422	2 - 3 (ft)	10/22/2014	N	587	148	177	ND (0.0819)	ND (0.0819)	ND (0.0819)	ND (0.0819)	1.59	ND (0.0819)	ND (0.0819)	0.704	ND (0.0819)	2.294
VC-422	3 - 4 (ft)	10/22/2014	N	545	120	176	ND (0.406)	ND (0.406)	ND (0.406)	ND (0.406)	1.94	ND (0.406)	ND (0.406)	4.87	ND (0.406)	6.81
VC-422	4 - 5 (ft)	10/22/2014	N	859	206	249 B	ND (0.168)	ND (0.168)	ND (0.168)	ND (0.168)	0.845	ND (0.168)	ND (0.168)	1.59	ND (0.168)	2.435
VC-422	5 - 6 (ft)	10/22/2014	N	266	140	213	ND (0.0851)	ND (0.0851)	ND (0.0851)	ND (0.0851)	ND (0.0851)	0.624	ND (0.0851)	2.39	ND (0.0851)	3.014
VC-422	6 - 8 (ft)	10/22/2014	N	94.7	62.7	120 B	ND (0.0835)	ND (0.0835)	ND (0.0835)	ND (0.0835)	ND (0.0835)	ND (0.0835)	ND (0.0835)	ND (0.0835)	ND (0.0835)	ND (0.0835)
VC-501	0 - 0.5 (ft)	9/11/2014	N	41.7	39.5	111	ND (0.304)	ND (0.304)	ND (0.304)	ND (0.304)	0.723	ND (0.304)	ND (0.304)	3.76	ND (0.304)	4.483
VC-501	0.5 - 1 (ft)	9/11/2014	N	69.1	61.9	123	ND (0.145)	ND (0.145)	ND (0.145)	ND (0.145)	0.54	ND (0.145)	ND (0.145)	2.02	ND (0.145)	2.56
VC-501	1 - 2 (ft)	9/11/2014	N	96.3	103	178	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	1.15	ND (0.088)	ND (0.088)	0.363	ND (0.088)	1.513
VC-501	2 - 3 (ft)	9/11/2014	N	117	124	232	ND (0.0913)	ND (0.0913)	ND (0.0913)	ND (0.0913)	1.75	ND (0.0913)	ND (0.0913)	0.347	ND (0.0913)	2.097
VC-501	3 - 4 (ft)	9/11/2014	N	117	122	226	ND (0.0982)	ND (0.0982)	ND (0.0982)	ND (0.0982)	2.27	ND (0.0982)	ND (0.0982)	0.55	ND (0.0982)	2.82
VC-501	4 - 5 (ft)	9/11/2014	N	131	145	248	ND (0.195)	ND (0.195)	ND (0.195)	ND (0.195)	3.46	ND (0.195)	ND (0.195)	0.52	ND (0.195)	3.98
VC-501	5 - 6 (ft)	9/11/2014	N	194	158	246	ND (7.4)	ND (7.4)	ND (7.4)	ND (7.4)	35.3	ND (7.4)	ND (7.4)	130	ND (7.4)	165.3
VC-501	6 - 8 (ft)	9/11/2014	FD	355	198	273	ND (0.451)	ND (0.451)	ND (0.451)	ND (0.451)	6	ND (0.451)	ND (0.451)	6.18	ND (0.451)	12.18
VC-501	6 - 8 (ft)	9/11/2014	N	344	187	262	ND (0.883)	ND (0.883)	ND (0.883)	ND (0.883)	13.9	ND (0.883)	ND (0.883)	16.7	ND (0.883)	30.6
VC-502	0 - 0.5 (ft)	10/30/2014	N	40	41.8	112	ND (0.0965)	ND (0.0965)	ND (0.0965)	ND (0.0965)	0.17	ND (0.0965)	ND (0.0965)	0.0803 J	ND (0.0965)	0.2503
VC-502	0.5 - 1 (ft)	9/30/2014	N	94.5	88.4	166 B	ND (0.0853)	ND (0.0853)	ND (0.0853)	ND (0.0853)	0.899	ND (0.0853)	ND (0.0853)	1.02	ND (0.0853)	1.919
VC-502	1 - 2 (ft)	9/30/2014	N	77.5	70.8	153 B	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	0.597	ND (0.086)	ND (0.086)	0.698	ND (0.086)	1.295
VC-502	2 - 3 (ft)	9/30/2014	N	144	136	248 B	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	1.93	ND (0.192)	ND (0.192)	0.32	ND (0.192)	2.25
VC-502	3 - 4 (ft)	9/30/2014	N	129	127	239 B	ND (0.376)	ND (0.376)	ND (0.376)	ND (0.376)	3.06	ND (0.376)	ND (0.376)	0.352 J	ND (0.376)	3.412
VC-502	4 - 5 (ft)	9/30/2014	N	172	148	227 B	ND (0.557)	ND (0.557)	ND (0.557)	ND (0.557)	4.89	ND (0.557)	ND (0.557)	0.451 J	ND (0.557)	5.341

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-502	5 - 6 (ft)	9/30/2014	N	225	159	264 B	ND (0.276)	ND (0.276)	ND (0.276)	ND (0.276)	2.96	ND (0.276)	ND (0.276)	0.992	ND (0.276)	3.952
VC-502	6 - 8 (ft)	9/30/2014	N	238	112	325 B	ND (0.0887)	ND (0.0887)	ND (0.0887)	ND (0.0887)	0.131	ND (0.0887)	ND (0.0887)	0.165	ND (0.0887)	0.296
VC-503	0 - 0.5 (ft)	10/30/2014	N	47.5	47.6	127	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	0.0911 J	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	0.0911 J
VC-503	0.5 - 1 (ft)	9/30/2014	N	98.2	96.6	202	ND (0.174)	ND (0.174)	ND (0.174)	ND (0.174)	1.46	ND (0.174)	ND (0.174)	0.144 J	ND (0.174)	1.604
VC-503	1 - 2 (ft)	9/30/2014	N	120	124	248	ND (0.285)	ND (0.285)	ND (0.285)	ND (0.285)	2.43	ND (0.285)	ND (0.285)	ND (0.285)	ND (0.285)	2.43
VC-503	2 - 3 (ft)	9/30/2014	FD	117	123	228	ND (0.298)	ND (0.298)	ND (0.298)	ND (0.298)	3.54	ND (0.298)	ND (0.298)	0.197 J	ND (0.298)	3.737
VC-503	2 - 3 (ft)	9/30/2014	N	113	120	228	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	3.74	ND (0.299)	ND (0.299)	ND (0.299)	ND (0.299)	3.74
VC-503	3 - 4 (ft)	9/30/2014	N	174	142	239	ND (0.378)	ND (0.378)	ND (0.378)	ND (0.378)	4.24	ND (0.378)	ND (0.378)	0.379	ND (0.378)	4.619
VC-503	4 - 5 (ft)	9/30/2014	N	172	137	237	ND (0.265)	ND (0.265)	ND (0.265)	ND (0.265)	4.39	ND (0.265)	ND (0.265)	0.719	ND (0.265)	5.109
VC-503	5 - 6 (ft)	9/30/2014	N	184	160	271	ND (0.478)	ND (0.478)	ND (0.478)	ND (0.478)	5.47	ND (0.478)	ND (0.478)	0.302 J	ND (0.478)	5.772
VC-503	6 - 8 (ft)	9/30/2014	N	187	159	259	ND (0.367)	ND (0.367)	ND (0.367)	ND (0.367)	3.81	ND (0.367)	ND (0.367)	0.737	ND (0.367)	4.547
VC-504	0 - 0.5 (ft)	9/11/2014	N	48.1	47.1	133	ND (0.112)	ND (0.112)	ND (0.112)	0.836	ND (0.112)	ND (0.112)	ND (0.112)	0.231	ND (0.112)	1.067
VC-504	0.5 - 1 (ft)	9/11/2014	N	67.7	62.6	142	ND (0.0859)	ND (0.0859)	ND (0.0859)	ND (0.0859)	0.443	ND (0.0859)	ND (0.0859)	1.24	ND (0.0859)	1.683
VC-504	1 - 2 (ft)	9/11/2014	FD	96	91	167	ND (0.0866)	ND (0.0866)	ND (0.0866)	ND (0.0866)	0.909	ND (0.0866)	ND (0.0866)	0.752	ND (0.0866)	1.661
VC-504	1 - 2 (ft)	9/11/2014	N	82.3	82.1	156	ND (0.082)	ND (0.082)	ND (0.082)	ND (0.082)	0.77	ND (0.082)	ND (0.082)	0.483	ND (0.082)	1.253
VC-504	2 - 3 (ft)	9/11/2014	N	115	116	226	ND (0.0956)	ND (0.0956)	ND (0.0956)	ND (0.0956)	1.85	ND (0.0956)	ND (0.0956)	0.6	ND (0.0956)	2.45
VC-504	3 - 4 (ft)	9/11/2014	N	140	136	243	ND (0.192)	ND (0.192)	ND (0.192)	ND (0.192)	3.21	ND (0.192)	ND (0.192)	0.495	ND (0.192)	3.705
VC-504	4 - 5 (ft)	9/11/2014	N	152	150	247	ND (0.371)	ND (0.371)	ND (0.371)	ND (0.371)	5.03	ND (0.371)	ND (0.371)	ND (0.371)	ND (0.371)	5.03
VC-504	5 - 6 (ft)	9/11/2014	N	170	160	255	ND (0.485)	ND (0.485)	ND (0.485)	ND (0.485)	4.6	ND (0.485)	ND (0.485)	ND (0.485)	ND (0.485)	4.6
VC-504	6 - 8 (ft)	9/11/2014	N	222	155	261	ND (0.184)	ND (0.184)	ND (0.184)	ND (0.184)	1.64	ND (0.184)	ND (0.184)	1.26	ND (0.184)	2.9
VC-505	0 - 0.5 (ft)	10/2/2014	N	50.8	45.3	133 B	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.217	ND (0.116)	ND (0.116)	0.197	ND (0.116)	0.414
VC-505	0.5 - 1 (ft)	10/2/2014	N	110	108	215 B	ND (0.191)	ND (0.191)	ND (0.191)	ND (0.191)	1.32	ND (0.191)	ND (0.191)	0.27	ND (0.191)	1.59
VC-505	1 - 2 (ft)	10/2/2014	N	110	112	239 B	ND (0.206)	ND (0.206)	ND (0.206)	ND (0.206)	1.69	ND (0.206)	ND (0.206)	ND (0.206)	ND (0.206)	1.69
VC-505	2 - 3 (ft)	10/2/2014	N	133	131	234 B	ND (0.379)	ND (0.379)	ND (0.379)	ND (0.379)	3.77	ND (0.379)	ND (0.379)	0.347 J	ND (0.379)	4.117
VC-505	3 - 4 (ft)	10/2/2014	N	186	152	247 B	ND (0.564)	ND (0.564)	ND (0.564)	ND (0.564)	5.1	ND (0.564)	ND (0.564)	0.563 J	ND (0.564)	5.663
VC-505	4 - 5 (ft)	10/2/2014	N	175	165	260 B	ND (0.773)	ND (0.773)	ND (0.773)	ND (0.773)	6.05	ND (0.773)	ND (0.773)	ND (0.773)	ND (0.773)	6.05
VC-505	5 - 6 (ft)	10/2/2014	FD	206	169	254 B	ND (0.377)	ND (0.377)	ND (0.377)	ND (0.377)	3.29	ND (0.377)	ND (0.377)	1.28	ND (0.377)	4.57
VC-505	5 - 6 (ft)	10/2/2014	N	212	181	258 B	ND (0.383)	ND (0.383)	ND (0.383)	ND (0.383)	3.25	ND (0.383)	ND (0.383)	1.09	ND (0.383)	4.34
VC-505	6 - 8 (ft)	10/2/2014	N	250	127	236 B	ND (0.088)	ND (0.088)	ND (0.088)	ND (0.088)	0.601	ND (0.088)	ND (0.088)	1.05	ND (0.088)	1.651
VC-506	0 - 0.5 (ft)	10/30/2014	N	44.6	44.4	123	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.131	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.131
VC-506	0.5 - 1 (ft)	9/30/2014	N	54.5	52.1	139 B	ND (0.0951)	ND (0.0951)	ND (0.0951)	ND (0.0951)	0.213	ND (0.0951)	ND (0.0951)	ND (0.0951)	ND (0.0951)	0.213
VC-506	1 - 2 (ft)	9/30/2014	FD	80.4	71.7	161 B	ND (0.0898)	ND (0.0898)	ND (0.0898)	ND (0.0898)	0.564	ND (0.0898)	ND (0.0898)	0.213	ND (0.0898)	0.777
VC-506	1 - 2 (ft)	9/30/2014	N	82.6	72.4	161 B	ND (0.09)	ND (0.09)	ND (0.09)	ND (0.09)	0.529	ND (0.09)	ND (0.09)	0.188	ND (0.09)	0.717
VC-506	2 - 3 (ft)	9/30/2014	N	113	119	231 B	ND (0.185)	ND (0.185)	ND (0.185)	ND (0.185)	2.18	ND (0.185)	ND (0.185)	0.216	ND (0.185)	2.396
VC-506	3 - 4 (ft)	9/30/2014	N	114	123	229 B	ND (0.195)	ND (0.195)	ND (0.195)	ND (0.195)	2.99	ND (0.195)	ND (0.195)	0.305	ND (0.195)	3.295
VC-506	4 - 5 (ft)	9/30/2014	N	140	129	229 B	ND (0.46)	ND (0.46)	ND (0.46)	ND (0.46)	4.4	ND (0.46)	ND (0.46)	0.354 J	ND (0.46)	4.754
VC-506	5 - 6 (ft)	9/30/2014	N	184	160	256 B	ND (0.556)	ND (0.556)	ND (0.556)	ND (0.556)	5.35	ND (0.556)	ND (0.556)	ND (0.556)	ND (0.556)	5.35
VC-506	6 - 8 (ft)	9/30/2014	N	187	162	255 B	ND (0.572)	ND (0.572)	ND (0.572)	ND (0.572)	5.95	ND (0.572)	ND (0.572)	1.87	ND (0.572)	7.82
VC-507	0 - 0.5 (ft)	10/2/2014	N	53.6	51.5	143 B	ND (0.116)	ND (0.116)	ND (0.116)	ND (0.116)	0.259	ND (0.116)	ND (0.116)	0.0752 J	ND (0.116)	0.3342
VC-507	0.5 - 1 (ft)	10/2/2014	N	49.3	47.7	136 B	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.258	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.258
VC-507	1 - 2 (ft)	10/2/2014	N	62.8	58.7	157 B	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.361	ND (0.102)	ND (0.102)	0.0944 J	ND (0.102)	0.4554

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FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-507	2 - 3 (ft)	10/2/2014	N	89.7	89	187 B	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.786	ND (0.1)	ND (0.1)	0.242	ND (0.1)	1.028
VC-507	3 - 4 (ft)	10/2/2014	N	194	137	234 B	ND (0.268)	ND (0.268)	ND (0.268)	ND (0.268)	2.59	ND (0.268)	ND (0.268)	1.3	ND (0.268)	3.89
VC-507	4 - 5 (ft)	10/2/2014	N	271	142	228 B	ND (0.355)	ND (0.355)	ND (0.355)	ND (0.355)	1.59	ND (0.355)	ND (0.355)	4.72	ND (0.355)	6.31
VC-507	5 - 6 (ft)	10/2/2014	N	262	130	232 B	ND (0.169)	ND (0.169)	ND (0.169)	ND (0.169)	0.681	ND (0.169)	ND (0.169)	2.54	ND (0.169)	3.221
VC-507	6 - 8 (ft)	10/2/2014	FD	325	126	385 B	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)
VC-507	6 - 8 (ft)	10/2/2014	N	230	123	280 B	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)
VC-508	0 - 0.5 (ft)	9/11/2014	N	53.2	50.8	143	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	0.186	ND (0.122)	ND (0.122)	ND (0.122)	ND (0.122)	0.186
VC-508	0.5 - 1 (ft)	9/11/2014	N	51.5	47.4	140	ND (0.0974)	ND (0.0974)	ND (0.0974)	ND (0.0974)	0.274	ND (0.0974)	ND (0.0974)	ND (0.0974)	ND (0.0974)	0.274
VC-508	1 - 2 (ft)	9/11/2014	FD	69.2	68.4	147	ND (0.0994)	ND (0.0994)	ND (0.0994)	ND (0.0994)	0.61	ND (0.0994)	ND (0.0994)	0.41	ND (0.0994)	1.02
VC-508	1 - 2 (ft)	9/11/2014	N	63	57.3	140	ND (0.0931)	ND (0.0931)	ND (0.0931)	ND (0.0931)	0.476	ND (0.0931)	ND (0.0931)	0.926	ND (0.0931)	1.402
VC-508	2 - 3 (ft)	9/11/2014	N	64.6	60.4	141	ND (0.0919)	ND (0.0919)	ND (0.0919)	ND (0.0919)	0.447	ND (0.0919)	ND (0.0919)	0.339	ND (0.0919)	0.786
VC-508	3 - 4 (ft)	9/11/2014	N	103	101	198	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	1.35	ND (0.0863)	ND (0.0863)	0.285	ND (0.0863)	1.635
VC-508	4 - 5 (ft)	9/11/2014	N	135	139	227	ND (0.462)	ND (0.462)	ND (0.462)	ND (0.462)	4.42	ND (0.462)	ND (0.462)	3.34	ND (0.462)	7.76
VC-508	5 - 6 (ft)	9/11/2014	N	189	158	241	ND (0.0956)	ND (0.0956)	ND (0.0956)	ND (0.0956)	4.04	ND (0.0956)	ND (0.0956)	1.15	ND (0.0956)	5.19
VC-508	6 - 8 (ft)	9/11/2014	N	179	127	222	ND (0.0892)	ND (0.0892)	ND (0.0892)	ND (0.0892)	0.511	ND (0.0892)	ND (0.0892)	0.314	ND (0.0892)	0.825
VC-509	0 - 0.5 (ft)	10/21/2014	N	58.6	58.3	155 B	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.517	ND (0.117)	ND (0.117)	0.25	ND (0.117)	0.767
VC-509	0.5 - 1 (ft)	10/21/2014	N	103	106	206 B	ND (0.181)	ND (0.181)	ND (0.181)	ND (0.181)	1.28	ND (0.181)	ND (0.181)	0.32	ND (0.181)	1.6
VC-509	1 - 2 (ft)	10/21/2014	N	127	131	246 B	ND (0.284)	ND (0.284)	ND (0.284)	ND (0.284)	2.39	ND (0.284)	ND (0.284)	0.204 J	ND (0.284)	2.594
VC-509	2 - 3 (ft)	10/21/2014	N	122	138	245 B	ND (0.389)	ND (0.389)	ND (0.389)	ND (0.389)	3.03	ND (0.389)	ND (0.389)	0.343 J	ND (0.389)	3.373
VC-509	3 - 4 (ft)	10/21/2014	N	134	142	233 B	ND (0.454)	ND (0.454)	ND (0.454)	ND (0.454)	5.07	ND (0.454)	ND (0.454)	0.381 J	ND (0.454)	5.451
VC-509	4 - 5 (ft)	10/21/2014	FD	194	146	240 B	ND (0.465)	ND (0.465)	ND (0.465)	ND (0.465)	4.98	ND (0.465)	ND (0.465)	1.31	0.507	6.797
VC-509	4 - 5 (ft)	10/21/2014	N	191	151	238 B	ND (0.466)	ND (0.466)	ND (0.466)	ND (0.466)	4.78	ND (0.466)	ND (0.466)	1.13	ND (0.466)	5.91
VC-509	5 - 6 (ft)	10/21/2014	N	178	171	263 B	ND (0.386)	ND (0.386)	ND (0.386)	ND (0.386)	6.44	ND (0.386)	ND (0.386)	0.579	ND (0.386)	7.019
VC-509	6 - 8 (ft)	10/21/2014	N	254	146	238 B	ND (0.343)	ND (0.343)	ND (0.343)	ND (0.343)	2.85	ND (0.343)	ND (0.343)	4.26	1.23	8.34
VC-510	0 - 0.5 (ft)	10/29/2014	N	56.1	59.4	151	ND (0.131)	ND (0.131)	ND (0.131)	ND (0.131)	0.237	ND (0.131)	ND (0.131)	0.22	ND (0.131)	0.457
VC-510	0.5 - 1 (ft)	9/30/2014	N	54.5	50.1	149	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.208	ND (0.105)	ND (0.105)	ND (0.105)	ND (0.105)	0.208
VC-510	1 - 2 (ft)	9/30/2014	N	61.4	52	150	ND (0.0948)	ND (0.0948)	ND (0.0948)	ND (0.0948)	0.219	ND (0.0948)	ND (0.0948)	0.101	ND (0.0948)	0.32
VC-510	2 - 3 (ft)	9/30/2014	N	93.4	75.1	178	ND (0.0974)	ND (0.0974)	ND (0.0974)	ND (0.0974)	0.481	ND (0.0974)	ND (0.0974)	0.245	ND (0.0974)	0.726
VC-510	3 - 4 (ft)	9/30/2014	N	122	115	238	ND (0.0975)	ND (0.0975)	ND (0.0975)	ND (0.0975)	1.39	ND (0.0975)	ND (0.0975)	0.197	ND (0.0975)	1.587
VC-510	4 - 5 (ft)	9/30/2014	N	123	130	233 B	ND (0.185)	ND (0.185)	ND (0.185)	ND (0.185)	2.42	ND (0.185)	ND (0.185)	0.586	ND (0.185)	3.006
VC-510	5 - 6 (ft)	9/30/2014	FD	167	154	252 B	ND (0.478)	ND (0.478)	ND (0.478)	ND (0.478)	4.46	ND (0.478)	ND (0.478)	ND (0.478)	ND (0.478)	4.46
VC-510	5 - 6 (ft)	9/30/2014	N	169	146	246 B	ND (0.0933)	ND (0.0933)	ND (0.0933)	ND (0.0933)	4.4	ND (0.0933)	ND (0.0933)	0.5	ND (0.0933)	4.9
VC-510	6 - 8 (ft)	9/30/2014	N	182	162	258 B	ND (0.281)	ND (0.281)	ND (0.281)	ND (0.281)	4.74	ND (0.281)	ND (0.281)	0.447	ND (0.281)	5.187
VC-511	0 - 0.5 (ft)	10/1/2014	N	50.7	49.5	141 B	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	0.239	ND (0.107)	ND (0.107)	ND (0.107)	ND (0.107)	0.239
VC-511	0.5 - 1 (ft)	10/1/2014	N	56.1	50.6	142 B	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.247	ND (0.102)	ND (0.102)	0.1 J	ND (0.102)	0.347
VC-511	1 - 2 (ft)	10/1/2014	FD	65	58.8	156 B	ND (0.0959)	ND (0.0959)	ND (0.0959)	ND (0.0959)	0.3	ND (0.0959)	ND (0.0959)	0.448	ND (0.0959)	0.748
VC-511	1 - 2 (ft)	10/1/2014	N	64.9	58.1	151 B	ND (0.0971)	ND (0.0971)	ND (0.0971)	ND (0.0971)	0.253	ND (0.0971)	ND (0.0971)	ND (0.0971)	ND (0.0971)	0.253
VC-511	2 - 3 (ft)	10/1/2014	N	61.8	57.4	155 B	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.338	ND (0.102)	ND (0.102)	0.184	ND (0.102)	0.522
VC-511	3 - 4 (ft)	10/1/2014	N	63.5	59.4	156 B	ND (0.0958)	ND (0.0958)	ND (0.0958)	ND (0.0958)	0.414	ND (0.0958)	ND (0.0958)	0.139	ND (0.0958)	0.553
VC-511	4 - 5 (ft)	10/1/2014	N	96	94.4	205 B	ND (0.0908)	ND (0.0908)	ND (0.0908)	ND (0.0908)	0.711	ND (0.0908)	ND (0.0908)	0.0909	ND (0.0908)	0.8019
VC-511	5 - 6 (ft)	10/1/2014	N	128	143	252 B	ND (0.344)	ND (0.344)	ND (0.344)	ND (0.344)	3.88	ND (0.344)	ND (0.344)	0.237 J	ND (0.344)	4.117

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-511	6 - 8 (ft)	10/1/2014	N	175	167	261 B	ND (0.888)	ND (0.888)	ND (0.888)	ND (0.888)	9.8	ND (0.888)	ND (0.888)	1.21	ND (0.888)	11.01
VC-512	0 - 0.5 (ft)	10/21/2014	N	60.2	63.2	167 B	ND (0.135)	ND (0.135)	ND (0.135)	ND (0.135)	0.272	ND (0.135)	ND (0.135)	ND (0.135)	ND (0.135)	0.272
VC-512	0.5 - 1 (ft)	10/21/2014	N	56.5	57.8	157 B	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.302	ND (0.104)	ND (0.104)	ND (0.104)	ND (0.104)	0.302
VC-512	1 - 2 (ft)	10/21/2014	N	59.3	58.6	157 B	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.275	ND (0.112)	ND (0.112)	0.0687 J	ND (0.112)	0.3437
VC-512	2 - 3 (ft)	10/21/2014	FD	59.9	55.8	152 B	ND (0.0957)	ND (0.0957)	ND (0.0957)	ND (0.0957)	0.509	ND (0.0957)	ND (0.0957)	0.231	ND (0.0957)	0.74
VC-512	2 - 3 (ft)	10/21/2014	N	59.1	56.2	152 B	ND (0.0988)	ND (0.0988)	ND (0.0988)	ND (0.0988)	0.356	ND (0.0988)	ND (0.0988)	0.122	ND (0.0988)	0.478
VC-512	3 - 4 (ft)	10/21/2014	N	70.8	65.3	155	ND (0.0926)	ND (0.0926)	ND (0.0926)	ND (0.0926)	0.304	ND (0.0926)	ND (0.0926)	0.207	ND (0.0926)	0.511
VC-512	4 - 5 (ft)	10/21/2014	N	85.4	78.9	164	ND (0.654)	ND (0.654)	ND (0.654)	ND (0.654)	1.14	ND (0.654)	ND (0.654)	8.77	ND (0.654)	9.91
VC-512	5 - 6 (ft)	10/21/2014	N	96	88.9	175	ND (0.0912)	ND (0.0912)	ND (0.0912)	ND (0.0912)	0.43	ND (0.0912)	ND (0.0912)	0.0635 J	ND (0.0912)	0.4935
VC-512	6 - 8 (ft)	10/21/2014	N	194	137	247 B	ND (0.177)	ND (0.177)	ND (0.177)	ND (0.177)	2.33	ND (0.177)	ND (0.177)	2.01	ND (0.177)	4.34
VC-513	0 - 0.5 (ft)	10/21/2014	N	59.1	59.7	166 B	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.213	ND (0.118)	ND (0.118)	0.096 J	ND (0.118)	0.309
VC-513	0.5 - 1 (ft)	10/21/2014	N	64.7	59.1	152 B	ND (0.0978)	ND (0.0978)	ND (0.0978)	ND (0.0978)	0.439	ND (0.0978)	ND (0.0978)	0.211	ND (0.0978)	0.65
VC-513	1 - 2 (ft)	10/21/2014	N	108	108	191	ND (0.0845)	ND (0.0845)	ND (0.0845)	ND (0.0845)	2.54	ND (0.0845)	ND (0.0845)	0.675	ND (0.0845)	3.215
VC-513	2 - 3 (ft)	10/21/2014	N	143	141	226	ND (0.442)	ND (0.442)	ND (0.442)	ND (0.442)	4.11	ND (0.442)	ND (0.442)	ND (0.442)	ND (0.442)	4.11
VC-513	3 - 4 (ft)	10/21/2014	N	173	103	183	ND (0.401)	ND (0.401)	ND (0.401)	ND (0.401)	3.51	ND (0.401)	ND (0.401)	1.6	ND (0.401)	5.11
VC-513	4 - 5 (ft)	10/21/2014	N	183	112	192	ND (0.0758)	ND (0.0758)	ND (0.0758)	ND (0.0758)	1.5	ND (0.0758)	ND (0.0758)	1.08	ND (0.0758)	2.58
VC-513	5 - 6 (ft)	10/21/2014	N	310	127	236	ND (0.245)	ND (0.245)	ND (0.245)	ND (0.245)	1.07	ND (0.245)	ND (0.245)	3.09	1.29	5.45
VC-513	6 - 8 (ft)	10/21/2014	FD	279	116	431	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)	ND (0.0838)
VC-513	6 - 8 (ft)	10/21/2014	N	175	125	242	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)	ND (0.0856)
VC-514	0 - 0.5 (ft)	10/24/2014	N	51.5	54.9	150 B	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.307	ND (0.118)	ND (0.118)	ND (0.118)	ND (0.118)	0.307
VC-514	0.5 - 1 (ft)	10/24/2014	N	53.6	53.5	148 B	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.325	ND (0.11)	ND (0.11)	ND (0.11)	ND (0.11)	0.325
VC-514	1 - 2 (ft)	10/24/2014	N	60.8	56.8	157 B	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.243	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.243
VC-514	2 - 3 (ft)	10/24/2014	N	79.5	70.4	165 B	ND (0.0945)	ND (0.0945)	ND (0.0945)	ND (0.0945)	0.582	ND (0.0945)	ND (0.0945)	0.177	ND (0.0945)	0.759
VC-514	3 - 4 (ft)	10/24/2014	N	113	113	222 B	ND (0.0938)	ND (0.0938)	ND (0.0938)	ND (0.0938)	1.72	ND (0.0938)	ND (0.0938)	0.252	ND (0.0938)	1.972
VC-514	4 - 5 (ft)	10/24/2014	N	319	149	258	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	1.17	ND (0.0852)	ND (0.0852)	0.582	ND (0.0852)	1.752
VC-514	5 - 6 (ft)	10/24/2014	FD	278	135	266 B	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	ND (0.086)	1.73	ND (0.086)	1.73
VC-514	5 - 6 (ft)	10/24/2014	N	263	134	255	ND (0.0876)	ND (0.0876)	ND (0.0876)	ND (0.0876)	0.401	ND (0.0876)	ND (0.0876)	0.699	ND (0.0876)	1.1
VC-514	6 - 8 (ft)	10/24/2014	N	306	152	281 B	ND (1.67)	ND (1.67)	ND (1.67)	ND (1.67)	ND (1.67)	ND (1.67)	ND (1.67)	17	ND (1.67)	17
VC-515	0 - 0.5 (ft)	10/24/2014	N	47.8	50	140 B	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.254	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.254
VC-515	0.5 - 1 (ft)	10/24/2014	N	57.4	53.4	149 B	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.289	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.289
VC-515	1 - 2 (ft)	10/24/2014	FD	60.1	59.8	155 B	ND (0.0903)	ND (0.0903)	ND (0.0903)	ND (0.0903)	0.434	ND (0.0903)	ND (0.0903)	0.22	ND (0.0903)	0.654
VC-515	1 - 2 (ft)	10/24/2014	N	59.3	59.8	151 B	ND (0.091)	ND (0.091)	ND (0.091)	ND (0.091)	0.239	ND (0.091)	ND (0.091)	0.0801 J	ND (0.091)	0.3191
VC-515	2 - 3 (ft)	10/24/2014	N	87.2	88	189 B	ND (0.0938)	ND (0.0938)	ND (0.0938)	ND (0.0938)	1.04	ND (0.0938)	ND (0.0938)	0.209	ND (0.0938)	1.249
VC-515	3 - 4 (ft)	10/24/2014	N	386	132	232	ND (0.082)	ND (0.082)	ND (0.082)	ND (0.082)	0.814	ND (0.082)	ND (0.082)	2.34	ND (0.082)	3.154
VC-515	4 - 5 (ft)	10/24/2014	N	277	152	247	ND (0.54)	ND (0.54)	ND (0.54)	ND (0.54)	2.68	ND (0.54)	ND (0.54)	7.1	ND (0.54)	9.78
VC-515	5 - 6 (ft)	10/24/2014	N	190	120	208	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	0.0924	ND (0.0852)	0.0924
VC-515	6 - 8 (ft)	10/24/2014	N	197	129	229 B	ND (0.0869)	ND (0.0869)	ND (0.0869)	ND (0.0869)	ND (0.0869)	ND (0.0869)	ND (0.0869)	ND (0.0869)	ND (0.0869)	ND (0.0869)
VC-516	0 - 0.5 (ft)	10/24/2014	N	53.7	50.2	148 B	ND (0.103)	ND (0.103)	ND (0.103)	ND (0.103)	0.218	ND (0.103)	ND (0.103)	0.171	ND (0.103)	0.389
VC-516	0.5 - 1 (ft)	10/24/2014	N	53.8	52.3	154 B	ND (0.0997)	ND (0.0997)	ND (0.0997)	ND (0.0997)	0.243	ND (0.0997)	ND (0.0997)	ND (0.0997)	ND (0.0997)	0.243
VC-516	1 - 2 (ft)	10/24/2014	N	69.2	67.6	161 B	ND (0.0946)	ND (0.0946)	ND (0.0946)	ND (0.0946)	0.427	ND (0.0946)	ND (0.0946)	0.391	ND (0.0946)	0.818
VC-516	2 - 3 (ft)	10/24/2014	N	221	119	222 B	ND (0.0839)	ND (0.0839)	ND (0.0839)	ND (0.0839)	1.26	ND (0.0839)	ND (0.0839)	0.961	ND (0.0839)	2.221

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-516	3 - 4 (ft)	10/24/2014	N	275	129	257	ND (0.175)	ND (0.175)	ND (0.175)	ND (0.175)	1.29	ND (0.175)	ND (0.175)	1.86	ND (0.175)	3.15
VC-516	4 - 5 (ft)	10/24/2014	N	286	127	224	ND (0.869)	ND (0.869)	ND (0.869)	ND (0.869)	3.36	ND (0.869)	ND (0.869)	10.3	ND (0.869)	13.66
VC-516	5 - 6 (ft)	10/24/2014	N	149	132	227	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)	ND (0.0852)
VC-516	6 - 8 (ft)	10/24/2014	N	305	118	374 B	ND (0.0817)	ND (0.0817)	ND (0.0817)	ND (0.0817)	ND (0.0817)	ND (0.0817)	ND (0.0817)	ND (0.0817)	ND (0.0817)	ND (0.0817)
VC-601	0 - 0.5 (ft)	10/22/2014	N	46.8	43.6	119 B	ND (0.0996)	ND (0.0996)	ND (0.0996)	ND (0.0996)	0.199	ND (0.0996)	ND (0.0996)	0.402	ND (0.0996)	0.601
VC-601	0.5 - 1 (ft)	10/22/2014	N	58.5	45.4	47.7 B	ND (0.172)	ND (0.172)	ND (0.172)	ND (0.172)	0.135 J	ND (0.172)	ND (0.172)	2.15	ND (0.172)	2.285
VC-601	1 - 2 (ft)	10/22/2014	N	83.3	75.1	120 B	ND (0.229)	ND (0.229)	ND (0.229)	ND (0.229)	ND (0.229)	ND (0.229)	ND (0.229)	3.22	ND (0.229)	3.22
VC-601	2 - 3 (ft)	10/22/2014	N	94.8	157	188 B	ND (0.0639)	ND (0.0639)	ND (0.0639)	ND (0.0639)	0.47	ND (0.0639)	ND (0.0639)	0.591	ND (0.0639)	1.061
VC-601	3 - 4 (ft)	10/22/2014	N	169	320	227 B	ND (0.0798)	ND (0.0798)	ND (0.0798)	ND (0.0798)	2.79	ND (0.0798)	ND (0.0798)	1.06	ND (0.0798)	3.85
VC-601	4 - 5 (ft)	10/22/2014	N	223	210	255 B	ND (0.0874)	ND (0.0874)	ND (0.0874)	ND (0.0874)	2.41	ND (0.0874)	ND (0.0874)	0.715	ND (0.0874)	3.125
VC-601	5 - 6 (ft)	10/22/2014	N	376	201	251 B	ND (0.269)	ND (0.269)	ND (0.269)	ND (0.269)	2.39	ND (0.269)	ND (0.269)	1.61	ND (0.269)	4
VC-601	6 - 8 (ft)	10/22/2014	FD	1080	238	261 B	ND (0.0801)	ND (0.0801)	ND (0.0801)	ND (0.0801)	3.25	ND (0.0801)	ND (0.0801)	1.3	ND (0.0801)	4.55
VC-601	6 - 8 (ft)	10/22/2014	N	1440	217	293 B	ND (0.168)	ND (0.168)	ND (0.168)	ND (0.168)	4.93	ND (0.168)	ND (0.168)	2.32	ND (0.168)	7.25
VC-602	0 - 0.5 (ft)	10/29/2014	N	182	38.6	56.5	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	ND (0.0568)	0.411	ND (0.0568)	0.411
VC-602	0.5 - 1 (ft)	10/29/2014	N	29.6	31.3	201	ND (0.0572)	ND (0.0572)	ND (0.0572)	ND (0.0572)	0.0992	ND (0.0572)	ND (0.0572)	0.055 J	ND (0.0572)	0.1542
VC-602	1 - 2 (ft)	10/29/2014	N	46.9	44.3	89.1	ND (0.0637)	ND (0.0637)	ND (0.0637)	ND (0.0637)	0.261	ND (0.0637)	ND (0.0637)	0.194	ND (0.0637)	0.455
VC-602	2 - 3 (ft)	10/29/2014	FD	65.3	133	86.9	ND (0.0593)	ND (0.0593)	ND (0.0593)	ND (0.0593)	0.987	ND (0.0593)	ND (0.0593)	0.521	ND (0.0593)	1.508
VC-602	2 - 3 (ft)	10/29/2014	N	63.7	109	104	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	0.903	ND (0.0611)	ND (0.0611)	0.141	ND (0.0611)	1.044
VC-602	3 - 4 (ft)	10/29/2014	N	69.2	100	110	ND (0.0611)	ND (0.0611)	ND (0.0611)	ND (0.0611)	1.88	ND (0.0611)	ND (0.0611)	0.322	ND (0.0611)	2.202
VC-602	4 - 5 (ft)	10/29/2014	N	184	124	169	ND (0.0753)	ND (0.0753)	ND (0.0753)	ND (0.0753)	1.16	ND (0.0753)	ND (0.0753)	0.604	ND (0.0753)	1.764
VC-602	5 - 6 (ft)	10/29/2014	N	358	184	264	ND (0.0834)	ND (0.0834)	ND (0.0834)	ND (0.0834)	1.88	ND (0.0834)	ND (0.0834)	0.763	ND (0.0834)	2.643
VC-602	6 - 8 (ft)	10/29/2014	N	365	194	241	ND (0.333)	ND (0.333)	ND (0.333)	ND (0.333)	3.3	ND (0.333)	ND (0.333)	1.25	ND (0.333)	4.55
VC-603	0 - 0.5 (ft)	10/21/2014	N	71.8	62.6	171 B	ND (0.117)	ND (0.117)	ND (0.117)	ND (0.117)	0.274	ND (0.117)	ND (0.117)	0.086 J	ND (0.117)	0.36
VC-603	0.5 - 1 (ft)	10/21/2014	N	55.1	53	144 B	ND (0.102)	ND (0.102)	ND (0.102)	ND (0.102)	0.282	ND (0.102)	ND (0.102)	0.138	ND (0.102)	0.42
VC-603	1 - 2 (ft)	10/21/2014	FD	68.6	65	137	ND (0.0849)	ND (0.0849)	ND (0.0849)	ND (0.0849)	0.295	ND (0.0849)	ND (0.0849)	0.156	ND (0.0849)	0.451
VC-603	1 - 2 (ft)	10/21/2014	N	64.2	62.8	140	ND (0.0858)	ND (0.0858)	ND (0.0858)	ND (0.0858)	0.287	ND (0.0858)	ND (0.0858)	0.261	ND (0.0858)	0.548
VC-603	2 - 3 (ft)	10/21/2014	N	95.3	89.7	186 B	ND (0.0846)	ND (0.0846)	ND (0.0846)	ND (0.0846)	0.597	ND (0.0846)	ND (0.0846)	0.2	ND (0.0846)	0.797
VC-603	3 - 4 (ft)	10/21/2014	N	105	107	182	ND (0.0863)	ND (0.0863)	ND (0.0863)	ND (0.0863)	0.843	ND (0.0863)	ND (0.0863)	0.147	ND (0.0863)	0.99
VC-603	4 - 5 (ft)	10/21/2014	N	127	132	235 B	ND (0.335)	ND (0.335)	ND (0.335)	ND (0.335)	2.57	ND (0.335)	ND (0.335)	0.294 J	ND (0.335)	2.864
VC-603	5 - 6 (ft)	10/21/2014	N	147	392	210	ND (0.08)	ND (0.08)	ND (0.08)	ND (0.08)	2.01	ND (0.08)	ND (0.08)	0.269	ND (0.08)	2.279
VC-603	6 - 8 (ft)	10/21/2014	N	205	166	265 B	ND (0.697)	ND (0.697)	ND (0.697)	ND (0.697)	5.63	ND (0.697)	ND (0.697)	0.455 J	ND (0.697)	6.085
VC-604	0 - 0.5 (ft)	10/28/2014	N	51.9	51.2	144 B	ND (0.112)	ND (0.112)	ND (0.112)	ND (0.112)	0.324	ND (0.112)	ND (0.112)	1.25	ND (0.112)	1.574
VC-604	0.5 - 1 (ft)	10/28/2014	N	59.1	59.6	163 B	ND (0.125)	ND (0.125)	ND (0.125)	ND (0.125)	0.303	ND (0.125)	ND (0.125)	0.286	ND (0.125)	0.589
VC-604	1 - 2 (ft)	10/28/2014	N	64.4	50.5	133	ND (0.0997)	ND (0.0997)	ND (0.0997)	ND (0.0997)	0.231	ND (0.0997)	ND (0.0997)	0.275	ND (0.0997)	0.506
VC-604	2 - 3 (ft)	10/28/2014	N	45.7	47.2	125 B	ND (0.0991)	ND (0.0991)	ND (0.0991)	ND (0.0991)	0.501	ND (0.0991)	ND (0.0991)	0.286	ND (0.0991)	0.787
VC-604	3 - 4 (ft)	10/28/2014	N	98.1	97.3	185	ND (0.096)	ND (0.096)	ND (0.096)	ND (0.096)	0.86	ND (0.096)	ND (0.096)	0.35	ND (0.096)	1.21
VC-604	4 - 5 (ft)	10/28/2014	N	106	115	206 B	ND (0.18)	ND (0.18)	ND (0.18)	ND (0.18)	1.44	ND (0.18)	ND (0.18)	0.267	ND (0.18)	1.707
VC-604	5 - 6 (ft)	10/28/2014	N	135	148	248	ND (0.92)	ND (0.92)	ND (0.92)	ND (0.92)	5.33	ND (0.92)	ND (0.92)	20	ND (0.92)	25.33
VC-604	6 - 8 (ft)	10/28/2014	N	186	160	247 B	ND (0.0854)	ND (0.0854)	ND (0.0854)	ND (0.0854)	2.34	ND (0.0854)	ND (0.0854)	0.336	ND (0.0854)	2.676
VC-605	0 - 0.5 (ft)	11/3/2014	N	51.3	54.7	136	ND (0.145)	ND (0.145)	ND (0.145)	ND (0.145)	0.241	ND (0.145)	ND (0.145)	ND (0.145)	ND (0.145)	0.241
VC-605	0.5 - 1 (ft)	11/3/2014	N	57	57.3	155	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.21	ND (0.109)	ND (0.109)	ND (0.109)	ND (0.109)	0.21

TABLE - SEDIMENT ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Copper (mg/kg)	Lead (mg/kg)	Zinc (mg/kg)	Aroclor-1016 (mg/kg)	Aroclor-1221 (mg/kg)	Aroclor-1232 (mg/kg)	Aroclor-1242 (mg/kg)	Aroclor-1248 (mg/kg)	Aroclor-1254 (mg/kg)	Aroclor-1260 (mg/kg)	Aroclor-1262 (mg/kg)	Aroclor-1268 (mg/kg)	Total PCBs (mg/kg)
VC-605	1 - 2 (ft)	11/3/2014	FD	77.6	72.9	170	ND (0.0998)	ND (0.0998)	ND (0.0998)	ND (0.0998)	0.324	ND (0.0998)	ND (0.0998)	0.079 J	ND (0.0998)	0.403
VC-605	1 - 2 (ft)	11/3/2014	N	76.9	74.8	174	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.272	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.272
VC-605	2 - 3 (ft)	11/3/2014	N	102	101	198	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.94	ND (0.1)	ND (0.1)	0.201	ND (0.1)	1.141
VC-605	3 - 4 (ft)	11/3/2014	N	111	131	240	ND (0.0955)	ND (0.0955)	ND (0.0955)	ND (0.0955)	1.2	ND (0.0955)	ND (0.0955)	0.141	ND (0.0955)	1.341
VC-605	4 - 5 (ft)	11/3/2014	N	149	173	264	ND (0.366)	ND (0.366)	ND (0.366)	ND (0.366)	3.38	ND (0.366)	ND (0.366)	ND (0.366)	ND (0.366)	3.38
VC-605	5 - 6 (ft)	11/3/2014	N	207	166	249	ND (0.945)	ND (0.945)	ND (0.945)	ND (0.945)	7.56	ND (0.945)	ND (0.945)	1.21	ND (0.945)	8.77
VC-605	6 - 8 (ft)	11/3/2014	N	197	179	271	ND (0.0912)	ND (0.0912)	ND (0.0912)	ND (0.0912)	3.12	ND (0.0912)	ND (0.0912)	0.397	ND (0.0912)	3.517
VC-701	0 - 0.5 (ft)	10/27/2014	N	-	54.7	-	-	-	-	-	-	-	-	-	-	
VC-701	0.5 - 1 (ft)	10/27/2014	N	-	56.3	-	-	-	-	-	-	-	-	-	-	
VC-701	1 - 2 (ft)	10/27/2014	FD	-	57.9	-	-	-	-	-	-	-	-	-	-	
VC-701	1 - 2 (ft)	10/27/2014	N	-	61.4	-	-	-	-	-	-	-	-	-	-	
VC-701	2 - 3 (ft)	10/27/2014	N	-	373	-	-	-	-	-	-	-	-	-	-	
VC-701	3 - 4 (ft)	10/27/2014	N	-	83.6	-	-	-	-	-	-	-	-	-	-	
VC-702	0 - 0.5 (ft)	10/27/2014	N	-	53.6	-	-	-	-	-	-	-	-	-	-	
VC-702	0.5 - 1 (ft)	10/27/2014	N	-	51.2	-	-	-	-	-	-	-	-	-	-	
VC-702	1 - 2 (ft)	10/27/2014	N	-	63.9	-	-	-	-	-	-	-	-	-	-	
VC-702	2 - 3 (ft)	10/27/2014	N	-	81.7	-	-	-	-	-	-	-	-	-	-	
VC-702	3 - 4 (ft)	10/27/2014	FD	-	91	-	-	-	-	-	-	-	-	-	-	
VC-702	3 - 4 (ft)	10/27/2014	N	-	87.4	-	-	-	-	-	-	-	-	-	-	
VC-703	0 - 0.5 (ft)	10/27/2014	N	-	55.8	-	-	-	-	-	-	-	-	-	-	
VC-703	0.5 - 1 (ft)	10/27/2014	N	-	63	-	-	-	-	-	-	-	-	-	-	
VC-703	1 - 2 (ft)	10/27/2014	N	-	64.8	-	-	-	-	-	-	-	-	-	-	
VC-703	2 - 3 (ft)	10/27/2014	N	-	77.2	-	-	-	-	-	-	-	-	-	-	
VC-703	3 - 4 (ft)	10/27/2014	N	-	198	-	-	-	-	-	-	-	-	-	-	
VC-704	0 - 0.5 (ft)	10/28/2014	N	-	56.9	-	-	-	-	-	-	-	-	-	-	
VC-704	0.5 - 1 (ft)	10/28/2014	N	-	55.6	-	-	-	-	-	-	-	-	-	-	
VC-704	1 - 2 (ft)	10/28/2014	FD	-	65.1	-	-	-	-	-	-	-	-	-	-	
VC-704	1 - 2 (ft)	10/28/2014	N	-	63.4	-	-	-	-	-	-	-	-	-	-	
VC-704	2 - 3 (ft)	10/28/2014	N	-	68.7	-	-	-	-	-	-	-	-	-	-	
VC-704	3 - 4 (ft)	10/28/2014	N	-	107	-	-	-	-	-	-	-	-	-	-	
VC-705	0 - 0.5 (ft)	10/28/2014	N	-	48.2	-	-	-	-	-	-	-	-	-	-	
VC-705	0.5 - 1 (ft)	10/28/2014	N	-	49	-	-	-	-	-	-	-	-	-	-	
VC-705	1 - 2 (ft)	10/28/2014	N	-	60.5	-	-	-	-	-	-	-	-	-	-	
VC-705	2 - 3 (ft)	10/28/2014	FD	-	67.9	-	-	-	-	-	-	-	-	-	-	
VC-705	2 - 3 (ft)	10/28/2014	N	-	60.5	-	-	-	-	-	-	-	-	-	-	
VC-705	3 - 4 (ft)	10/28/2014	N	-	78.6	-	-	-	-	-	-	-	-	-	-	

TABLE - GROUNDWATER ANALYTICAL RESULTS
FORMER ANACONDA CABLE AND WIRE COMPANY - HASTINGS-ON-HUDSON, NEW YORK
AUGUST 2015

Location	Depth	Date	Sample Type	Beryllium (ug/L)	Copper (ug/L)	Lead (ug/L)	Zinc (ug/L)	Aroclor-1016 (ug/L)	Aroclor-1221 (ug/L)	Aroclor-1232 (ug/L)	Aroclor-1242 (ug/L)	Aroclor-1248 (ug/L)	Aroclor-1254 (ug/L)	Aroclor-1260 (ug/L)	Aroclor-1262 (ug/L)	Aroclor-1268 (ug/L)	Total PCBs (ug/L)
MW-01A	-	8/5/2014	N	ND (4)	ND (5)	ND (5)	ND (5)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)
MW-05	-	8/5/2014	N	ND (4)	6.14	ND (5)	16.2	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.826	ND (0.1)	ND (0.1)	0.826
MW-09	-	8/4/2014	FD	ND (4)	177	ND (5)	752	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	0.269	ND (0.05)	ND (0.05)	0.269
MW-09	-	8/4/2014	N	ND (4)	177	ND (5)	752	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	0.241	ND (0.05)	ND (0.05)	0.241
PDMW-16S	-	8/1/2014	N	ND (4)	ND (5)	ND (5)	ND (5)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)
PDMW-19S	-	8/4/2014	N	ND (4)	22.7	18.3	112	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	ND (0.1)	0.979	ND (0.1)	ND (0.1)	0.979
PDMW-20S	-	8/4/2014	N	ND (4)	ND (5)	ND (5)	ND (5)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)
PDMW-27S	-	12/2/2014	N	ND (4)	43.3	80.7	69.7	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	ND (0.05)	0.652	ND (0.05)	0.652

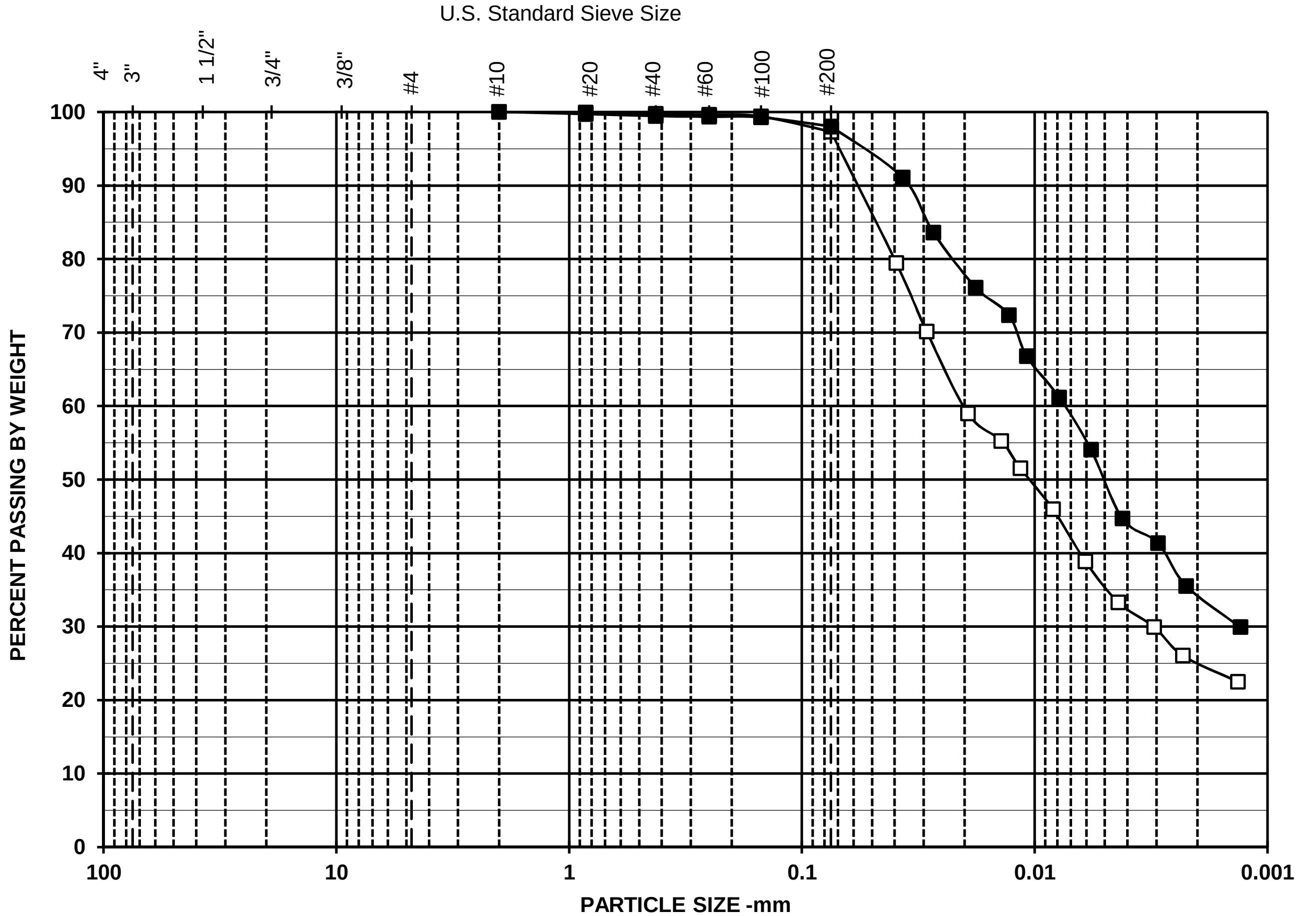
SECTION 3.7
GRAIN SIZE DISTRIBUTION

Haley & Aldrich #28612-317
Former Anaconda Wire and Cable Plant
LABORATORY TESTING DATA SUMMARY

BORING NO.	SAMPLE NO.	DEPTH (ft)	IDENTIFICATION TESTS				REMARKS
			WATER CONTENT (%)	USCS SYMB. (1)	SIEVE MINUS NO. 200 (%)	HYDRO. % MINUS 2 μm (%)	
	2242-102013-1155		114.8	OH	97.3	25	
	2242-102013-1240		167.0	OH	98.0	34	
	2242-102013-1540		129.3	OH	96.4	21	
	2242-102013-1640		81.2	OH	80.9	18	
	2242-102113-0810		101.9	OH	93.5	22	
	2242-102113-0840		109.1	OH	93.5	23	
	2242-102113-1222		113.9	OH	98.6	21	
	2242-102113-1602		104.9	OH	96.0	21	
	2242-102113-1528		124.4	OH	93.7	24	
	2242-102113-1357		133.2	OH	93.2	23	
	2242-102113-0933		94.7	OH	88.4	20	
	2242-102113-1438		133.8	OH	93.8	25	
	2242-102213-0812		72.6	OH	92.5	21	
	2242-102213-1245		110.8	OH	92.0	26	
	2242-102213-1136		128.2	OH	98.9	28	
	2242-102213-0951		91.5	OH	96.4	27	

Note: (1) USCS symbol based on visual observation and Sieve reported.

COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	



Symbol	□	■	○
Boring	2242-102013	2242-102013	
Sample	1155	1240	
Depth			
% +3"	0.0	0.0	
% Gravel	0.0	0.0	
% SAND	2.7	2.0	
%C SAND	0.0	0.0	
%M SAND	0.2	0.5	
%F SAND	2.4	1.4	
% FINES	97.3	98.0	
% -2μ	25	34	
D_{100} (mm)	2.00	2.00	
D_{60} (mm)	0.02	0.01	
D_{30} (mm)	0.00	0.00	
D_{10} (mm)			
Cc			
Cu			

Particle Size	PERCENT FINER		
(Sieve #)	□	■	○
4"			
3"			
1 1/2"			
3/4"			
3/8"			
4			
10	100.0	100.0	
20	99.9	99.7	
40	99.8	99.5	
60	99.6	99.4	
100	99.4	99.3	
200	97.3	98.0	

SYMBOL	w (%)	LL	PL	PI	USCS	DESCRIPTION AND REMARKS	Date Tested
□	114.8				OH	Gray, Organic silt	3/14/2014
■	167.0				OH	Gray, Organic silt	3/14/2014
○							

TerraSense, LLC	**Haley & Aldrich**
7788-14002	28612-317

PARTICLE SIZE DISTRIBUTION

Former Anaconda Wire and Cable Plant

Analysis File: 3SV-MasterRev3

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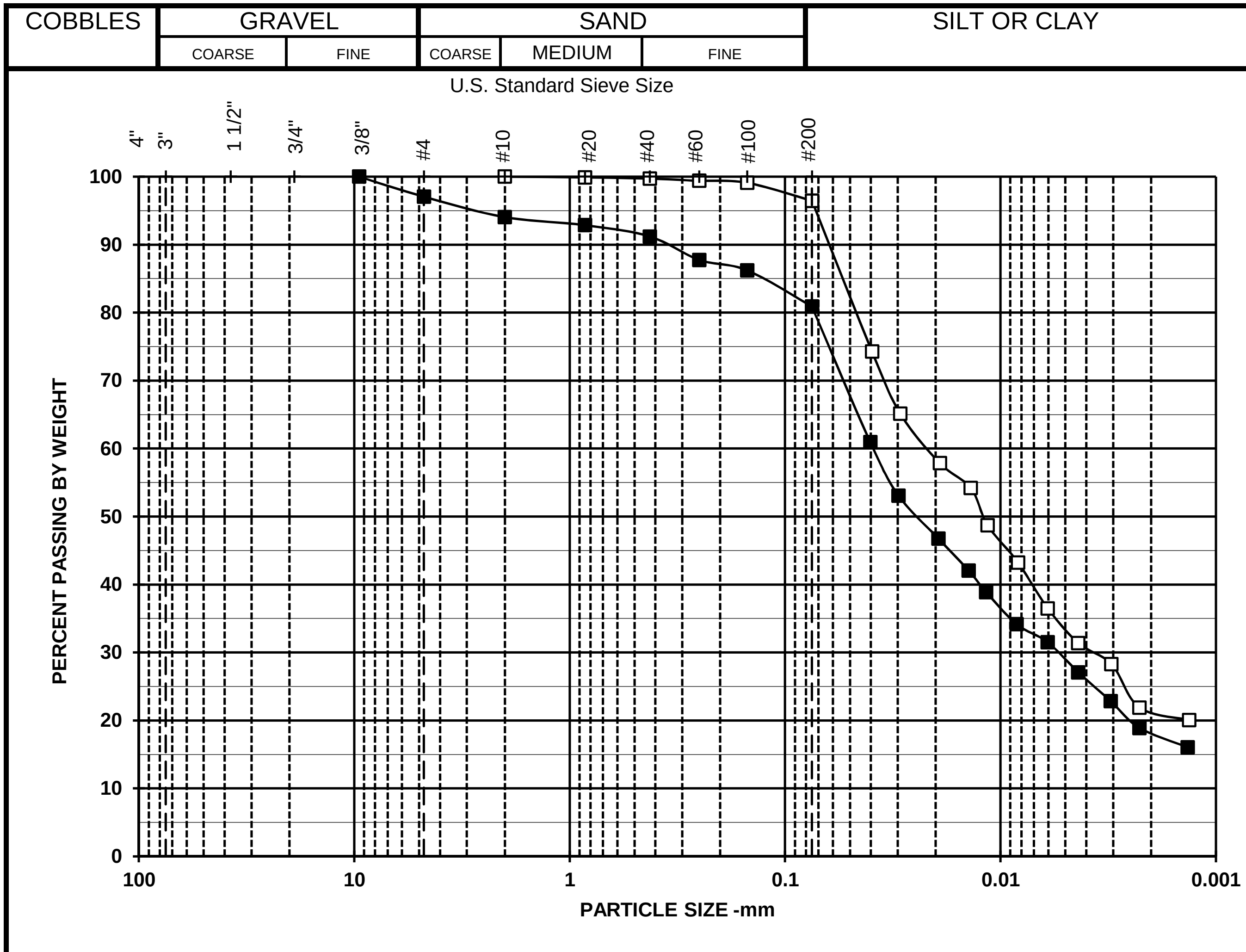

Symbol	□	■	○
Boring	2242-102013	2242-102013	
Sample	1540	1640	
Depth			
% +3"	0.0	0.0	
% Gravel	0.0	3.0	
% SAND	3.6	16.1	
%C SAND	0.0	3.0	
%M SAND	0.3	2.8	
%F SAND	3.3	10.3	
% FINES	96.4	80.9	
% -2μ	21	18	
D_{100} (mm)	2.00	9.50	
D_{60} (mm)	0.02	0.04	
D_{30} (mm)	0.00	0.01	
D_{10} (mm)			
Cc			
Cu			

Particle Size (Sieve #)	PERCENT FINER □	■	○
4"			
3"			
1 1/2"			
3/4"			
3/8"		100.0	
4		97.0	
10	100.0	94.0	
20	99.9	92.9	
40	99.7	91.2	
60	99.4	87.7	
100	99.1	86.2	
200	96.4	80.9	

SYMBOL	w (%)	LL	PL	PI	USCS	DESCRIPTION AND REMARKS	Date Tested
□	129.3				OH	Gray, Organic silt	3/14/2014
■	81.2				OH	Gray, Organic silt with sand	3/14/2014
○							

TerraSense, LLC	Haley & Aldrich
7788-14002	28612-317

PARTICLE SIZE DISTRIBUTION
Former Anaconda Wire and Cable Plant

Analysis File: 3SV-MasterRev3

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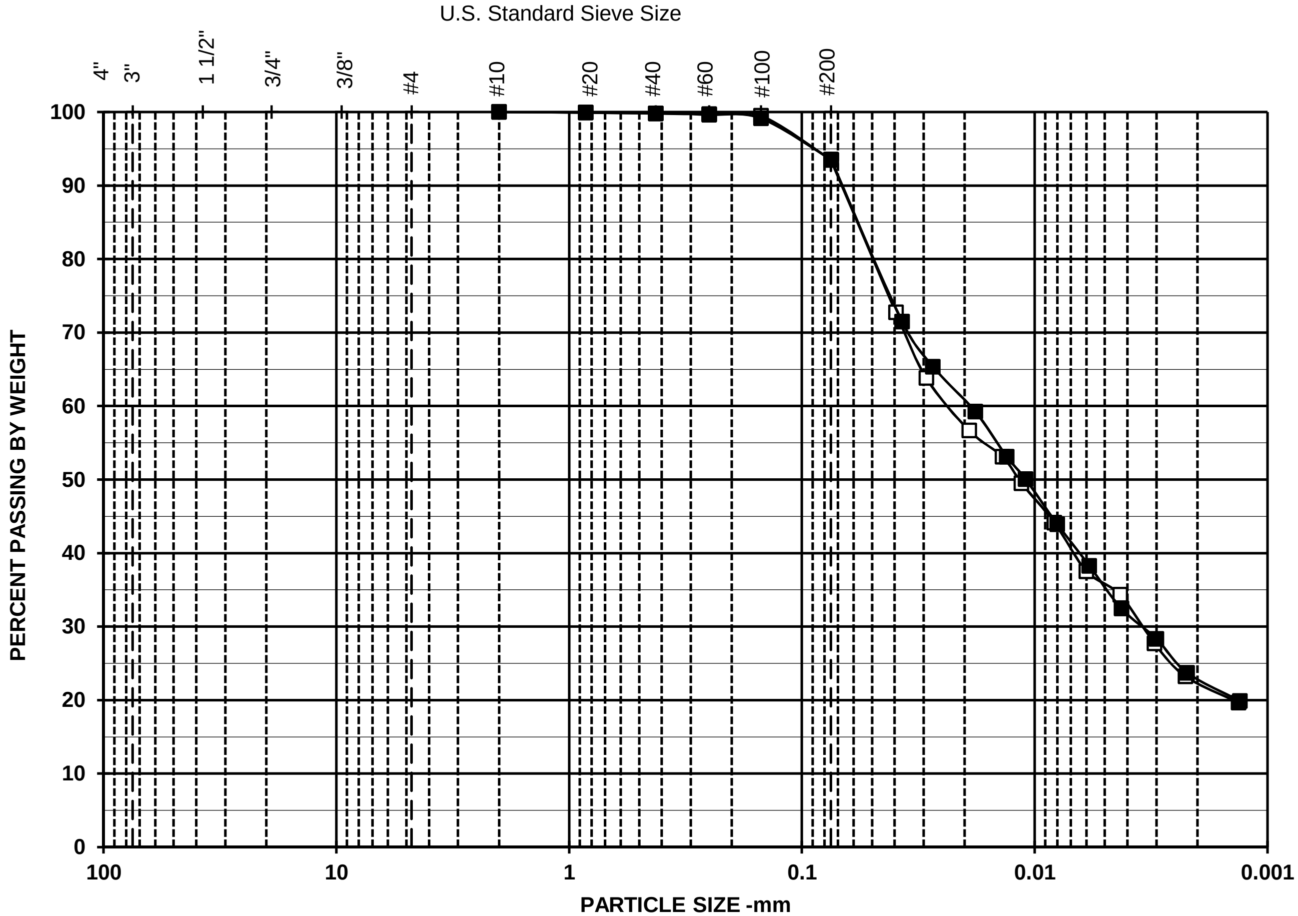
COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	



Symbol	□	■	○
Boring	2242-102113	2242-102113	
Sample	0810	0840	
Depth			
% +3"	0.0	0.0	
% Gravel	0.0	0.0	
% SAND	6.5	6.5	
%C SAND	0.0	0.0	
%M SAND	0.2	0.2	
%F SAND	6.3	6.3	
% FINES	93.5	93.5	
% -2μ	22	23	
D_{100} (mm)	2.00	2.00	
D_{60} (mm)	0.02	0.02	
D_{30} (mm)	0.00	0.00	
D_{10} (mm)			
Cc			
Cu			

Particle Size	PERCENT FINER		
(Sieve #)	□	■	○
4"			
3"			
1 1/2"			
3/4"			
3/8"			
4			
10	100.0	100.0	
20	99.9	99.9	
40	99.8	99.8	
60	99.7	99.6	
100	99.5	99.1	
200	93.5	93.5	

SYMBOL	w (%)	LL	PL	PI	USCS	DESCRIPTION AND REMARKS	Date Tested
□	101.9				OH	Gray, Organic silt	3/14/2014
■	109.1				OH	Gray, Organic silt	3/14/2014
○							

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PARTICLE SIZE DISTRIBUTION
Former Anaconda Wire and Cable Plant

Analysis File: 3SV-MasterRev3

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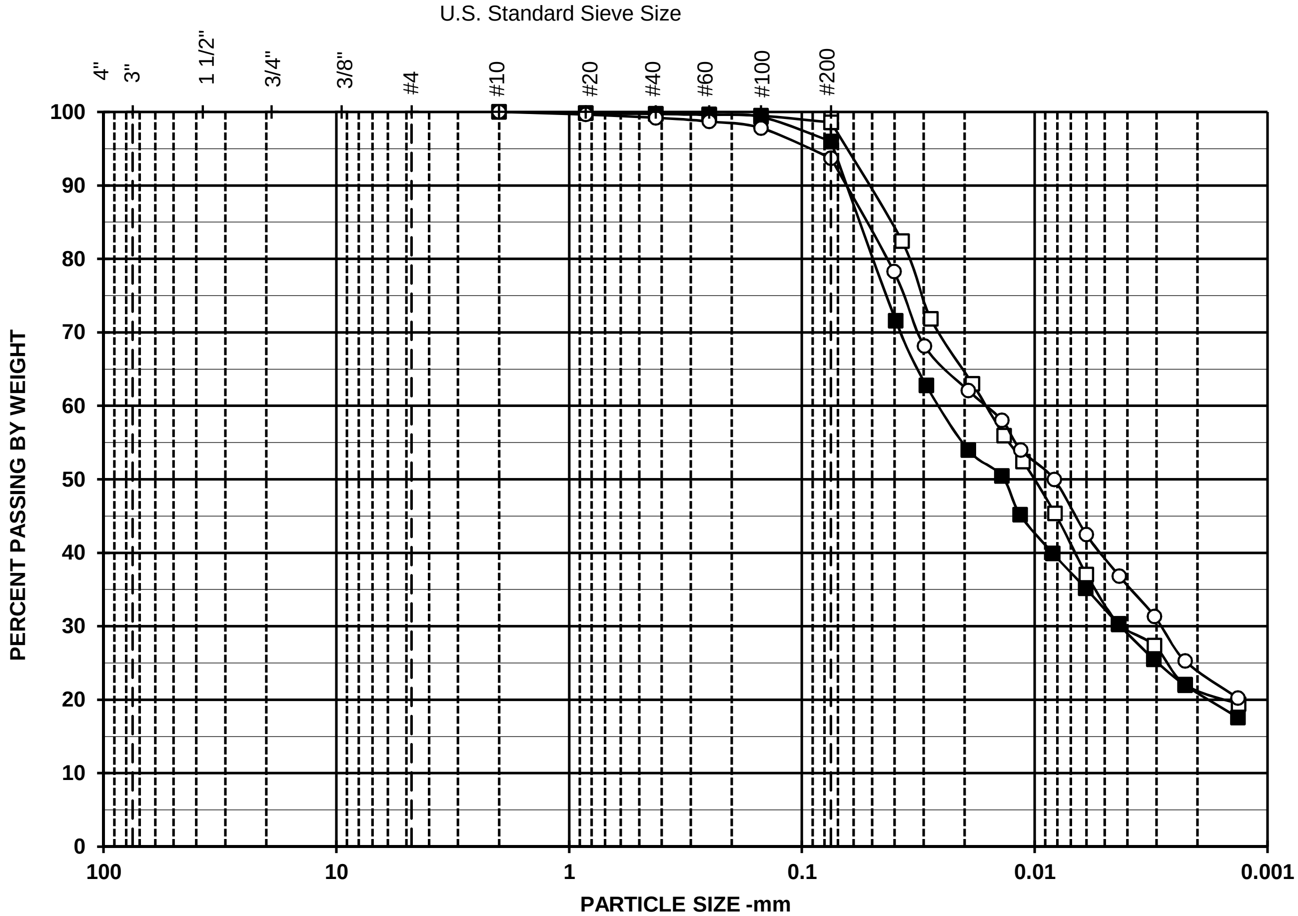
COBBLES	GRAVEL		SAND			SILT OR CLAY
	COARSE	FINE	COARSE	MEDIUM	FINE	



Symbol	□	■	○
Boring	2242-102113	2242-102113	2242-102113
Sample	1222	1602	1528
Depth			
% +3"	0.0	0.0	0.0
% Gravel	0.0	0.0	0.0
% SAND	1.4	4.0	6.3
%C SAND	0.0	0.0	0.0
%M SAND	0.2	0.3	0.8
%F SAND	1.2	3.7	5.5
% FINES	98.6	96.0	93.7
% -2μ	21	21	24
D_{100} (mm)	2.00	2.00	2.00
D_{60} (mm)	0.02	0.03	0.02
D_{30} (mm)	0.00	0.00	0.00
D_{10} (mm)			
Cc			
Cu			

Particle Size (Sieve #)	PERCENT FINER □	■	○
4"			
3"			
1 1/2"			
3/4"			
3/8"			
4			
10	100.0	100.0	100.0
20	99.9	99.8	99.7
40	99.8	99.7	99.2
60	99.7	99.6	98.7
100	99.5	99.3	97.8
200	98.6	96.0	93.7

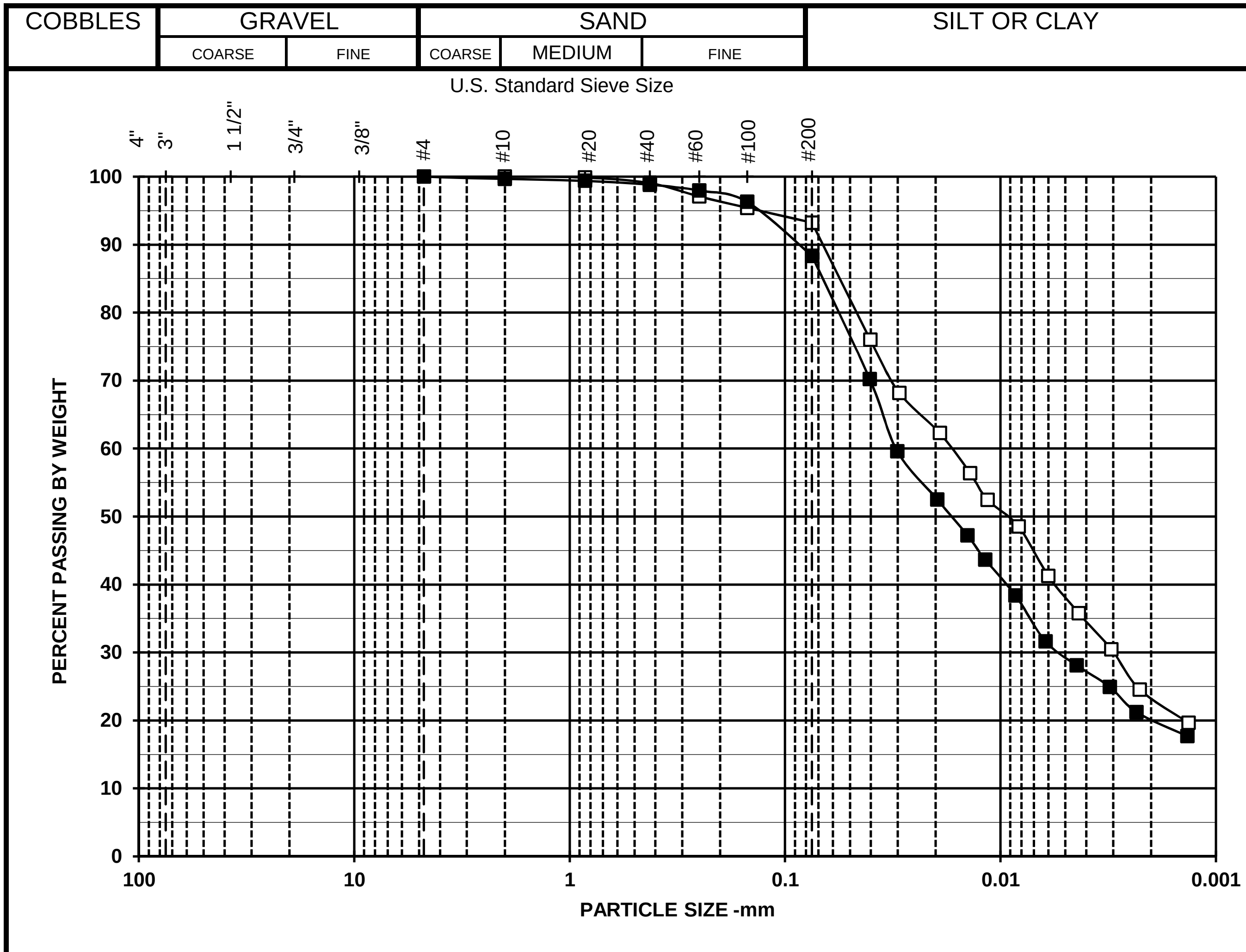
SYMBOL	w (%)	LL	PL	PI	USCS	DESCRIPTION AND REMARKS	Date Tested
□	113.9				OH	Gray, Organic silt	3/14/2014
■	104.9				OH	Gray, Organic silt	3/14/2014
○	124.4				OH	Gray, Organic silt	3/14/2014

TerraSense, LLC	**Haley & Aldrich**
7788-14002	28612-317

PARTICLE SIZE DISTRIBUTION
Former Anaconda Wire and Cable Plant

Analysis File: 3SV-MasterRev3

siev1d.xls 3/28/2014



Symbol	□	■	○
Boring	2242-102113	2242-102113	
Sample	1357	0933	
Depth			
% +3"	0.0	0.0	
% Gravel	0.0	0.0	
% SAND	6.8	11.6	
%C SAND	0.0	0.3	
%M SAND	1.0	0.9	
%F SAND	5.8	10.4	
% FINES	93.2	88.4	
% -2μ	23	20	
D_{100} (mm)	2.00	4.75	
D_{60} (mm)	0.02	0.03	
D_{30} (mm)	0.00	0.01	
D_{10} (mm)			
Cc			
Cu			

Particle Size (Sieve #)	PERCENT FINER □	■	○
4"			
3"			
1 1/2"			
3/4"			
3/8"			
4		100.0	
10	100.0	99.7	
20	99.9	99.4	
40	99.0	98.8	
60	97.1	98.0	
100	95.4	96.3	
200	93.2	88.4	

SYMBOL	w (%)	LL	PL	PI	USCS	DESCRIPTION AND REMARKS	Date Tested
□	133.2				OH	Gray, Organic silt	3/14/2014
■	94.7				OH	Gray, Organic silt	3/14/2014
○							

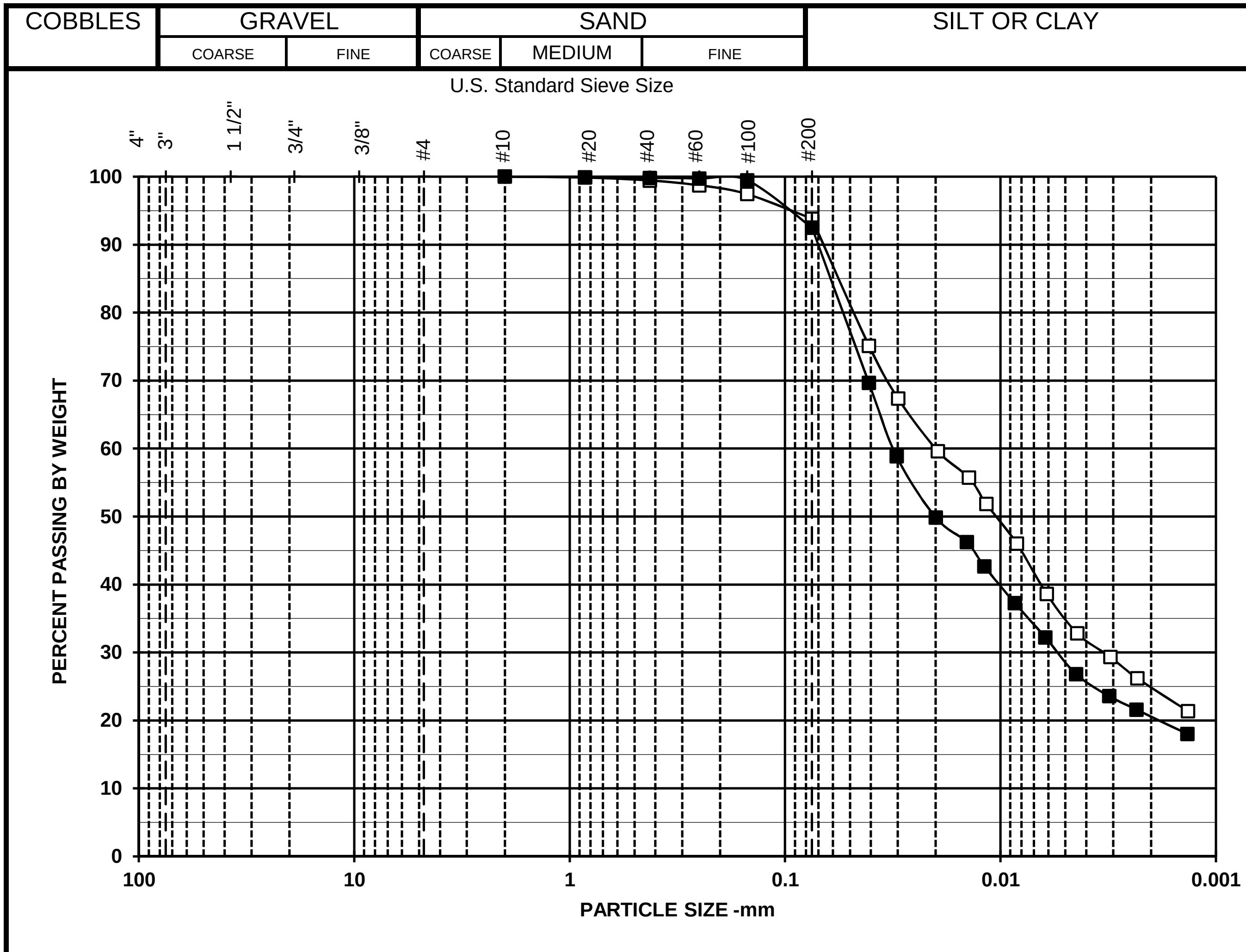
TerraSense, LLC	Haley & Aldrich
7788-14002	28612-317

PARTICLE SIZE DISTRIBUTION

Former Anaconda Wire and Cable Plant

Analysis File: 3SV-MasterRev3

siev1e.xls 3/28/2014



Symbol	□	■	○
Boring	2242-102113	2242-102213	
Sample	1438	0812	
Depth			
% +3"	0.0	0.0	
% Gravel	0.0	0.0	
% SAND	6.2	7.5	
%C SAND	0.0	0.0	
%M SAND	0.6	0.2	
%F SAND	5.6	7.3	
% FINES	93.8	92.5	
% -2μ	25	21	
D_{100} (mm)	2.00	2.00	
D_{60} (mm)	0.02	0.03	
D_{30} (mm)	0.00	0.01	
D_{10} (mm)			
Cc			
Cu			

Particle Size (Sieve #)	PERCENT FINER □	■	○
4"			
3"			
1 1/2"			
3/4"			
3/8"			
4			
10	100.0	100.0	
20	99.9	99.9	
40	99.4	99.8	
60	98.7	99.7	
100	97.4	99.5	
200	93.8	92.5	

SYMBOL	w (%)	LL	PL	PI	USCS	DESCRIPTION AND REMARKS	Date Tested
□	133.8				OH	Gray, Organic silt	3/14/2014
■	72.6				OH	Gray, Organic silt	3/14/2014
○							

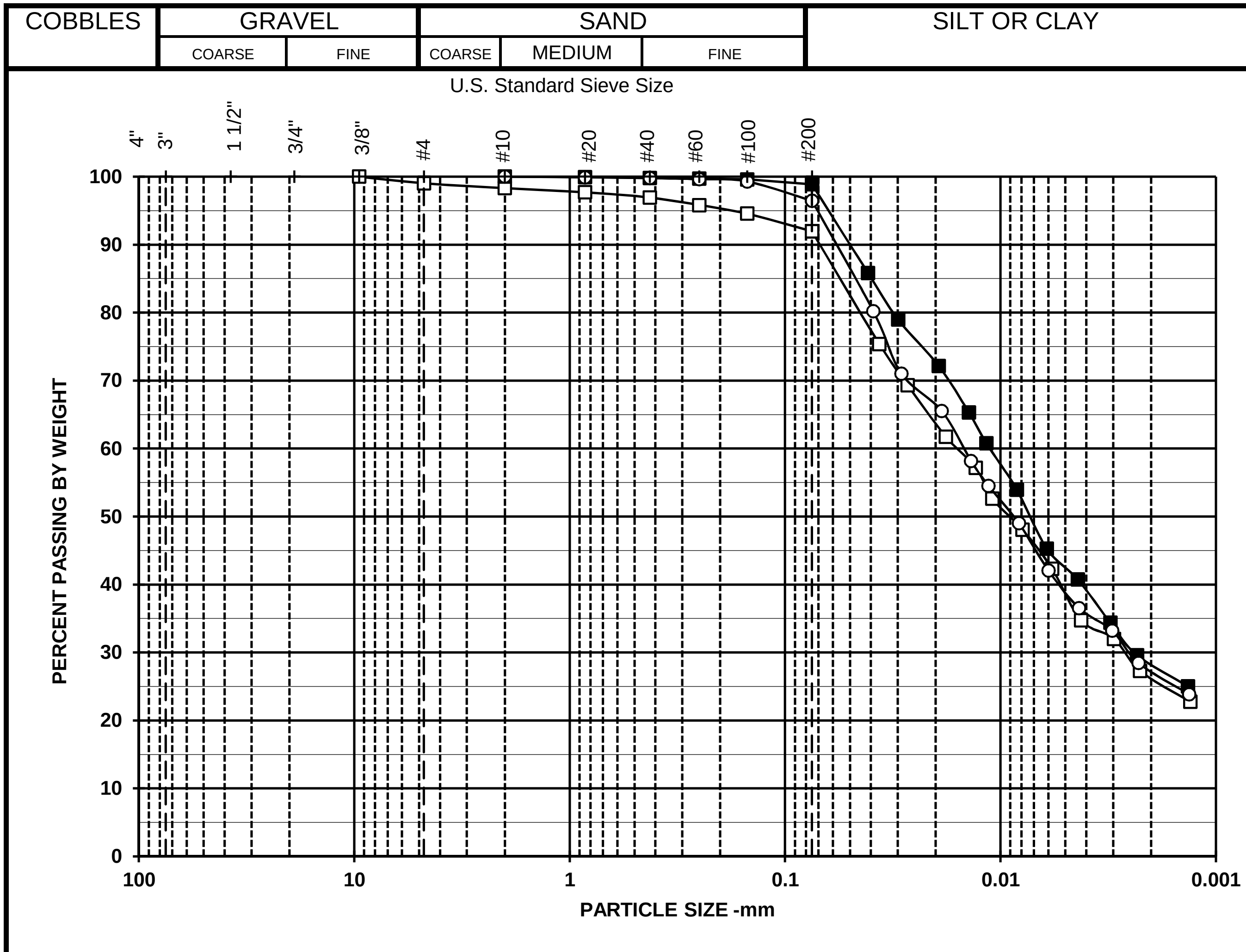
TerraSense, LLC	Haley & Aldrich
7788-14002	28612-317

PARTICLE SIZE DISTRIBUTION

Former Anaconda Wire and Cable Plant

Analysis File: 3SV-MasterRev3

siev1f.xls 3/28/2014



Symbol	□	■	○
Boring	2242-102213	2242-102213	2242-102213
Sample	1245	1136	0951
Depth			
% +3"	0.0	0.0	0.0
% Gravel	1.0	0.0	0.0
% SAND	7.0	1.1	3.6
%C SAND	0.7	0.0	0.0
%M SAND	1.4	0.2	0.2
%F SAND	5.0	0.9	3.4
% FINES	92.0	98.9	96.4
% -2µ	26	28	27
D_{100} (mm)	9.50	2.00	2.00
D_{60} (mm)	0.02	0.01	0.01
D_{30} (mm)	0.00	0.00	0.00
D_{10} (mm)			
Cc			
Cu			

Particle Size (Sieve #)	PERCENT FINER □	■	○
4"			
3"			
1 1/2"			
3/4"			
3/8"	100.0		
4	99.0		
10	98.3	100.0	100.0
20	97.7	99.9	99.9
40	96.9	99.8	99.8
60	95.8	99.7	99.6
100	94.6	99.6	99.3
200	92.0	98.9	96.4

SYMBOL	w (%)	LL	PL	PI	USCS	DESCRIPTION AND REMARKS	Date Tested
□	110.8				OH	Gray, Organic silt	3/14/2014
■	128.2				OH	Gray, Organic silt	3/14/2014
○	91.5				OH	Gray, Organic silt	3/14/2014

TerraSense, LLC	Haley & Aldrich
7788-14002	28612-317

PARTICLE SIZE DISTRIBUTION

Former Anaconda Wire and Cable Plant

Analysis File: 3SV-MasterRev3

siev1g.xls 3/28/2014

SECTION 3.8 APPENDICES

Kemron 2006 Solids Dewatering Report
“Hudson River Dewatering Study”

KEMRON ENVIRONMENTAL SERVICES

1359-A Ellsworth Industrial Boulevard • Atlanta, GA 30318 • TEL 404-636-0928 • FAX 404-636-7162

June 12, 2006

Ms. Kris Carbonneau
ENSR International
2 Technology Park Dr.
Westford, Massachusetts 01888
(978) 589-3377

Re: **Hudson River Dewatering Study**
Final Report Revision 1
KEMRON Project # SE0154

Dear Ms. Carbonneau:

KEMRON Environmental Services, Inc. (KEMRON) is pleased to present the results of the bench-scale treatability study conducted for ENSR. The treatability study was performed on sediment material sampled from a site located on the Hudson River (the Site). Testing was performed by KEMRON's Applied Technologies Group (ATG) located in Atlanta, Georgia. All testing was conducted in general accordance with the cost proposal developed by KEMRON and dated 22 August 2005.

The primary objective of the treatability study is evaluate dewatering techniques capable of reducing free liquid in the site material in order to pass Liquid Release Testing (LRT), and to evaluate the effectiveness of filtration applications at removing PCB containing sediments from liquids removed during dewatering activities. The treatability testing methods and results are summarized in the following sections of this letter report. Note that sampling services were provided during the treatability study; however, analytical data evaluation and presentation were included in the report.

Untreated Waste Characterization

In November 2005, KEMRON received six 5-gallon containers of sediment material from the site. The materials were delivered to KEMRON's Atlanta, Georgia facility by Federal Express. Upon receipt, each distinct site material was sieved through a pan sieve in order to remove debris larger than 0.5 inches in diameter. This particle size reduction is performed to facilitate full-scale treatment applications on a laboratory bench-scale. Table 1, attached to this report, summarizes the quantity of debris removed from each site material. The following is a summary of the information presented in Table 1.

TABLE 1				
Container No	As-Received Weight (lbs)	Debris Removed (lbs)	Available Sample (lbs)	Description
1	58	20	38	Brown with angular porous rock, glass
2	44	10	34	Black with angular porous rock, glass
3	58	8	50	Brown with smooth rounded stone
4	43	17	26	Black with angular rock
5	42	7	35	Brown with angular rock, glass, some sticks
6	55	20	35	Brown with angular rock, glass
Composite	300	82	218	Brown saturated sediment

Note that the tables included within this text are summaries of the attached documents. As such, tables within the text may not include all information presented in the attached documents.

Following debris removal, each site material was then composited together and homogenized to better ensure a uniform material for testing. Note that all testing was performed on this master composite material and/or materials developed from treatment of the composite sample. Homogenization was performed by placing the waste material into a large blending chamber and gently mixing with stainless steel utensils. Upon completion of homogenization, the master composite was placed into the original shipping containers and placed into refrigerated storage maintained at a temperature of four degrees Celsius (^{0}C).

Immediately upon completion of homogenization, KEMRON performed untreated characterization testing on the master composite material. Untreated characterization testing was performed to establish a baseline level of characteristics in the sediment and to help ensure that the material exhibits similar properties to those expected at the site. The following tests were performed on aliquots of the master composite sediment in accordance with the referenced test methods:

Parameter	Method
Paint Filter	EPA Method 9095
Moisture / Solids Content	ASTM D2216
Grain Size Distribution	ASTM D422
Atterberg Limits	ASTM D4318

In addition to the above geotechnical testing performed by KEMRON, aliquots of the untreated material were submitted to Severn Trent Laboratories (STL) located in Colchester, Vermont. Note that STL was selected by ENSR to perform all analytical testing for this project. KEMRON's responsibility related to analytical testing was to provide sampling services only. Inclusion and evaluation of the analytical testing in this report is outside the scope of the treatability study per the original agreement.

The results of geotechnical testing performed by KEMRON are presented in Table 2. The following is a summary of the data presented in Table 2:

TABLE 2		
TESTING PARAMETER	UNIT	UNTREATED COMPOSITE
Moisture Content	%	43.9
Solids Content	%	69.5
Particle Size Distribution		
Gravel	%	22.8
Sand	%	61.4
Silt	%	11.6
Clay	%	4.2
Atterberg Limits		
Liquid Limit		NL
Plastic Limit		NP
Plasticity Index		NA

Dewatering Evaluations

Dewatering evaluations were performed in order to evaluate methods and parameters for dewatering the site materials. Specifically, KEMRON evaluated gravity drainage and filter press dewatering techniques during this phase of the study. In addition to testing the as-received site material, KEMRON evaluated dewatering applications performed on the untreated composite material which was pretreated with diatomaceous earth (DE), to determine if pretreatment increased the performance of dewatering techniques applied to the site composite.

Gravity Drainage Testing
Gravity drainage testing was performed to evaluate the reduction in moisture content that can be achieved by allowing the site material to gravity drain while stockpiled during field operations. The primary advantages of the gravity drainage dewatering method include low operating cost and ease of operation. In order to simulate the process on the laboratory scale, laboratory testing was performed by allowing a known quantity of the sediment material to drain through a filter medium. Monitoring was performed over a 7-day test duration to evaluate the rate at which water drains from the sample. Additionally, KEMRON performed moisture / solids content testing on the test samples at 3, 5, and 7 days of treatment.

Table 3 summarizes the results of gravity drainage testing performed on the untreated composite material and the DE pretreated composite material. The following is a summary of the data presented in Table 3:

TABLE 3			
TESTING PARAMETER	UNIT	RESULTS	
		GD-001	GD-002
Initial Untreated Weight	g	1005.7	1048.2
Conditioner Used		None	5% DE (1)
Initial Moisture Content (ASTM)	%	43.9	43.9
Initial Solids Content	%	69.5	69.5
Final Weight of Cake	g	929.9	1003.8
Effluent	g	27.56	12.05
Moisture Content (ASTM)			
3 Day	%	29.48	36.17
5 Day	%	29.33	35.03
7 Day	%	28.89	42.02
Solids Content			
3 Day	%	77.23	73.44
5 Day	%	77.32	74.06
7 Day	%	77.59	70.41
Paint Filter Test	Pass / Fail	Fail	Fail
Liquid Release Test	Pass / Fail	Fail	Fail

(1) DE – diatomaceous earth

Note that due to the relatively low quantity of effluent removed from the as-received site material, GD-001, and because the addition of conditioner did not improve the test results, GD-002, it was determined that further gravity drainage testing would not be performed. Complete data reports for all testing performed by KEMRON are included as Attachment B.

Filter Press Testing

Filter press testing was performed to evaluate the reduction in moisture content achieved by the application of a positive pressure to the sediment sludge. Bench-scale testing was performed at several different positive pressures using a Baroid filter press apparatus. The Baroid filter press apparatus consists of a material reservoir mounted in a frame, a filtering medium, a means of capturing the filtrate, and attachments for a compressed air-supply line. The filtering medium had a pore size of approximately 24 micrometers (µm). KEMRON performed a total of 4 filter press tests, labeled FP-001 through FP-004.

Filter press testing was performed by placing pre-weighed aliquots of sediment into the reservoir and then introducing pressurized air into the system. Testing was continued under these conditions until pressure breakthrough occurred. Breakthrough was identified as the point at which pressure was released from the apparatus through cracking of the filter cake. Upon release of pressure, testing was terminated and the apparatus was dismantled. The weight of the filter cake and the volume of filtrate were recorded. Aliquots of each filter cake were then sampled for moisture content testing.

The results of filter press testing are summarized in Table 4.

TABLE 4					
TESTING PARAMETER	UNIT	RESULTS			
		FP-001	FP-002	FP-003	FP-004
Initial Untreated Weight	g	464.22	454.33	455.78	455.1
Initial Moisture Content	%	43.9	43.9	43.9	43.9
Initial Solids Content	%	69.5	69.5	69.5	69.5
Gauge Pressure	lbs/in^2	25	50	75	100
Run Time	min	2.5	2.0	1.5	1.0
Final Weight of Cake	g	400.3	390.8	387.6	378.10
Final Moisture Content	%	33.38	27.77	26.00	24.65
Final Solids Content	%	74.98	78.26	79.37	80.22
Paint Filter Test	Pass /	Fail	Pass	Pass	Pass
Liquid Release Test	Pass /	Fail	Fail	Fail	Pass

Review of the data presented in Table 4 indicate that filter press testing using a positive pressure of 100 psi results in a treated filter cake capable of passing both paint filter and liquid release testing. Additionally, the run time for this treatment was approximately 1 minute indicating that this material is relatively easily treated using full-scale treatment applications similar to filter press testing. Note that due to the successful results from the 100 psi filter press treatment, testing using a pretreatment additive was eliminated from this study.

Water Treatment Filtration Evaluations

Filtrate from Dewatering Activities

Based on the results from dewatering evaluations, KEMRON applied filter press treatment at 100 psi to develop a bulk filtrate material for filtration evaluations. Specifically, replicate batches of the site sediment were treated using the filter press application in order to create a sufficient volume of filtrate for additional testing.

Once developed, KEMRON homogenized the filtrate material to ensure the entire quantity of filtrate was similar in nature. Following homogenization, KEMRON performed total dissolved solids (TDS) and total suspended solids (TSS) content testing on the filtrate material. In accordance with EPA test methods 160.0 and 161 TSS and TDS evaluations are typically performed using a filter media with a nominal pore size of 1.1 µm. In order to evaluate the potential effectiveness of filtration applications at reducing groundwater contamination concentrations, TSS and TDS testing were performed using 4 different filter media. The results of TSS and TDS evaluations are presented in Table 5. The following is a summary of the data in Table 5:

TABLE 5		
SAMPLE ID	RESULTS (mg/L)	
	TSS	TDS
SE0154-002 (0.45 µm Filter)	12	3,996
SE0154-003 (1.2 µm Filter)	13	3,772
SE0154-004 (5.0 µm Filter)	14	3,855
SE0154-005 (11.0 µm Filter)	18	4,122

Review of the data in Table 5 indicate very similar TSS and TDS concentrations were reported regardless of the filter media used in testing.

In addition to TSS and TDS testing, aliquots of each filtered test material, as well as an aliquot of the unfiltered filtrate material were forwarded to STL laboratories for analytical testing.

Site Groundwater
KEMRON was provided an additional water material for filtration evaluations. This material was identified as site groundwater. Testing of this groundwater followed the testing protocol outlined for the evaluation of the filtrate developed from dewatering activities applied to the site sediment material. The results of TSS and TDS testing performed on the site groundwater are presented in Table 6. The following is a summary of Table 6:

TABLE 6		
SAMPLE ID	RESULTS (mg/L)	
	TSS	TDS
SE0154-007 (0.45 µm Filter	9.7	3,760
SE0154-008 (1.2 µm Filter	24	3,746
SE0154-009 (5.0 µm Filter	8.7	3,719
SE0154-010 (11.0 µm Filter	11	3,695

As seen in the testing of the dewatering filtrate, the results of TSS and TDS testing performed on the site groundwater are very similar regardless of the filter media used. Additionally, the TSS and TDS results are very similar between the dewatering filtrate and the site groundwater. Aliquots of each filtered site groundwater, as well as an unfiltered aliquot, were submitted to STL laboratories for analytical testing.

Discussion of Results

The results of dewatering evaluations indicate that gravity drainage treatment performed on a bench-scale produced a cake material with a moisture content of approximately 29%, which failed both paint filter and liquid release testing. Treatment of the site sediment, using a dewatering application at 50 psi positive pressure resulted in a cake material with a moisture content of approximately 28% which is capable of passing paint filter but not liquid release testing. At a positive pressure of 100 psi the treated filter cake exhibits a moisture content of 24.65% and passes both paint filter and liquid release testing.

While KEMRON has identified that the use of a dewatering application utilizing a positive pressure of 50 psi, FP-002, results in a treated material which passes paint filter testing, it would be worthwhile noting that bench-scale gravity drainage treatment, GD-001, produced a treated material with a moisture content less than 4% higher than that in the FP-002 material. KEMRON's experience is that gravity drainage is often more effective in a full-scale application. Additional moisture removal may be realized on a full-scale basis due to overburden pressure created by large stockpiles, evaporation, and tilling or manipulation of the stockpile which is not performed during laboratory testing.

Testing of the filtrate material developed using a positive pressure of 100 psi indicated that filtration using filter media with pore sizes ranging from 0.45 to 11.0 µm resulted in very similar TSS and TDS values. Additionally, groundwater collected from the site exhibited TSS and TDS results very similar to the filtrate developed during the dewatering study.

At this time KEMRON has not reviewed any analytical data developed by STL. As such, KEMRON cannot determine the effectiveness of the testing protocol on reducing concentrations of contaminants in the site materials.

Closure

KEMRON Environmental Services, Inc. appreciates the opportunity to provide ENSR with treatability testing services. If you have any questions, or require additional information, please call either of the undersigned at (404) 636-0928.

Sincerely,
KEMRON Environmental Services, Inc.

Mark Clark
Applied Technologies Group
Project Manager

Kelly Clemons
Applied Technologies Group
Program Manager

Attachments

TREATABILITY STUDY

9.1 Introduction

This Treatability study has been prepared for the design of the temporary remediation of adversely impacted soils and groundwater at the former Anaconda Wire and Cable Plant Site in Hastings-on-the-Hudson (the Site). The soils and groundwater to be treated are those associated with the excavation for Operable Unit No. 1 (OU-1). This Treatability study provides documentation of filter press and filtration simulations performed in 2005 for soils and groundwater that are potentially impacted with polychlorinated biphenyls (PCBs).

The objectives of this treatability study as described in the Remedial Design Work Plan (Parsons, September 2004) are to

- Provide and evaluation to determine treatment options available for the construction water expected during excavation;
- Evaluate the feasibility and the cost associated with these options; and
- Determine potential disposal alternatives.

9.2 Sampling Methods

Haley & Aldrich, Inc. collected representative soil and water samples to be used in a treatability tests. Saturated soil samples were collected at several locations over a four to thirteen (13) foot below ground surface interval from test pits to fill six 5-gallon containers. Saturated soils were encountered at or below four feet below ground surface. The six containers were then shipped via Federal Express to KEMRON's Atlanta, Georgia facility for treatability tests.

Groundwater samples were collected from groundwater monitoring wells and from a pumping test performed at the site. These samples were shipped to STL for analytical testing for PCBs and metals in accordance with EPA method 8082B and EPA method 6010B/7470 respectively. The remainder of the collected samples were then compiled and sent to KEMRON for treatability testing.

9.3 Treatability Testing Procedures and Results

Kemron Environmental Services, Inc (KEMRON) performed treatability tests on sediment material samples from a site located on he Hudson River. Testing was performed by KEMRON's Applied Technologies Group (ATG) located in Atlanta, Georgia. All testing was conducted in general accordance with the cost proposal developed by KEMRON and dated 22 August 2005.

Untreated Waste Characterization

In November 2005, KEMRON received six 5-gallon containers of sediment material from the site. The materials were delivered to KEMRON's Atlanta, Georgia facility by Federal Express. Upon receipt, each distinct site material was sieved through a pan sieve in order to remove debris larger than 0.5 inches in diameter. This particle size reduction is performed to facilitate full-scale treatment applications on a laboratory bench-scale.

Following debris removal, each site material was then composited together and homogenized to better ensure a uniform material for testing. Note that all testing was performed on this master composite material and/or materials developed from treatment of the composite sample. Homogenization was performed by placing the waste material into a large blending chamber and gently mixing with stainless steel utensils. Upon completion of homogenization, the master composite was placed into the original shipping containers and placed into refrigerated storage maintained at a temperature of four degrees Celsius (^{o}C). Immediately upon completion of homogenization, KEMRON performed untreated characterization testing on the master composite material. Untreated characterization testing was performed to establish a baseline level of characteristics in the sediment and to help ensure that the material exhibits similar properties to those expected at the site. The following tests were performed on aliquots of the master composite sediment in accordance with the referenced test methods:

Parameter	**Method**
Paint Filter	EPA Method 9095
Moisture / Solids Content	ASTM D2216
Grain Size Distribution	ASTM D422
Atterberg Limits	ASTM D4318

The results of the untreated composite are as follows:

Table IX-1.1 - Untreated Material Characterization
Summary of Physical Analyses

TESTING PARAMETER	UNIT	UNTREATED COMPOSITE
Moisture Content	%	43.9
Solids Content	%	69.5
Particle Size Distribution		
Gravel	%	22.8
Sand	%	61.4
Silt	%	11.6
Clay	%	4.2
Atterberg Limits		
Liquid Limit		NL
Plastic Limit		NP
Plasticity Index		NA

In addition to the above geotechnical testing performed by KEMRON, aliquots of the untreated material were submitted to Severn Trent Laboratories (STL) located in Colchester, Vermont. These analytical testing results can be found in Appendix IX-2.

Dewatering Evaluations

Dewatering evaluations were performed in order to evaluate methods and parameters for dewatering the site materials. Specifically, KEMRON evaluated gravity drainage and filter press dewatering techniques during this phase of the study. In addition to testing the as-received site material, KEMRON evaluated dewatering applications performed on the untreated composite material which was pretreated with diatomaceous earth (DE), to determine if pretreatment increased the performance of dewatering techniques applied to the site composite.

Gravity Drainage Testing

Gravity drainage testing was performed to evaluate the reduction in moisture content that can be achieved by allowing the site material to gravity drain while stockpiled during field operations. The primary advantages of the gravity drainage dewatering method include low operating cost and ease of operation. In order to simulate the process on the laboratory scale, laboratory testing was performed by allowing a known quantity of the sediment material to drain through a filter medium. Monitoring was performed over a 7-day test duration to evaluate the rate at which water drains from the sample. Additionally, KEMRON performed moisture / solids content testing on the test samples at 3, 5, and 7 days of treatment. Table IX-1.2 summarizes the results of the gravity drainage testing performed on the untreated composite material and the DE pretreated composite material.

Table IX-1.2 - Dewatering Evaluations

Summary of Gravity Drainage Testing

TESTING PARAMETER	UNIT	RESULTS	
		GD-001	GD-002
Initial Untreated Weight	g	1005.7	455.1
Conditioner Used		None	5% DE (1)
Initial Moisture Content (ASTM)	%	43.9	43.9
Initial Solids Content	%	69.5	69.5
Final Weight of Cake	g	929.9	1.0
Effluent	g	27.56	378.10
Moisture Content (ASTM)			
3 Day	%	29.48	77.23
5 Day	%	29.33	77.32
7 Day	%	28.89	77.59
Final Solids Content			
3 Day	%	36.17	73.44
5 Day	%	35.03	74.06
7 Day	%	42.02	70.41
Paint Filter Test	Pass / Fail	Fail	Fail
Liquid Release Test	Pass / Fail	Fail	Fail

(1) Diatomaceous Earth was added to the untreated material on a by-weight basis. For a 5% addition 5 grams of DE was added to every 100 grams of untreated material and blended prior to testing.

Filter Press Testing

Filter press testing was performed to evaluate the reduction in moisture content achieved by the application of a positive pressure to the sediment sludge. Bench-scale testing was performed at several different positive pressures using a Baroid filter press apparatus. The Baroid filter press apparatus consists of a material reservoir mounted in a frame, a filtering medium, a means of capturing the filtrate, and attachments for a compressed air-supply line. The filtering medium had a pore size of approximately 24 micrometers (μm). KEMRON performed a total of 4 filter press tests, labeled FP-001 through FP-004. Filter press testing was performed by placing pre-weighed aliquots of sediment into the reservoir and then introducing pressurized air into the system. Testing was continued under these conditions until pressure breakthrough occurred. Breakthrough was identified as the point at which pressure was released from the apparatus through cracking of the filter cake. Upon release of pressure, testing was terminated and the apparatus was dismantled. The weight of the filter cake and the volume of filtrate were recorded. Aliquots of each filter cake were then sampled for moisture content testing. The results of filter press testing are as follows:

Table IX-1.3 - Dewatering Evaluations

Summary of Filter Press Testing

		RESULTS			
	UNIT	**FP-001**	**FP-002**	**FP-003**	**FP-004**
Initial Untreated Weight	g	464.22	454.33	455.78	455.1
Initial Moisture Content (ASTM)	%	43.9	43.9	43.9	43.9
Initial Solids Content	%	69.5	69.5	69.5	69.5
Gauge Pressure	lbs/in^2	25	50	75	100
Run Time	min	2.5	2.0	1.5	1.0
Final Weight of Cake	g	400.3	390.8	387.6	378.10
Final Moisture Content (ASTM)	%	27.77	33.38	26.00	24.65
Final Solids Content	%	78.26	74.98	79.37	80.22
Paint Filter Test	Pass / Fail	Fail	Pass	Pass	Pass
Liquid Release Test	Pass / Fail	Fail	Fail	Fail	Pass

Review of the data presented in Table IX-1.3 indicate that filter press testing using a positive pressure of 100 psi results in a treated filter cake capable of passing both paint filter and liquid release testing. Additionally, the run time for this treatment was approximately 1 minute indicating that this material is relatively easily treated using full-scale treatment applications similar to filter press testing.

Water Treatment Filtration Evaluations

Filtrate from Dewatering Activities Based on the results from dewatering evaluations, KEMRON applied filter press treatment at 100 psi to develop a bulk filtrate material for filtration evaluations. Specifically, replicate batches of the site sediment were treated using the filter press application in order to create a sufficient volume of filtrate for additional testing.

Once developed, KEMRON homogenized the filtrate material to ensure the entire quantity of filtrate was similar in nature. Following homogenization, KEMRON performed total dissolved solids (TDS) and total suspended solids (TSS) content testing on the filtrate material. In accordance with EPA test methods 160.0 and 161 TSS and TDS evaluations are typically performed using a filter media with a nominal pore size of 1.1 μm. In order to evaluate the potential effectiveness of filtration applications at reducing groundwater contamination concentrations, TSS and TDS testing were performed using 4 different filter media. These filter sizes were 0.45 μm, 1.2 μm, 5.0 μm, and 11.0 μm. Table IX-2.1 is a summary of the results of the filtrate from dewatering activities.

Table IX-2.1 – TSS and TDS results for dewatering filtrate

SAMPLE ID	RESULTS (mg/L)	
	TSS	TDS
SE0154-002 (0.45 μm Filter)	12	3,996
SE0154-003 (1.2 μm Filter)	13	3,772
SE0154-004 (5.0 μm Filter)	14	3,855
SE0154-005 (11.0 μm Filter)	18	3,511

Review of the data in Table IX-2.1 indicate very similar TSS and TDS concentrations were reported regardless of the filter media used in testing.

Site Groundwater

KEMRON was provided an additional water material for filtration evaluations. This material was identified as site groundwater. Testing of this groundwater followed the testing protocol outlined for the evaluation of the filtrate developed from dewatering activities applied to the site sediment material. The results of the site groundwater are as follows:

Table IX-2.2 – TSS and TDS results for groundwater

SAMPLE ID	RESULTS (mg/L)	
	TSS	TDS
SE0154-007 (0.45 μm Filter)	9.7	3,760
SE0154-008 (1.2 μm Filter)	24	3,746
SE0154-009 (5.0 μm Filter)	8.7	3,719
SE0154-010 (11.0 μm Filter)	11	3,695

As seen in the testing of the dewatering filtrate, the results of TSS and TDS testing performed on the site groundwater are very similar regardless of the filter media used. Additionally, the TSS and TDS results are very similar between the dewatering filtrate and the site groundwater.

In addition to TSS and TDS testing, aliquots of each filtered test material, as well as an aliquot of the unfiltered filtrate material were forwarded to STL laboratories for analytical testing. The analytical results of the filtrate from dewatering treated with the various filters and from groundwater treated with the various filters can be found in Appendix IX-2.

9.4 Basis of Design

Soil Filter Press Design

Review of the results of dewatering evaluations performed by KEMRON indicate that treatment of the site sediment, using a dewatering application at 100 psi positive pressure, results in a filter cake capable of passing both paint filter and liquid release testing. The 100 psi trial of the test shows a 19.25% reduction in moisture content (43.9% to 24.65%) which will be the basis for the dewatering filtrate water flow rate.

A summary of design parameters for soil treatment are shown in Table IX-3.

Water Filtration Design

The screening values used for water effluent are compiled from the following:

1. Site No. 5-58-013 Permit Limits provided for General Electric Company's Hudson River Superfund Site (Provided to Haley & Aldrich, Inc. from the NYSDEC);
2. Surface Water and Groundwater Quality Standards and Groundwater Effluent Limitations (6 NYCRR Part 703); and
3. Division of Water Technical and Operational Guidance Series (1.1.1).

A preference is given to site no. 5-58-013 permit limits as a basis for screening values due to the precedence that was set by that site for the Hudson River effluent limits for PCBs. The Hudson River has been classified as Class I as defined by 6 NYCRR Part 701.13 and this class is used as a basis for effluent water limits from items 2 and 3 above. A summary table of effluent water limits is provided in Appendix IX-3.

Filtration using filter media with pore sizes ranging from 0.45 to 11.0 μm effectively reduced metal concentrations from above effluent limits to below effluent limits in water for aluminum, lead, and copper (in groundwater). PCBs were reduced from 1.2 μm/L to non-detect (detection limit of 0.5 μm/L) from the dewatering filtrate with each filter tested. None of the filters tested reduced water below effluent metal concentration limits for antimony, cobalt, copper (in dewatering filtrate), magnesium, manganese, and sodium.

Testing of the filtrate material developed using this dewatering parameter indicated that filtration using filter media with pore sizes ranging from 0.45 to 11.0 μm resulted in very similar TSS and TDS values. Additionally, groundwater collected from the site exhibited TSS and TDS results very similar to the filtrate developed during the dewatering study. Total suspended solids were only reduced to below water effluent limits by the 0.45 μm filter in groundwater.

A design of a water treatment system using filtration can not be completed at this time with the results of this treatability study.

DEVIATIONS FROM WORK PLAN

Change in Sampling Methods

(H&A error: GW samples not sent to Kemron, used "left over" from lab analytical)

Change in Soil Treatability Procedures

(Based on results, changed

DATA GAP INVESTIGATION

UNKNOWN AT THIS TIME: Analytical results have not yet been received. Data set in currently incomplete.

TABLE D9.1
BENCH TESTING, INITIAL CHARACTERIZATION SUMMARY OF PHYSICAL ANALYSES

OU-1 REMEDIATION
NYSDEC SITE #3-60-022
1 RIVER STREET
HASTINGS-ON-HUDSON, NEW YORK

PARAMETER	UNIT	RESULTS
Moisture Content	%	43.9
Solids Content	%	69.5
Particle Size Distribution		
Gravel	%	22.8
Sand	%	61.4
Silt	%	11.6
Clay	%	4.2
Atterberg Limits		
Liquid Limit		Not Liquid
Plastic Limit		Not Plastic
Plasticity Index		Not Applicable

TABLE D9.2
SUMMARY OF GRAVITY DRAINAGE TESTING

OU-1 REMEDIATION
NYSDEC SITE #3-60-022
1 RIVER STREET
HASTINGS-ON-HUDSON, NEW YORK

PARAMETER	UNIT	RESULTS	
		GD-001	GD-002
Initial Weight	grams	1005.7	1048.2
Conditioner Used		None	5% DE (1)
Initial Moisture Content (ASTM)	%	43.9	43.9
Initial Solids Content	%	69.5	69.5
Final Weight of Cake	grams	929.9	1003.8
Effluent	grams	27.56	12.05
Moisture Content (ASTM)			
3 Day	%	29.48	36.17
5 Day	%	29.33	35.03
7 Day	%	28.89	42.02
Final Solids Content			
3 Day	%	77.23	73.44
5 Day	%	77.32	74.06
7 Day	%	77.59	70.41
Paint Filter Test	Pass / Fail	Fail	Fail
Liquid Release Test	Pass / Fail	Fail	Fail

(1) DE was added on a by-weight basis. For a 5% addition 5 grams of DE was added to every 100 grams of master composite material and blended prior to testing.

TABLE D9.3
SUMMARY OF FILTER PRESS TESTING

OU-1 REMEDIATION
NYSDEC SITE #3-60-022
1 RIVER STREET
HASTINGS-ON-HUDSON, NEW YORK

PARAMETER	UNITS	RESULTS			
		FP-001	FP-002	FP-003	FP-004
Initial Weight	g	464.22	454.33	455.78	455.1
Initial Moisture Content (ASTM)	%	43.9	43.9	43.9	43.9
Initial Solids Content	%	69.5	69.5	69.5	69.5
Gauge Pressure	lbs/in^2	25	50	75	100
Run Time	min	2.5	2	1.5	1
Final Weight of Cake	g	400.3	390.8	387.6	378.1
Final Moisture Content (ASTM)	%	33.38	27.77	26	24.65
Final Solids Content	%	74.98	78.26	79.37	80.22
Paint Filter Test	Pass / Fail	Fail	Pass	Pass	Pass
Liquid Release Test	Pass / Fail	Fail	Fail	Fail	Pass

TABLE D9.4
TSS AND TDS RESULTS FOR FILTRATE FROM BENCH TESTING

OU-1 REMEDIATION
NYSDEC SITE #3-60-022
1 RIVER STREET
HASTINGS-ON-HUDSON, NEW YORK

SAMPLE ID	RESULTS (mg/L)	
	TSS	TDS
SE0154-002 (0.45 μm Filter)	12	3,996
SE0154-003 (1.2 μm Filter)	13	3,772
SE0154-004 (5.0 μm Filter)	14	3,855
SE0154-005 (11.0 μm Filter)	18	4,122

TABLE D9.5
GROUNDWATER ANALYTICAL DATA FOR FILTRATE FROM BENCH TESTING

OU-1 REMEDIATION
NYSDEC SITE #3-60-022
1 RIVER STREET
HASTINGS-ON-HUDSON, NEW YORK

Sample ID	154-001	154-002	154-003	154-004	154-005
Date Sampled	12/5/2005	12/5/2005	12/5/2005	12/5/2005	12/5/2005
Matrix	Water	Water	Water	Water	Water
FILTER	untreated	0.45 µm	1.2 µm	5.0 µm	11.0 µm
PCBs (µg/L)					
PCB-1016 (AROCLOR 1016)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1221 (AROCLOR 1221)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1232 (AROCLOR 1232)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1242 (AROCLOR 1242)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1248 (AROCLOR 1248)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1254 (AROCLOR 1254)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1260 (AROCLOR 1260)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1262 (AROCLOR 1262)	1.2	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1268 (AROCLOR 1268)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
METALS (µg/L)					
Aluminum	1190 J	72.1 U*	65.3 U	79 U*	106 U*
Antimony	10.8	7.6	8.6	5.8 U	8.6
Arsenic	4.7 U	4.7 U	4.7 U	4.7 U	4.7 U
Barium	86.8	56.2	81	57.2	61
Beryllium	1.2 U	1.2 U	1.2 U	1.2 U	1.2 U
Cadmium	2.1	0.85	0.82	0.8 U	1.6
Calcium	492000	516000	472000	485000	499000
Chromium (Total)	2.9 U*	0.9 U	0.9 U	0.9 U	0.9 U
Cobalt	13.8	14.6	16.4	14.1	14.8
Copper	366	66	56.5	77.2	105
Iron	2510	49.9 U*	43.8 U	1330	303 J
Lead	55.7	2.2 U	2.2 U	5.4	3.1
Magnesium	140000	140000	136000	133000	141000
Manganese	12100	13100	13000	13200	12300
Nickel	71.8	32.8	52.7	101	52.4
Potassium	27600	27700	26300	26100	27500
Selenium	5.5	7.5	6.8	4.9 U	7.6
Silver	1.9 U	1.9 U	1.9 U	1.9 U	1.9 U
Sodium	397000	370000	379000	355000	389000
Thallium	4.8 UJ	4.8 UJ	4.8 UJ	4.8 UJ	7.4 U
Vanadium	3.4 J	2.3 U	2.3 U	2.3 U	2.3 U
Zinc	192	105	134	109	135
Mercury	0.52	0.1 U	0.1	0.14	0.16

NOTES:

U - This compound was not detected at or above the associated quantitation limit

U* - This compound should be considered "not detected" because it was detected in an associated blank at a similar level

J - Quantitation is approximate due to limitations identified during the QA review

UJ- This compound was not detected, but the reporting limit is probably higher due to a low bias identified during the QA review

TABLE D9.6
TSS AND TDS RESULTS FOR GROUNDWATER

OU-1 REMEDIATION
NYSDEC SITE #3-60-022
1 RIVER STREET
HASTINGS-ON-HUDSON, NEW YORK

SAMPLE ID	RESULTS (mg/L)	
	TSS	TDS
SE0154-007 (0.45 µm Filter)	9.7	3,760
SE0154-008 (1.2 µm Filter)	24	3,746
SE0154-009 (5.0 µm Filter)	8.7	3,719
SE0154-010 (11.0 µm Filter)	11	3,695

DRAFT

TABLE D9.7
GROUNDWATER ANALYTICAL DATA FOR FILTRATE FROM GROUNDWATER

OU-1 REMEDIATION
NYSDEC SITE #3-60-022
1 RIVER STREET
HASTINGS-ON-HUDSON, NEW YORK

Sample ID	SE0154-006	SE0154-007	SE0154-008	SE0154-009	SE0154-010
Date Sampled	12/20/2005	12/20/2005	12/20/2005	12/20/2005	12/20/2005
Matrix	Water	Water	Water	Water	Water
FILTER	untreated	0.45 µm	1.2 µm	5.0 µm	11.0 µm
PCBs (µg/L)					
PCB-1016 (AROCLOR 1016)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1221 (AROCLOR 1221)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1232 (AROCLOR 1232)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1242 (AROCLOR 1242)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1248 (AROCLOR 1248)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1254 (AROCLOR 1254)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1260 (AROCLOR 1260)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1262 (AROCLOR 1262)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
PCB-1268 (AROCLOR 1268)	0.50 U	0.50 U	0.50 U	0.50 U	0.50 U
METALS (µg/L)					
Aluminum	114 U*	46.4 U	46.4 U	46.4 U	46.4 U
Antimony	3.5 U	3.5 U	3.5 U	3.5 U	3.5 U
Arsenic	4.3 U	4.3 U	4.3 U	4.3 U	4.3 U
Barium	358	327	403	324	370
Beryllium	0.2 U	0.2 U	0.2 U	0.2 U	0.2 U
Cadmium	0.4 U	0.4 U	0.4 U	0.4 U	0.4 U
Calcium	81300	86000	94500	83600	93400
Chromium (Total)	1.5 U	1.5 U	1.5 U	1.5 U	1.5 U
Cobalt	2.4 U	2.4 U	2.4 U	2.4 U	2.4 U
Copper	18.5	2.1 U	2.1 U	5.8	6
Iron	3870	80.2 U*	85.2 U*	1350	1740
Lead	39.3	2.7 U	2.7 U	11.4	14.2
Magnesium	110000	116000	128000	113000	126000
Manganese	304	312	343	304	341
Nickel	1.8 U	1.8 U	1.8 U	1.8 U	1.8 U
Potassium	46200	48800	53300	47600	53000
Selenium	3.5 U	3.5 U	3.5 U	3.5 U	3.5 U
Silver	2.3 U	2.3 U	2.3 U	2.3 U	2.3 U
Sodium	846000	898000	968000	812000	959000
Thallium	4.6 U	4.6 U	4.6 U	4.6 U	4.6 U
Vanadium	2.2 U	2.2 U	2.2 U	2.2 U	2.2 U
Zinc	173	9.6	36.5	77.8	102
Mercury	0.1 U	0.1 U	0.1 U	0.1 U	0.1 U

NOTES:

U - This compound was not detected at or above the associated quantitation limit

U* - This compound should be considered "not detected" because it was detected in an associated blank at a similar level

J - Quantitation is approximate due to limitations identified during the QA review

TABLE D9.8
ANTICIPATED WATER EFFLUENT LIMITS

OU-1 REMEDIATION
NYSDEC SITE #3-60-022
1 RIVER STREET
HASTINGS-ON-HUDSON, NEW YORK

	Effluent Limit	Reference
PCBs (µg/L)		
PCB-1016 (AROCLOR 1016)	0.065	NYSDEC Personnel
PCB-1221 (AROCLOR 1221)	0.065	NYSDEC Personnel
PCB-1232 (AROCLOR 1232)	0.065	NYSDEC Personnel
PCB-1242 (AROCLOR 1242)	0.065	NYSDEC Personnel
PCB-1248 (AROCLOR 1248)	0.065	NYSDEC Personnel
PCB-1254 (AROCLOR 1254)	0.065	NYSDEC Personnel
PCB-1260 (AROCLOR 1260)	0.065	NYSDEC Personnel
PCB-1262 (AROCLOR 1262)	0.065	NYSDEC Personnel
PCB-1268 (AROCLOR 1268)	0.065	NYSDEC Personnel
METALS (µg/L)		
Aluminum	999	Site No. 5-58-013 Permit
Antimony	3	6 NYCRR 703
Arsenic	63	6 NYCRR 703 (Water Class I)
Barium	1000	6 NYCRR 703
Beryllium	3	TOGS 1.1.1
Cadmium	10	Site No. 5-58-013 Permit
Calcium	NA	6 NYCRR 703
Chromium (Total)	50	6 NYCRR 703
Cobalt	5	6 NYCRR 703
Copper	3.4	6 NYCRR 703 (Water Class I)
Iron	3994	Site No. 5-58-013 Permit
Lead	20	Site No. 5-58-013 Permit
Magnesium	35000	6 NYCRR 703
Manganese	300	6 NYCRR 703
Nickel	74	6 NYCRR 703 (Water Class I)
Potassium	NA	6 NYCRR 703
Selenium	10	6 NYCRR 703
Silver	2.3	6 NYCRR 703
Sodium	20000	6 NYCRR 703
Thallium	8	6 NYCRR 703
Vanadium	14	6 NYCRR 703
Zinc	999	Site No. 5-58-013 Permit
Mercury	0.7	6 NYCRR 703
TSS (mg/L)	10	Site No. 5-58-013 Permit

Kemron 2014 Solids Dewatering Report
“Dewatering Bench Scale Study”

DEWATERING BENCH-SCALE STUDY
HASTINGS-ON-THE-HUDSON

KEMRON PROJECT #: SH0522

July 23, 2014

Prepared for:

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TABLE OF CONTENTS

LIST OF TABLES AND APPENDICES

1.0 INTRODUCTION

KEMRON Environmental Services, Inc. (KEMRON) is pleased to present Haley & Aldrich Inc. with the results of the dewatering study performed on materials from the Hastings Site. The purpose of the dewatering study was to evaluate Gravity Drainage and Baroid Filter Press dewatering techniques at reducing the free liquids of the site material in order to pass Paint Filter and Liquid Release Testing (LRT). KEMRON also performed dewatering evaluations on the site material treated with a 5% addition of Diatomaceous Earth (DE) as requested by Haley & Aldrich. The following sections of this report include information regarding the protocols followed during each phase of the study as well as the results of the testing performed. Note that the tabular data presentations included within the text are summaries of tables presented in the attachments at the end of the report. As such, the tables embedded within the text may not include all information as presented in the attachments.

2.0 MATERIAL RECEIPT AND CHARACTERIZATION

On March 11, 2014, KEMRON received three site samples identified Bench Test-01, Bench Test-02 and Bench Test-03. All materials were logged into KEMRON's sample tracking database and placed in secure, refrigerated storage maintained at a temperature of 4 degrees Celsius (^{o}C). Copies of the chains of custody are provided in **Appendix A**.

On June 10, 2014 the three site materials were composited together and then homogenized to form a single Master Composite sample. The homogenized Master Composite was used for the duration of the dewatering study. Compositing / homogenization was performed by placing the contents of the chilled sample shipping containers into a large plastic mixing container. The composited sample was then gently mixed by hand using stainless steel utensils until visually homogenous.

The Master Composite material was subjected to physical characterization testing to establish a baseline of physical properties to determine dewatering treatment effectiveness, and to ensure that the material provided for the study are similar to those anticipated at the site. The following is a summary of physical testing performed on the untreated materials:

Parameter	Method
Paint Filter Test	EPA Method 9095
Moisture/Solids Content	ASTM D2216
Grain Size Distribution	ASTM D422
Atterberg Limits	ASTM D4318

The results of untreated characterization testing are presented in **Table 1**. Copies of the data sheets from the testing are included in **Appendix B**. The following is a summary of the information presented in Table 1:

Table 1
Physical Properties Testing

TESTING PARAMETER	TEST METHOD	UNIT	SAMPLE Master Composite
Moisture Content	ASTM D2216		
ASTM Moisture Content		%	119.47
Percent Solids		%	45.57
Particle Size Distribution	ASTM D422/D854		
Gravel		%	0.3
Sand		%	7.7
Silt		%	67.9
Clay		%	24.1
Atterberg Limits	ASTM 4318		
Liquid Limit			53.0
Plastic Limit			29.0
Plasticity Index			24.0
Sample Description	USCS (D2487)		Dark Grey Fat Clay
Sample Classification	USCS (D2487)		CH
Paint Filter Test	EPA 9095		Fail

Review of Table 1 indicates that the untreated Master Composite was classified as a Fat Clay with a plasticity index of 24.0. The high moisture content resulted in the material failing paint filter testing.

3.0 DEWATERING TRIALS

KEMRON performed two bench scale dewatering applications including gravity drainage and Baroid Filter Press testing. Each dewatering application was performed on two feed materials; the untreated Master Composite, and the Master Composite amended with a 5 percent (%) addition of Diatomaceous Earth (DE). The DE was added to the untreated Master Composite material on a by-weight basis according to the amount of Master Composite being tested. For example with testing performed on a 100 gram (g) aliquot of the Master Composite, 5 grams of DE was added to the Master Composite and blended until visually homogenous.

KEMRON performed two gravity drainage tests. One test was performed on the homogenized Master Composite material and a second test was conducted on the Master Composite material after being pretreated with 5% Diatomaceous Earth (DE). Gravity drainage testing was performed to evaluate the reduction in moisture that may be achieved by allowing the site material to gravity drain while stockpiled during field operations. In order to simulate the process on the laboratory scale, testing was performed by allowing a known quantity of the untreated material to drain via gravity through a porous filter paper media. Monitoring was performed at 3-day, 5-day, and 7-day intervals to evaluate the rate at which water drained from the sample. At each of these intervals KEMRON tested an aliquot of each material for moisture content. Following the termination of each test after 7 days, the solids from each test were rehomogenized and subjected to paint filter testing. The results of paint filter testing indicated that both of the gravity drainage treated materials released free liquid and therefore failed paint filter testing. As a result, Liquid Release Testing was not conducted. Complete data sheets for gravity drainage testing are included in Appendix C.

Baroid Filter Press testing is a dewatering simulation where positive pressure is applied to the site material. This testing is considered a viable simulation to evaluate dewatering applications such as plate and frame and belt filter press treatments. Filter press testing was performed at a positive pressure of 50, 75, 100, 125 and 150 pounds per square inch (psi). A 500g aliquot of the test material was placed into a stainless steel Baroid Filter Press chamber. The appropriate positive air pressure was introduced into the chamber to force any free liquid from the test material. The air pressure was applied until breakthrough occurred. As with the gravity drainage testing, KEMRON performed filter press testing on the homogenized Master Composite material and the Master Composite pretreated with a 5% addition of DE at the described positive pressures. After air break through occurred, each filter cake from treatment was then subjected to moisture content, paint filter, and LRT testing. Complete data sheets for testing performed during the Baroid filter press trials is provided in Appendix D attached to this report.

The results of dewatering testing are presented in **Table 2**. **Table 2** presents the initial and final moisture contents as well as additional testing information.

AECOM
Hasting's Dewatering Study
KEMRON Project No. SH0522

Table 2

Dewatering Test Summary

Dewatering Method	Testing Parameter	Test Method	Units	Master Composite					Master Composite+5% DE				
Gravity Drain	Initial Moisture Content	ASTM 2216	%	119.47					114.67				
	Initial Solids Content	ASTM 2216	%	45.57					46.58				
	Final Moisture Content	ASTM 2216	%	106.57					99.66				
	Final Solids Content	ASTM 2216	%	48.41					50.08				
	Paint Filter Testing	EPA Method 9095	PASS/FAIL	Fail					Fail				
	Liquid Release Testing	EPA Method 9096	PASS/FAIL	Not Tested Due to Failed Paint Filter Test					Not Tested Due to Failed Paint Filter Test				
Baroid Filter Press	**Pressure Applied**			**50 psi**	**75 psi**	**100 psi**	**125 psi**	**150 psi**	**50 psi**	**75 psi**	**100 psi**	**125 psi**	**150 psi**
	Initial Sample Quantity		Grams	500	500	500	500	508	525	525	525	525	525
	Total Test Run Time		Minutes	349	233	252	321	242	121	82	159	155	161
	Filtrate Collected		Milliliters	170	150	180	134	138	160	130	120	132	132
	Cake Thickness		Inches	1.84	1.94	1.74	2.01	1.87	2.15	2.13	2.14	2.04	1.97
	Initial Moisture Content	ASTM 2216	%	119.47	119.47	119.47	119.47	119.47	114.67	114.67	114.67	114.74	114.74
	Initial Percent Solids	ASTM 2216	%	50.49	50.49	50.49	45.57	45.57	46.58	46.58	46.58	46.57	46.57
	Final Moisture Content	ASTM 2216	%	62.48	64.63	58.39	57.36	53.43	63.53	71.06	54.23	53.77	51.41
	Final Percent Solids	ASTM 2216	%	61.55	60.96	63.26	63.55	65.21	61.24	58.48	64.88	65.04	66.05
	Paint Filter Testing	EPA Method 9095	PASS/FAIL	Pass	Pass	Pass	Pass	Pass	Pass	Pass	Pass	Pass	Pass
	Liquid Release Testing	EPA Method 9096	PASS/FAIL	Fail	Fail	Fail	Fail	Fail	Fail	Fail	Fail	Fail	Fail

Notes:
psi = Pounds per Square Inch
%= Percent

Review of Table 2 shows that the Master Composite and the Master Composite amended with a 5% addition of DE exhibited an ASTM moisture content reduction of approximately 13 and 15% respectively when subjected to gravity drainage dewatering after a seven (7) day treatment period. Both of the gravity drainage dewatered materials failed paint filter testing and therefore were not subjected to LRT testing.

The results of Baroid Filter Press testing, also summarized in Table 2, show a general trend of reduced moisture / increased solids content with an increase in positive pressure applied to the test material. However, note that for both the Master Composite feed material and the Master Composite amended with a 5% addition of DE, an increase in treatment pressure from 50 psi to 150 psi only resulted in an increase in solids content of less than 5%. Additionally, Table 2 indicates that the addition of 5% DE to the Master Composite resulted in little additional dewatering compared to the unamended Master Composite material, but the rate of liquid removal was significantly faster in the DE amended Master Composite.

4.0 Conclusions

KEMRON evaluated the effectiveness of two different dewatering techniques on the untreated site material. KEMRON performed Gravity Drainage testing and Baroid Filter Press testing on the homogenized Master Composite as well as the Master Composite treated with 5% Diatomaceous Earth. The results of the study revealed the Gravity Drainage testing was not an effective means of dewatering. This determination was based off the samples failing a Paint Filter Test. After seven days, the Master Composite material showed a decrease in moisture content of about 13% while the Master Composite and DE material showed a decrease in moisture content of about 15%. Due to failed Paint Filter Testing, Liquid Release Testing was not conducted.

KEMRON conducted Baroid filter press testing at five pressures ranging from 50psi to 150psi. Pressure was applied until air breakthrough occurred from the testing chamber, or the recovery of liquid ceased. The results of filter press simulations indicated a general trend of increasing solids content with higher applied positive pressures. However, a significant increase in solids content was not achieved at the highest applied pressure compared to lower treatment pressure.

KEMRON observed that there was a noticeable difference in visual moisture with the treated materials especially in the samples treated at higher positive pressures. KEMRON observed that the bottom layer of the test material in the filter press chamber was significantly drier than the material near the top of the chamber. This is often observed when testing fine grained material similar to the Master Composite evaluated in this study. Moisture is easily removed from the bottom portion of the sample and with the removal of this moisture the fine grained particles are compacted and become less permeable and moisture from the top of the sample is unable to pass through this dense fine grained layer of soil.

Testing of the filter press treated materials showed that all of the treated materials passed paint filter testing but failed liquid release testing (LRT). Paint filter testing relies on gravity to release liquid from the test sample while LRT testing utilizes a mechanical piston operating at a 50 psi force to squeeze any free liquid from the test material. The pass or fail determination of the LRT test is the presence of any liquid staining on indicator paper that is placed on the top and bottom surfaces of the test sample. LRT testing is a very aggressive evaluation of the presence of free liquids.

KEMRON understands that LRT testing was utilized to evaluate the potential of liquid release from the dewatered material during transportation activities. Additional testing may be required to evaluate the further reduction of liquids through the use of absorbent bulking materials. There are many additives that have the capability of absorbing free liquids, including corn cob grit, super absorbent polymers (SAP), fly ashes, kiln dusts, etc. Many of these materials are available at relatively low costs.

More appropriate testing procedures may be available for determining if free liquids would be released during transportation. KEMRON has performed several studies to determine this by placing an aliquot of sample on a shaker or vibratory table to evaluate if free liquid is released from the sample.

In general, the results of the treatability study shows that mechanical dewatering applications using an applied positive pressure of 50 psi is capable of reducing liquid content sufficiently to pass paint filter testing. The use of higher positive pressures may result in higher moisture removals and many mechanical applications are easily modified to operate at a wide range of pressures. The use of DE as an amendment did not significantly increase the removal of liquid from the test material. However, it did significantly speed up the removal process.

The failure of the dewatered materials to pass LRT testing does not necessarily indicate that mechanical dewatering applications are not capable of successfully treating the site materials. The incorporation of additional absorbent material into the dewatered soil may provide sufficient moisture binding to allow transportation of the site materials. KEMRON can provide additional or alternative options for evaluating the ability of the site materials to be transported to an off-site location.

APPENDIX A

Chain of Custody

Atlantic Richfield Company
A BP affiliated company

Laboratory Management Program LaMP Chain of Custody Record

BP/ARC Project Name: Former Anaconda Wire & Cable
Req Due Date (mm/dd/yy):
Rush TAT: Yes ___ No ___
BP/ARC Facility No:
Lab Work Order Number:

Lab Name: Kemron Environmental Services	BP/ARC Facility Address: 1 River Street	Consultant/Contractor: Haley & Aldrich, Inc.
Lab Address: 1359-A Ellsworth Industrial Blvd., Atlanta, GA 30318	City, State, ZIP Code: Hastings on Hudson, New York 10706	Consultant/Contractor Project No: 28612
Lab PM: Tommy Jordan	Lead Regulatory Agency: NYSDEC	Address: 200 Town Centre Drive Suite 2, Rochester, NY 14632
Lab Phone: 404-636-0928	California Global ID No.: NA	Consultant/Contractor PM: Ryan Scott
Lab Shipping Accnt:	Enfos Proposal No:	Phone: 585-321-4204
Lab Bottle Order No:	Accounting Mode: Provision ___ OOC-BU ___ OOC-RM ___	Email EDD To: rscott@haleyaldrich.com
Other Info:	Stage: Activity:	Invoice To: BP/ARC ___ Contractor X

BP/ARC EBM: Paul Johnson
EBM Phone: 630-420-5992
EBM Email: Paul.Johnson4@bp.com

Report Type & QC Level: Standard ___ Full Data Package ___

Lab No.	Sample Description	Date	Time	Matrix: Soil / Solid	Water / Liquid	Air / Vapor	Sediment	Total Number of Containers	Unpreserved	H_2SO_4	HNO_3	HCl	Methanol		Requested Analyses										Comments
	Bench Test-01	09/25/13	1000				X	1	X																Dewatering
	Benchtest-02	09/25/13	1015				X	1	X																↓
	Benchtest-03	09/25/13	1020				X	1	X																↓

Comments note: If sample not collected, indicate "No Sample" in comments and single-strike out and initial any preprinted sample description.

	Relinquished By / Affiliation	Date	Time	Accepted By / Affiliation	Date	Time
Sampler's Name:	[signature] / H&A	3/10/14	1900	[signature]	3/11/14	1055
Sampler's Company:						
Shipment Method: Ship Date:						
Shipment Tracking No:						

Special Instructions:

THIS LINE - LAB USE ONLY: Custody Seals In Place: Yes / No | Temp Blank: Yes / No | Cooler Temp on Receipt: ______ °F/C | Trip Blank: Yes / No | MS/MSD Sample Submitted: Yes / No

APPENDIX B

Untreated Physical Properties Testing

Data Sheets

MOISTURE CONTENT DETERMINATION

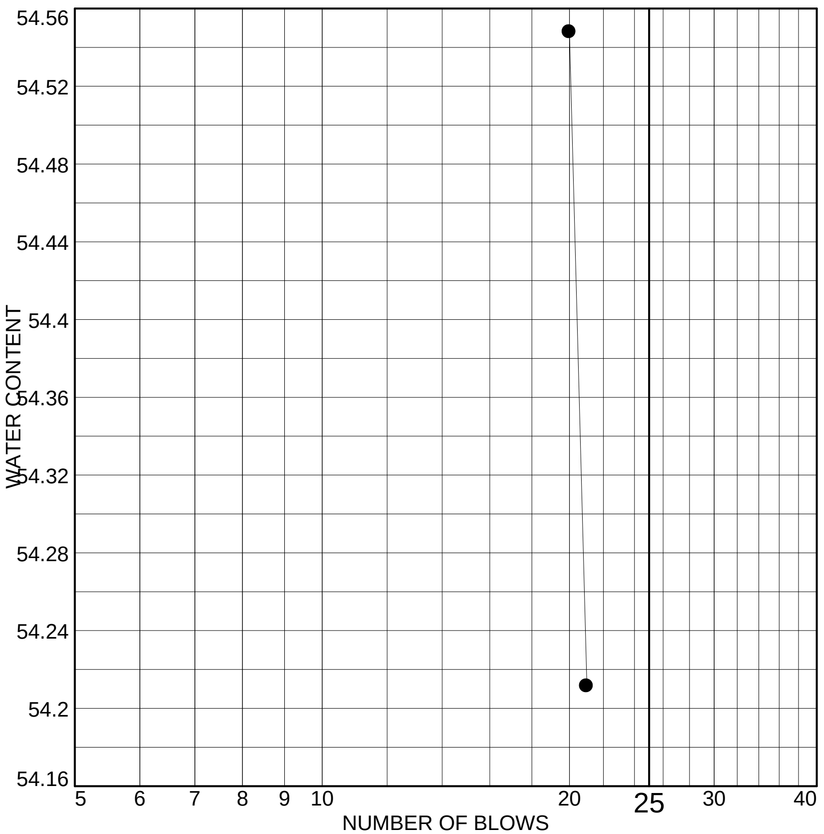
REPORT FORM

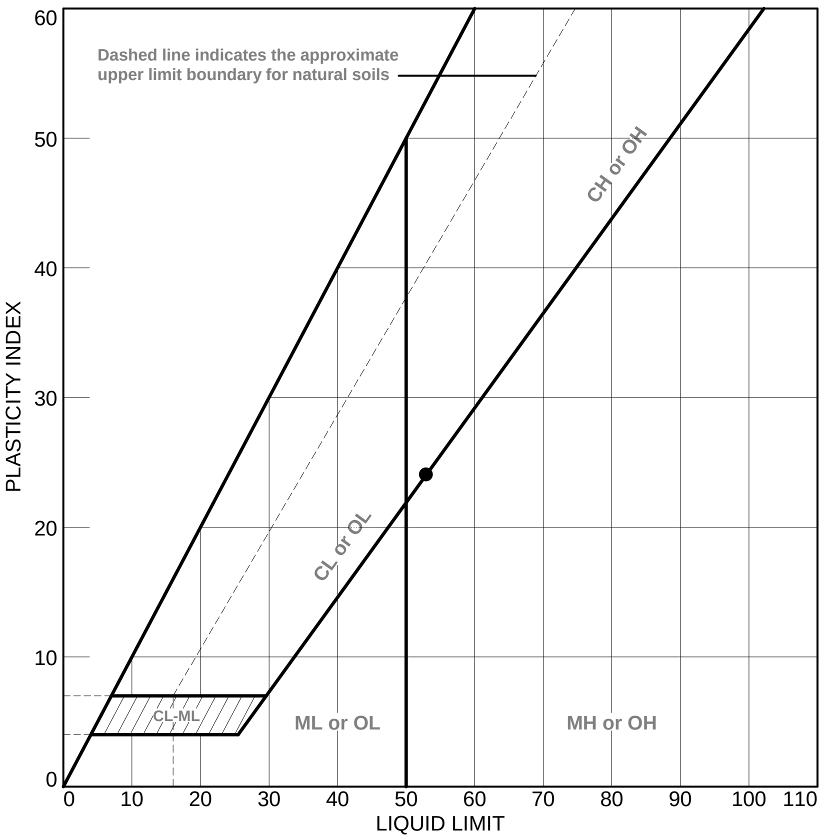
ASTM D 2216

PROJECT:	Hasting's Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
TESTING DATE:	06/23/14
TESTED BY:	JDM
TRACKING CODE:	9621DUP_MC

MOISTURE CONTENT (Dry & Wet Basis)						
1. MOISTURE TIN NO.	A		B		C	
2. WT MOISTURE TIN (tare weight)	70.5559	g	63.3955	g	63.7285	g
3. WT WET SOIL + TARE	94.6939	g	92.8518	g	85.9947	g
4. WT DRY SOIL + TARE	81.3537	g	76.9798	g	73.9409	g
5. WT WATER, Ww	13.3402	g	15.8720	g	12.0538	g
6. WT DRY SOIL, Ws	10.7978	g	13.5843	g	10.2124	g
7. ASTM MOISTURE CONTENT	123.55	%	116.84	%	118.03	%
8. PERCENT SOLIDS	44.73	%	46.12	%	45.87	%
9. AVERAGE ASTM MOISTURE CONTENT	119.47	%				
10. AVERAGE PERCENT SOLIDS	45.57	%				

LIQUID AND PLASTIC LIMITS TEST REPORT





	SOURCE	SAMPLE #	DEPTH/ELEV.	DATE SAMPLED	USCS	MATERIAL DESCRIPTION	NM %	LL	PI
●		Master Composite		6/20/14	CH	Dark Grey fat clay	114.7	53	24

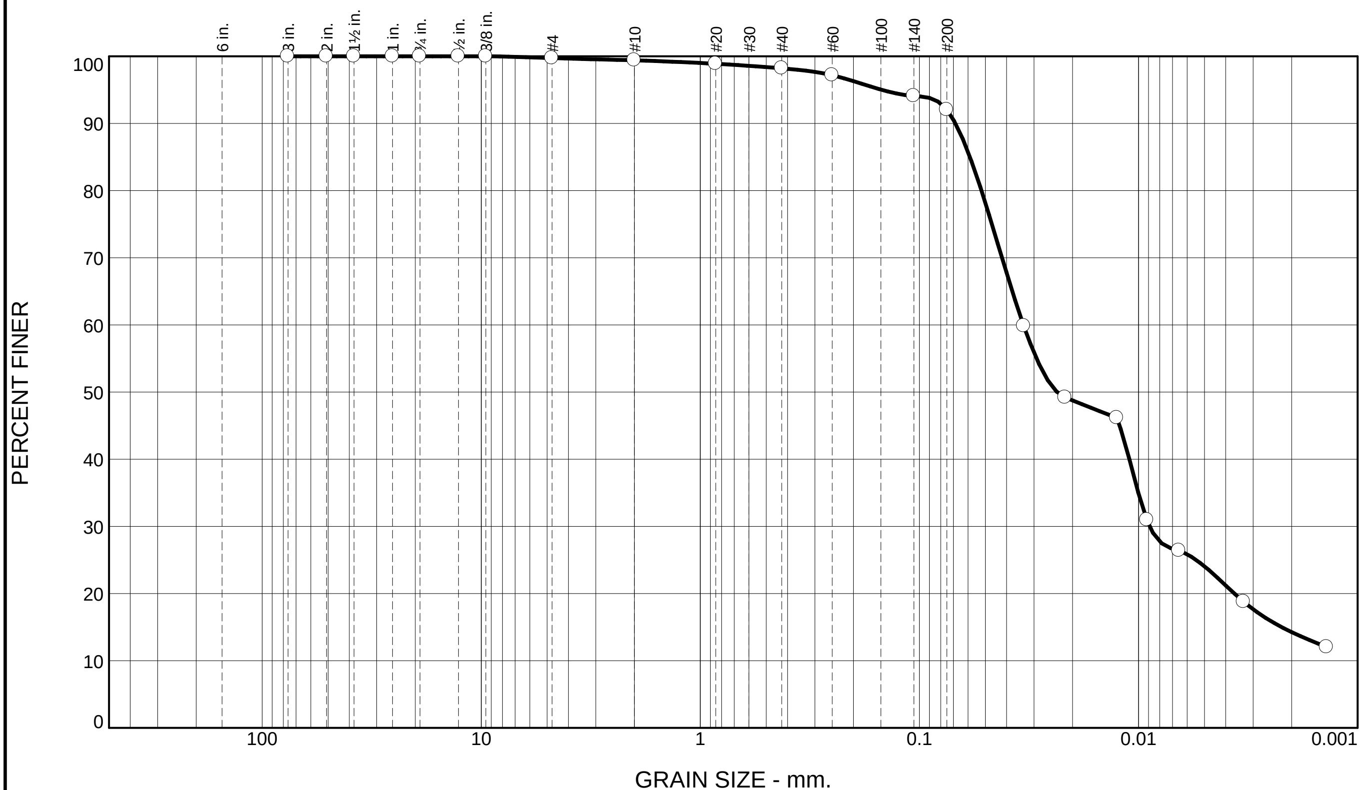
Client AECOM

Project Hastings Dewatering Study

Project No. SH0522 Figure 9621_AT

KEMRON Environmental Services Inc.
Atlanta, Georgia

Particle Size Distribution Report



% +3"	% Gravel		% Sand			% Fines	
	Coarse	Fine	Coarse	Medium	Fine	Silt	Clay
0.0	0.0	0.3	0.3	1.2	6.2	67.9	24.1

SIEVE SIZE	PERCENT FINER	SPEC.* PERCENT	PASS? (X=NO)
3	100.0		
2	100.0		
1.5	100.0		
1	100.0		
.75	100.0		
.5	100.0		
.375	100.0		
#4	99.7		
#10	99.4		
#20	98.9		
#40	98.2		
#60	97.2		
#140	94.1		
#200	92.0		
0.0334 mm.	59.8		
0.0216 mm.	49.2		
0.0126 mm.	46.1		
0.0092 mm.	30.9		
0.0065 mm.	26.4		
0.0033 mm.	18.8		
0.0014 mm.	12.0		

* (no specification provided)

Soil Description

Dark Grey fat clay

Atterberg Limits

PL= 29 LL= 53 PI= 24

Coefficients

D_{90}= 0.0685 D_{85}= 0.0588 D_{60}= 0.0335
D_{50}= 0.0236 D_{30}= 0.0089 D_{15}= 0.0022
D_{10}= C_u= C_c=

Classification

USCS= CH AASHTO= A-7-6(26)

Remarks

Sample Number: Master Composite

Date: 6/20/14

KEMRON Environmental Services Inc. Atlanta, Georgia

Client: AECOM
Project: Hastings Dewatering Study
Project No: SH0522 **Figure** 9621_GR

Tested By: JDM **Checked By:** TAJ

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/11/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9621_Paint Filter Test
TESTING METHOD:			

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	100.37	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	3.80	**g**
RESULTS (PASS / FAIL) *	FAIL	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

APPENDIX C

Dewatering Gravity Drainage Evaluation

Data Sheets

GRAVITY DRAINAGE TESTING

DATA SHEET

PROJECT: Hastings Dewatering Study
PROJECT No.: SH0522
SAMPLE No.: Master Composite
MATERIAL TYPE:
TESTING DATE: 6/11/2014
TESTED BY: JDM
TRACKING COD 9622_GD

SET-UP INFORMATION GRAVITY DRAINAGE TESTING	
1. FUNNEL	1906.00 g
2. FUNNEL + SOIL (INITIAL)	2886.00 g
3. FUNNEL + SOIL (FINAL)	2741.50 g
4. BEAKER	67.00 g
5. BEAKER + EFFLUENT	161.00 g
6. SOIL (INITIAL)	980.00 g
7. SOIL (FINAL)	835.50 g
8. EFFLUENT	94.00 g

MONITORING INFORMATION

TIME (HR)	EFFLUENT (g)	VISUAL OBSERVATIONS
2	26.5	
18	80.0	
44	88.0	
118	91.5	
168	94.0	

MOISTURE CONTENT (Dry & Wet Basis)

1. MOISTURE TIN NO.	3 Day		5 Day		7 Day	
2. WT MOISTURE TIN (tare weight)	1.29	g	1.30	g	1.30	g
3. WT WET SOIL + TARE	15.06	g	17.11	g	10.83	g
4. WT DRY SOIL + TARE	7.99	g	8.84	g	5.91	g
5. WT WATER, Ww	7.07	g	8.26	g	4.92	g
6. WT DRY SOIL, Ws	6.70	g	7.55	g	4.62	g
7. ASTM MOISTURE CONTENT, W	105.57	%	109.50	%	106.57	%
8. EPA MOISTURE CONTENT, W	51.35	%	52.27	%	51.59	%

VISUALS AND OBSERVATIONS

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/18/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9622_PaintFilter
TESTING METHOD:	EPA 9095		

After 7-Day Gravity Drain

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	105.35	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.12	**g**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/18/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9622_LR
TESTING METHOD:	EPA Method 9096		

After 7-Day Gravity Drain

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL		**g**
LENGTH OF TEST		**min.**
RESULTS (PASS / FAIL) *		
Not Tested Due To Failed Paint Filter Test		

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

GRAVITY DRAINAGE TESTING

DATA SHEET

PROJECT:	Hastings Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE	5% DE
TESTING DATE:	6/11/2014
TESTED BY:	JDM
TRACKING COD	9623_GD

SET-UP INFORMATION GRAVITY DRAINAGE TESTING	
1. FUNNEL	1891.50 g
2. FUNNEL + SOIL (INITIAL)	2947.00 g
3. FUNNEL + SOIL (FINAL)	2865.00 g
4. BEAKER	67.50 g
5. BEAKER + EFFLUENT	90.50 g
6. SOIL (INITIAL)	1055.50 g
7. SOIL (FINAL)	973.50 g
8. EFFLUENT	23.00 g

MONITORING INFORMATION		
TIME (HR)	**EFFLUENT (g)**	**VISUAL OBSERVATIONS**
2	0.0	
18	8.0	
44	22.0	
118	22.0	
168	23.0	

MOISTURE CONTENT (Dry & Wet Basis)						
1. MOISTURE TIN NO.	3 Day		5 Day		7 Day	
2. WT MOISTURE TIN (tare weight)	1.29	g	1.28	g	1.26	g
3. WT WET SOIL + TARE	19.45	g	14.71	g	12.13	g
4. WT DRY SOIL + TARE	10.42	g	8.32	g	6.71	g
5. WT WATER, Ww	9.03	g	6.39	g	5.42	g
6. WT DRY SOIL, Ws	9.13	g	7.03	g	5.44	g
7. ASTM MOISTURE CONTENT, W	98.86	%	90.86	%	99.66	%
8. EPA MOISTURE CONTENT, W	49.71	%	47.61	%	49.92	%

VISUALS AND OBSERVATIONS

MOISTURE CONTENT DETERMINATION

REPORT FORM

ASTM D 2216

PROJECT:	Hastings Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite+5% DE
TESTING DATE:	06/18/14
TESTED BY:	RJB
TRACKING CODE:	9622_MC

MOISTURE CONTENT (Dry & Wet Basis)						
1. MOISTURE TIN NO.	A		B		C	
2. WT MOISTURE TIN (tare weight)	1.2851	g	1.2941	g	1.3013	g
3. WT WET SOIL + TARE	6.5908	g	5.0253	g	6.8118	g
4. WT DRY SOIL + TARE	3.7596	g	3.0321	g	3.8655	g
5. WT WATER, Ww	2.8312	g	1.9932	g	2.9463	g
6. WT DRY SOIL, Ws	2.4745	g	1.7380	g	2.5642	g
7. ASTM MOISTURE CONTENT	114.42	%	114.68	%	114.90	%
8. PERCENT SOLIDS	46.64	%	46.58	%	46.53	%
9. AVERAGE ASTM MOISTURE CONTENT	114.67	%				
10. AVERAGE PERCENT SOLIDS	46.58	%				

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/18/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite+5% DE	TRACKING CODE:	9623_PaintFilter
TESTING METHOD:	EPA 9095		

After 7-Day Gravity Drain

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	103.78	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.13	**g**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/18/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite+5% De	TRACKING CODE:	9623_LR
TESTING METHOD:	EPA Method 9096		

After 7-Day Gravity Drain

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL		**g**
LENGTH OF TEST		**min.**
RESULTS (PASS / FAIL) *		
Not Tested Due To Failed Paint Filter Test		

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

APPENDIX D

Dewatering Baroid Filter Press Evaluation

Data Sheets

FILTER PRESS TEST

REPORT FORM

PROJECT:	Hastings Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE:	
TESTING DATE:	6/19/2014
TESTED BY:	JDM
TRACKING CODE:	9624_FP

TESTING CONDITIONS	
1. CONDITIONER	No Additions
2. RUN TIME (min)	349
3. INITIAL MATERIAL WEIGHT (g)	500
4. GAGE PRESSURE (psi)	50 psi
5. FILTRATE VOLUME (ml)	170
6. CAKE WEIGHT (g)	336.15
7. CAKE THICKNESS (in)	1.84

FEED PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	70.56 g	63.40 g	63.73 g
3. TOTAL SAMPLE + TARE, WT	94.69 g	92.85 g	85.99 g
4. DRY SOLIDS + TARE, WT	81.35 g	76.98 g	73.94 g
5. PERCENT SOLIDS	44.73 %	46.12 %	45.87 %

CAKE PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	1.29 g	1.29 g	1.30 g
3. TOTAL SAMPLE + TARE, WT	10.94 g	13.08 g	12.52 g
4. DRY SOLIDS + TARE, WT	7.30 g	8.58 g	8.10 g
5. PERCENT SOLIDS	62.21 %	61.87 %	60.57 %

FILTRATE PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	166.09 g	70.11 g	67.67 g
3. TOTAL SAMPLE + TARE, WT	229.64 g	122.62 g	104.25 g
4. DRY SOLIDS + TARE, WT	166.85 g	70.72 g	68.10 g
5. PERCENT SOLIDS	1.20 %	1.17 %	1.18 %

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/11/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9624_Paint Filter Test
TESTING METHOD:			

After 50 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	100.30	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/18/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9624_LR
TESTING METHOD:	EPA Method 9096		

After 50 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	296.50	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

FILTER PRESS TEST

REPORT FORM

PROJECT:	Hastings Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE:	
TESTING DATE:	6/17/2014
TESTED BY:	JDM
TRACKING CODE:	9625_FP

TESTING CONDITIONS	
1. CONDITIONER	5% Diatomaceous Earth
2. RUN TIME (min)	121
3. INITIAL MATERIAL WEIGHT (g)	525
4. GAGE PRESSURE (psi)	50 psi
5. FILTRATE VOLUME (ml)	160
6. CAKE WEIGHT (g)	362.14
7. CAKE THICKNESS (in)	2.15

FEED PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	1.29 g	1.29 g	1.30 g
3. TOTAL SAMPLE + TARE, WT	6.59 g	5.03 g	6.81 g
4. DRY SOLIDS + TARE, WT	3.76 g	3.03 g	3.87 g
5. PERCENT SOLIDS	46.64 %	46.58 %	46.53 %

CAKE PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	1.29 g	1.29 g	1.28 g
3. TOTAL SAMPLE + TARE, WT	6.01 g	8.83 g	9.20 g
4. DRY SOLIDS + TARE, WT	4.23 g	5.67 g	6.30 g
5. PERCENT SOLIDS	62.34 %	57.98 %	63.42 %

FILTRATE PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	168.59 g	52.77 g	50.99 g
3. TOTAL SAMPLE + TARE, WT	231.12 g	92.50 g	92.48 g
4. DRY SOLIDS + TARE, WT	169.34 g	53.24 g	51.48 g
5. PERCENT SOLIDS	1.20 %	1.17 %	1.18 %

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/11/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9625_Paint Filter Test
TESTING METHOD:			

After 50 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	100.09	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/18/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9625_LR
TESTING METHOD:	EPA Method 9096		

After 50 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	340.98	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

FILTER PRESS TEST
REPORT FORM

PROJECT:	Hastings Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE:	
TESTING DATE:	6/19/2014
TESTED BY:	JDM
TRACKING CODE:	9626_FP

TESTING CONDITIONS	
1. CONDITIONER	No Additions
2. RUN TIME (min)	233
3. INITIAL MATERIAL WEIGHT (g)	500
4. GAGE PRESSURE (psi)	75 psi
5. FILTRATE VOLUME (ml)	150
6. CAKE WEIGHT (g)	341.74
7. CAKE THICKNESS (in)	1.94

FEED PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	70.56	g	63.40	g	63.73	g
3. TOTAL SAMPLE + TARE, WT	94.69	g	92.85	g	85.99	g
4. DRY SOLIDS + TARE, WT	81.35	g	76.98	g	73.94	g
5. PERCENT SOLIDS	44.73	%	46.12	%	45.87	%

CAKE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.28	g	1.28	g	1.29	g
3. TOTAL SAMPLE + TARE, WT	11.10	g	14.10	g	11.28	g
4. DRY SOLIDS + TARE, WT	6.99	g	9.78	g	7.13	g
5. PERCENT SOLIDS	58.14	%	66.30	%	58.46	%

FILTRATE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.62.90	g	65.05	g	63.56	g
3. TOTAL SAMPLE + TARE, WT	200.41	g	106.43	g	115.37	g
4. DRY SOLIDS + TARE, WT	163.32	g	65.54	g	64.17	g
5. PERCENT SOLIDS	81.49	%	1.18	%	1.18	%

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/11/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9626_Paint Filter Test
TESTING METHOD:			

After 75 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	100.00	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/18/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9626_LR
TESTING METHOD:	EPA Method 9096		

After 75 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	281.45	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

FILTER PRESS TEST
REPORT FORM

PROJECT:	Hastings Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE:	
TESTING DATE:	6/17/2014
TESTED BY:	JDM
TRACKING CODE:	9627_FP

TESTING CONDITIONS	
1. CONDITIONER	5% Diatomaceous Earth
2. RUN TIME (min)	82
3. INITIAL MATERIAL WEIGHT (g)	525
4. GAGE PRESSURE (psi)	75 psi
5. FILTRATE VOLUME (ml)	130
6. CAKE WEIGHT (g)	387.29
7. CAKE THICKNESS (in)	2.13

FEED PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.29	g	1.29	g	1.30	g
3. TOTAL SAMPLE + TARE, WT	6.59	g	5.03	g	6.81	g
4. DRY SOLIDS + TARE, WT	3.76	g	3.03	g	3.87	g
5. PERCENT SOLIDS	46.64	%	46.58	%	46.53	%

CAKE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.29	g	1.30	g	1.27	g
3. TOTAL SAMPLE + TARE, WT	12.02	g	9.20	g	10.34	g
4. DRY SOLIDS + TARE, WT	7.60	g	5.79	g	6.69	g
5. PERCENT SOLIDS	58.85	%	56.88	%	59.72	%

FILTRATE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	168.40	g	63.71	g	63.36	g
3. TOTAL SAMPLE + TARE, WT	196.75	g	107.55	g	102.33	g
4. DRY SOLIDS + TARE, WT	168.77	g	64.22	g	63.81	g
5. PERCENT SOLIDS	1.31	%	1.16	%	1.15	%

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/11/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9627_Paint Filter Test
TESTING METHOD:			

After 75 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	105.03	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/18/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9627_LR
TESTING METHOD:	EPA Method 9096		

After 75 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	320.71	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

FILTER PRESS TEST

REPORT FORM

PROJECT:	Hastings Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE:	
TESTING DATE:	6/19/2014
TESTED BY:	JDM
TRACKING CODE:	9628_FP

TESTING CONDITIONS	
1. CONDITIONER	No Additions
2. RUN TIME (min)	252
3. INITIAL MATERIAL WEIGHT (g)	500
4. GAGE PRESSURE (psi)	100 psi
5. FILTRATE VOLUME (ml)	180
6. CAKE WEIGHT (g)	309.71
7. CAKE THICKNESS (in)	1.74

FEED PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	70.56	g	63.40	g	63.73	g
3. TOTAL SAMPLE + TARE, WT	94.69	g	92.85	g	85.99	g
4. DRY SOLIDS + TARE, WT	81.35	g	76.98	g	73.94	g
5. PERCENT SOLIDS	44.73	%	46.12	%	45.87	%

CAKE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.28	g	1.30	g	1.28	g
3. TOTAL SAMPLE + TARE, WT	16.56	g	8.44	g	14.50	g
4. DRY SOLIDS + TARE, WT	11.17	g	5.99	g	9.13	g
5. PERCENT SOLIDS	64.72	%	65.69	%	59.38	%

FILTRATE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	168.16	g	50.99	g	52.77	g
3. TOTAL SAMPLE + TARE, WT	244.75	g	100.14	g	91.22	g
4. DRY SOLIDS + TARE, WT	169.06	g	51.55	g	53.21	g
5. PERCENT SOLIDS	1.18	%	1.14	%	1.14	%

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/11/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9628_Paint Filter Test
TESTING METHOD:			

After 100 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	102.97	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/18/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9628_LR
TESTING METHOD:	EPA Method 9096		

After 100 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	247.00	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

FILTER PRESS TEST

REPORT FORM

PROJECT:	Hastings Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE:	
TESTING DATE:	6/25/2014
TESTED BY:	JDM
TRACKING CODE:	9629DUP_FP

TESTING CONDITIONS	
1. CONDITIONER	5% Diatomaceous Earth
2. RUN TIME (min)	159 Minutes
3. INITIAL MATERIAL WEIGHT (g)	525
4. GAGE PRESSURE (psi)	100 psi
5. FILTRATE VOLUME (ml)	120
6. CAKE WEIGHT (g)	398.56
7. CAKE THICKNESS (in)	2.14

FEED PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.29	g	1.29	g	1.30	g
3. TOTAL SAMPLE + TARE, WT	6.59	g	5.03	g	6.81	g
4. DRY SOLIDS + TARE, WT	3.76	g	3.03	g	3.87	g
5. PERCENT SOLIDS	46.64	%	46.58	%	46.53	%

CAKE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.28	g	1.28	g	1.28	g
3. TOTAL SAMPLE + TARE, WT	23.12	g	23.09	g	21.65	g
4. DRY SOLIDS + TARE, WT	15.19	g	15.22	g	14.93	g
5. PERCENT SOLIDS	63.69	%	63.92	%	67.02	%

FILTRATE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	168.72	g	52.46	g	69.41	g
3. TOTAL SAMPLE + TARE, WT	215.79	g	93.98	g	115.54	g
4. DRY SOLIDS + TARE, WT	169.27	g	52.95	g	69.94	g
5. PERCENT SOLIDS	1.17	%	1.17	%	1.16	%

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/11/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9629_Paint Filter Test
TESTING METHOD:			

After 100 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	103.72	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/18/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9629_LR
TESTING METHOD:	EPA Method 9096		

After 100 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	344.60	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

FILTER PRESS TEST

REPORT FORM

PROJECT:	Hasting's Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE:	
TESTING DATE:	6/24/2014
TESTED BY:	JDM
TRACKING CODE:	9630DUP_FP

TESTING CONDITIONS	
1. CONDITIONER	No Addition
2. RUN TIME (min)	321
3. INITIAL MATERIAL WEIGHT (g)	500
4. GAGE PRESSURE (psi)	125
5. FILTRATE VOLUME (ml)	134
6. CAKE WEIGHT (g)	359.38
7. CAKE THICKNESS (in)	2.011

FEED PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	70.56 g	63.40 g	63.73 g
3. TOTAL SAMPLE + TARE, WT	94.69 g	92.85 g	85.99 g
4. DRY SOLIDS + TARE, WT	81.35 g	76.98 g	73.94 g
5. PERCENT SOLIDS	44.73 %	46.12 %	45.87 %

CAKE PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	1.28 g	1.28 g	1.28 g
3. TOTAL SAMPLE + TARE, WT	25.29 g	26.71 g	25.21 g
4. DRY SOLIDS + TARE, WT	16.39 g	17.59 g	16.50 g
5. PERCENT SOLIDS	62.94 %	64.13 %	63.58 %

FILTRATE PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	70.11 g	67.74 g	65.08 g
3. TOTAL SAMPLE + TARE, WT	113.04 g	114.25 g	109.39 g
4. DRY SOLIDS + TARE, WT	70.60 g	68.22 g	65.57 g
5. PERCENT SOLIDS	1.15 %	1.02 %	1.10 %

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/24/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9630DUP_Paint Filter Test
TESTING METHOD:	EPA Method 9095		

After 125 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	104.63	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/24/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9630DUP_LR
TESTING METHOD:	EPA Method 9096		

After 125 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	283.94	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

FILTER PRESS TEST
REPORT FORM

PROJECT: Hasting's Dewatering Study
PROJECT No.: SH0522
SAMPLE No.: Master Composite
MATERIAL TYPE:
TESTING DATE: 6/24/2014
TESTED BY: JDM
TRACKING CODE: 9631DUP_FP

TESTING CONDITIONS	
1. CONDITIONER	5% Diatomaceous Earth
2. RUN TIME (min)	155
3. INITIAL MATERIAL WEIGHT (g)	525
4. GAGE PRESSURE (psi)	125
5. FILTRATE VOLUME (ml)	132
6. CAKE WEIGHT (g)	381.34
7. CAKE THICKNESS (in)	2.035

FEED PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.29	g	1.29	g	1.30	g
3. TOTAL SAMPLE + TARE, WT	6.59	g	5.03	g	6.81	g
4. DRY SOLIDS + TARE, WT	3.76	g	3.03	g	3.87	g
5. PERCENT SOLIDS	46.59	%	46.58	%	46.53	%

CAKE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.28	g	1.29	g	1.28	g
3. TOTAL SAMPLE + TARE, WT	23.46	g	22.35	g	22.34	g
4. DRY SOLIDS + TARE, WT	15.90	g	14.88	g	14.90	g
5. PERCENT SOLIDS	65.90	%	64.54	%	64.68	%

FILTRATE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	51.00	g	52.77	g	52.46	g
3. TOTAL SAMPLE + TARE, WT	93.88	g	97.56	g	91.39	g
4. DRY SOLIDS + TARE, WT	51.49	g	53.29	g	52.90	g
5. PERCENT SOLIDS	1.13	%	1.16	%	1.14	%

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/24/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9631DUP_Paint Filter Test
TESTING METHOD:	EPA Method 9095		

After 125 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	101.52	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/24/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9631DUP_LR
TESTING METHOD:	EPA Method 9096		

After 125 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	325.40	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

FILTER PRESS TEST
REPORT FORM

PROJECT:	Hasting's Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE:	
TESTING DATE:	6/23/2014
TESTED BY:	JDM
TRACKING CODE:	9632DUP_FP

TESTING CONDITIONS	
1. CONDITIONER	No Addition
2. RUN TIME (min)	242
3. INITIAL MATERIAL WEIGHT (g)	508
4. GAGE PRESSURE (psi)	150
5. FILTRATE VOLUME (ml)	138
6. CAKE WEIGHT (g)	363.18
7. CAKE THICKNESS (in)	1.8725

FEED PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	70.56	g	63.40	g	63.73	g
3. TOTAL SAMPLE + TARE, WT	94.69	g	92.85	g	85.99	g
4. DRY SOLIDS + TARE, WT	81.35	g	76.98	g	73.94	g
5. PERCENT SOLIDS	44.73	%	46.12	%	45.87	%

CAKE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	1.29	g	1.30	g	1.30	g
3. TOTAL SAMPLE + TARE, WT	24.69	g	22.19	g	24.04	g
4. DRY SOLIDS + TARE, WT	16.22	g	14.75	g	16.64	g
5. PERCENT SOLIDS	63.79	%	64.39	%	67.47	%

FILTRATE PERCENT SOLIDS						
1. SAMPLE No.	A		B		C	
2. TARE, WT	51.02	g	52.78	g	52.51	g
3. TOTAL SAMPLE + TARE, WT	99.42	g	94.86	g	99.17	g
4. DRY SOLIDS + TARE, WT	51.55	g	53.25	g	52.99	g
5. PERCENT SOLIDS	1.10	%	1.12	%	1.02	%

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/23/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9632DUP_Paint Filter Test
TESTING METHOD:			

After 150 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	101.84	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/23/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9632DUP_LR
TESTING METHOD:	EPA Method 9096		

After 150 psi filter press

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	301.89	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

FILTER PRESS TEST
REPORT FORM

PROJECT:	Hasting's Dewatering Study
PROJECT No.:	SH0522
SAMPLE No.:	Master Composite
MATERIAL TYPE:	
TESTING DATE:	6/23/2014
TESTED BY:	JDM
TRACKING CODE:	9633DUP_FP

TESTING CONDITIONS	
1. CONDITIONER	5% Diatomaceous Earth
2. RUN TIME (min)	161
3. INITIAL MATERIAL WEIGHT (g)	525
4. GAGE PRESSURE (psi)	150
5. FILTRATE VOLUME (ml)	132
6. CAKE WEIGHT (g)	386.67
7. CAKE THICKNESS (in)	1.9685

FEED PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	1.29 g	1.29 g	1.30 g
3. TOTAL SAMPLE + TARE, WT	6.59 g	5.03 g	6.81 g
4. DRY SOLIDS + TARE, WT	3.76 g	3.03 g	3.87 g
5. PERCENT SOLIDS	46.59 %	46.58 %	46.53 %

CAKE PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	1.28 g	1.28 g	1.28 g
3. TOTAL SAMPLE + TARE, WT	21.57 g	22.86 g	21.55 g
4. DRY SOLIDS + TARE, WT	14.78 g	15.38 g	14.72 g
5. PERCENT SOLIDS	66.52 %	65.33 %	66.31 %

FILTRATE PERCENT SOLIDS			
1. SAMPLE No.	A	B	C
2. TARE, WT	52.79 g	51.00 g	52.46 g
3. TOTAL SAMPLE + TARE, WT	97.94 g	96.02 g	95.01 g
4. DRY SOLIDS + TARE, WT	53.29 g	51.51 g	52.97 g
5. PERCENT SOLIDS	1.11 %	1.13 %	1.20 %

PAINT FILTER TEST

SUMMARY OF RESULTS

PROJECT:	Hastings Dewatering Study	TESTING DATE:	6/23/2014
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9633DUP_Paint Filter Test
TESTING METHOD:			

After 150 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	100.62	**g**
LENGTH OF TEST	5.0	**min.**
QUANTITY OF LIQUID	0.00	**g**
RESULTS (PASS / FAIL) *	Pass	

* In accordance with EPA Method 9095, if any liquid from the test material collects after 5 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the paint filter test.

LIQUID RELEASE TESTING

SUMMARY OF RESULTS

PROJECT:	Hasting Dewatering Study	TESTING DATE:	6/23/14
PROJECT No.:	SH0522	TESTED BY:	JDM
SAMPLE No.:	Master Composite	TRACKING CODE:	9633DUP_LR
TESTING METHOD:	EPA Method 9096		

After 150 psi filter press
5% DE

TESTING PARAMETER AND RESULTS		
QUANTITY OF MATERIAL	308.29	**g**
LENGTH OF TEST	10.0	**min.**
RESULTS (PASS / FAIL) *	Fail	

* In accordance with EPA Method 9096, if any liquid from the test material collects on the filters after 10 minutes of testing, the material is deemed to contain free liquids, and therefore has failed the liquid release test.

Kemron 2015 Treatability Study Report:
“Phase II Soil and Water Bench Scale Treatability Study”

HASTINGS ON THE HUDSON PHASE II
Soil and Water Bench Scale Treatability Study
SH0522-02

Prepared For:

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August 10, 2015

Table of Contents

List of Tables and Appendices

1.0 INTRODUCTION

KEMRON Environmental Services, Inc. (KEMRON) is pleased to present Haley & Aldrich (H&A), with this report of the Hastings on the Hudson Phase II bench scale treatability study performed on materials sampled from the Hastings on the Hudson Site. The treatability study was conducted on four (4) materials including dewatered sediment, pore liquid (referred to as “effluent” liquid) generated during dewatering activities, site soil, and site groundwater. Testing was performed to evaluate potential solidification applications capable of improving the physical characteristics of previously dewatered sediment material as well as reduction in concentrations of metals and polychlorinated biphenyls (PCBs) potentially present in both the effluent liquid from dewatering activities and site groundwater. Testing performed during this study was conducted in general accordance with the cost proposal dated April 7, 2015, telephone and electronic mail communications between KEMRON and H&A, and information ascertained throughout the study. This report provides the methodology and protocols used, as well as the results of testing performed on the untreated and treated site materials.

2.0 MATERIAL PREPARATION, HOMOGENIZATION, AND CHARACTERIZATION

Based on the results of the Hastings on the Hudson Phase I treatability study a positive pressure dewatering application was selected to for potential full-scale site dewatering activities. KEMRON employed numerous simulations of this dewatering technique using a Baroid filter press operating at a pressure of 50 pounds per square inch (psi) and utilizing a filter media with a nominal pore size of approximately 30 microns to generate a sufficient volume of dewatered sediment material and effluent water for use in this Phase II study. For the remainder of this report, including tables and data reports, the terms “Soil-002” and “sediment” may be used interchangeably to identify the dewatered site sediment.

In addition to the dewatered sediment and effluent water, KEMRON was provided with groundwater and clean soil materials from the site. The clean site soil will be referred to as “site soil” or “Soil-001”. Prior to initiating the study KEMRON homogenized each material to ensure uniform samples for testing. The dewatered sediment material and site soil were individually homogenized by passing the sample through a mesh screen with a nominal opening size of 0.5 inches. The screened material was then homogenized by hand until visually uniform. Note that KEMRON observed that many of the dewatered sediment filter cakes varied in moisture content, however homogenization activities attempted to create a material with a uniform consistency and moisture content, however, testing performed on the dewatered sediment indicated some variability in moisture content. The following characterization testing was conducted on the dewatered sediment solids and site soil in accordance with the referenced test methods:

PARAMETER	METHOD
Moisture / Solids Content	ASTM D2216
Particle Size Distribution	ASTM D422
Atterberg Limits	ASTM D4318
Sample Description / Classification	USCS ASTM D2487
Standard Proctor Density	ASTM D698
Unconfined Compressive Strength	ASTM D 2166
Pocket Penetrometer Testing	Handheld Penetrometer

The results of characterization testing performed on the sediment and site soil materials are summarized in **Table 1** attached to this report. Review of this data indicates that the site soil exhibited a moisture content of approximately 20 percent (%), and is classified as an "SM" silty sand soil with a plasticity index of 1. When compacted to a dry density of 93.8 pounds per cubic foot (pcf), which was slightly lower than the dry density of 98.9 pcf determined by standard proctor compaction testing, the site soil had a UCS of 10.2 psi. The dewatered sediment was significantly wetter with a moisture content of 43.76% and contained significantly more fines. The sediment was classified as a "ML" silt with sand and had a plasticity index of 4. The compacted sediment material exhibited very little UCS strength.

Homogenization of the effluent water as well as the site groundwater, were conducted by gently stirring the individual liquids with stainless steel utensils until homogenous. The following testing was conducted on the dewatered sediment solids and effluent water. Following homogenization aliquots of the effluent water and the groundwater were subjected to the following analyses in accordance with the referenced test methods:

PARAMETER	METHOD
Total Suspended Solids	EPA Method 160.2
Total Dissolved Solids	EPA Method 160.1
Total PCBs (as aroclors)	EPA Method 8082A
Total Metals (Be, Cu, Pb, Zn)	EPA Method 6010C
Dissolved Metals (Be, Cu, Pb, Zn)	EPA Method 6010C

The results of testing conducted on the liquid samples are summarized in Table 2. The data presented in Table 2 shows significantly higher dissolved solids in the effluent water than the groundwater. PCB analyses conducted on the samples showed that the effluent water exhibited no PCBs above the analytical Practical Quantitation Limit (PQL) and the site groundwater contained two detectable aroclors which were identified as Aroclors 1252, and 1262. However, note that the analyses indicated that the results exhibited altered PCB patterns and were reported as the best match for these two aroclors. The results of these two PCB aroclors were relatively low concentrations. The results of metals analyses indicated that beryllium was not detected in either the effluent or groundwater materials. Copper, lead and zinc were detected at significantly higher concentrations in the effluent water than that exhibited in the groundwater sample.

Additionally, the results of dissolved metals analyses indicates that copper, and lead present in the two waters are in the dissolved state as shown in the virtually identical total and dissolved copper and lead concentrations. The results of zinc analyses indicate that approximately one-half of the zinc is present in the dissolved state. Complete analytical reports are provided in **Appendix B**.

3.0 Solidification / Bulking Evaluations

3.1 Dewatered Sediment

Evaluation of treatment simulations for the improvement of the physical properties of the dewatered sediment material took place in multiple phases of the study and included two primary treatment approaches. The first treatment option was designed to create a solidified treated material that exhibited a minimum UCS strength of 50 psi. This option would be utilized for placement and re-use of the treated sediment material at the site. The second option was to reduce any free liquids in the sediment while maintaining a relatively soil like consistency and a minimal increase in treated material volume. This second option would be used to transport and dispose of the sediment material at an off-site location without releasing any liquids during material transport.

KEMRON conducted testing of various reagent additives capable of meeting the goals of the two treatment approaches. Reagents evaluated included Type I Portland cement (Portland), Ground Granulated Blast Furnace Slag (GGBFS), Cement Kiln Dust (CKD), Lime Kiln Dust (LKD), Fly Ash from Unit #2 of the Hudson Generating Station, located in Jersey City, New Jersey, and Bottom Ash from the Unit #2 Hudson Generating Station. The mixtures were evaluated alone or in various combinations. **Table 3** presents the mixture designs evaluated during this phase of the study.

All mixtures were prepared using a bench-scale KitchenAid countertop mixer. The mixer has a 4½ quart stainless steel mixing bowl and “flat beater” type paddles. Treatment utilizing this mixing technique is intended to simulate potential full-scale remediation options, to the closest extent possible on the bench-scale. This approach is routinely utilized to simulate a wide range of potential full-scale remediation approaches, including both in-situ and ex-situ applications. Each treatment was produced by placing an aliquot of the dewatered sediment into the mixing chamber and the appropriate reagent or reagent combination was added dry to the untreated sediment. Each mixture was blended for a period of approximately 60 to 90 seconds at a rate of approximately 60 revolutions per minute (rpm).

Following the preparation of each mixture, approximately 100 grams of each treated material was compacted into a small plastic cup for curing. These small samples were utilized for pocket penetrometer testing to evaluate potential setting characteristics of the treated materials. Results of the pocket penetrometer testing are noted individually on each of the mixture design sheets provided in **Appendix C**, and are summarized on **Table 3**. KEMRON also prepared multiple cylindrical molds for the mixtures for UCS testing, and a volumetric expansion test mold. After mixture development all of the treated materials had a moist clay-like consistency. As such each material was compacted into the appropriate curing container using compaction energy similar to a standard proctor compaction. All treated materials were allowed to cure at ambient temperature (68 ˚F to 72 ˚F) in moisture-sealed containers. Throughout curing, KEMRON conducted pocket penetrometer testing to evaluate potential material setting characteristics. Results of the pocket penetrometer testing are noted individually on each of the mixture design sheets provided in **Appendix C**, and are summarized on **Table 3**. Review of the penetrometer data indicates that mixtures including a 5%, and 7% Portland cement alone addition, and a combination of 3% Portland and 7% Unit #2 fly ash achieved a maximum penetrometer result of greater than (>) 4.5 tons per square foot (TSF) after only one day of curing. Several other mixtures exceeded the 4.5 TSF limit of the penetrometer at the 7 day cure interval.

At the 7 day curing interval each treated material was subjected to UCS, paint filter, liquid release testing (LRT) and volumetric expansion (VE) determination. Volumetric expansion is intended to estimate the potential site material volume increase created from the treatment process. VE testing was conducted by compacting 100 grams of the untreated dewatered sediment material into a 2 inch diameter by 4 inch high cylindrical plastic curing mold. The volume of the untreated sediment material was determined and labelled as Initial volume. KEMRON then prepared small aliquots of each mixture design using 100 grams of dewatered sediment and the appropriate reagent formulation. Each treated material was then compacted into curing cylinders and allowed to cure in a humid environment for 7 days. At the end of the curing interval KEMRON determined the volume of the treated material inside the cylinder (labeled Final Volume) and calculated the volume increase using the following formula:

((Final Volume - Initial Volume) / Initial Volume) x 100%

Table 3 shows that all of the mixture formulations passed paint filter testing and many of the mixtures passed the LRT. Liquid release testing is a procedure designed to determine the potential for the release of free liquids from a soil material. The testing is conducted by placing an aliquot of the test material into a stainless steel chamber. A pneumatic piston under a force of 50 psi pressure compresses the sample and any free liquid is forced from the sample and is collected on an indicator or “litmus” paper that changes color in the presence of liquid. Based on the test method if any discoloration of the indicator paper is observed the sample is deemed to have failed the test. In this study LRT is being used to evaluate the potential of liquid release during transportation and as such is being evaluated subjectively. Specifically, a test that may technically fail but only shows slight spotting of the indicator paper may still be a successful candidate for off-site transportation.

The results of UCS testing presented in Table 3 shows that none of the mixtures met the 50 psi UCS strength criteria at the 7-day cure interval. Mixtures which exceeded the 4.5 TSF penetrometer test limit had UCS values ranging from 22.6 to 35.2 psi. Review of the bulk density, and moisture content testing performed during UCS testing shows relatively uniform densities were achieved for all of the treated materials, and in general the moisture content results corresponded as anticipated with the reagent type and addition rates utilized.

While UCS results indicated that none of the mixtures met the 50 psi criteria for on-site placement of the treated material, several mixtures passed both LRT and paint filter testing which indicate potential candidates for off-site transportation and disposal. Candidate off-site disposal mixtures using limited reagent addition rates that exhibited low volumetric increase, and that passed LRT and paint filter testing include a 3% addition rate of Portland cement alone, and 5% addition rates of CKD and LKD alone. Complete data sheets for paint filter, LRT and UCS testing are provided in **Appendix D.**

3.2 Dewatered Sediment and Site Soil Composite Evaluations

In addition to treatment evaluations conducted on the dewatered sediment, KEMRON was tasked with evaluating potential treatments of the sediment material combined with native soil material. This testing was conducted to determine if blending site soil with the dewatered sediment would provide beneficial solidification or disposal options during full-scale activities, or to determine if an inadvertent incorporation, or a limited incorporation of site soil with the dewatered sediment would affect treatment. KEMRON prepared five (5) combinations of dewatered sediment and site soil to determine the physical characteristics of the various blends. The following combinations were prepared and tested:

KEMRON Sample Number	Reagent Type and Identification Number(s)	Reagent Addition % by Wet Soil wt.
0522-023	Soil-002/ Site Soil-001	40/60
0522-024	Soil-002/ Site Soil-001	50/50
0522-025	Soil-002/ Site Soil-001	60/40
0522-026	Soil-002/ Site Soil-001	70/30
0522-027	Soil-002/ Site Soil-001	80/20

Soil 002 = dewatered sediment
Site Soil 001 = native site soil

For clarification, sample 0522-023 contained 40 grams of dewatered sediment and 60 grams of site soil for every 100 grams of material prepared. Individual mixture design sheets are provided in **Appendix E.**

The results of testing conducted on the 5 combinations are summarized in **Table 4.** Review of this data indicates anticipated results regarding volumetric expansion and moisture content. Specifically, the more site soil used in the combination, the higher the volumetric expansion, and the higher soil addition of the lower moisture content site soil, the lower the composite moisture content. Note that volumetric expansion estimations conducted on these materials were based on the initial volume of the sediment material alone. That is, the volume of a known quantity of dewatered sediment was determined, then the site soil was added at the appropriate ratio and the volume of the sediment and soil combination was determined and the increase in volume was calculated.

Table 4 also presents the results of liquid release, paint filter and UCS testing as well as visual observations. This information shows that all of the combinations passed paint filter testing but technically failed liquid release testing. Visual observations conducted by KEMRON indicate that the higher soil addition combinations showed very limited spotting on the LRT indicator paper, and mixtures with high sediment ratios showed more spotting but did not reveal a significant amount of indicator paper saturation. Complete data sheets for the composite soil evaluations are provided in **Appendix F.**

Based on review of the data presented in Table 4 and conversations between KEMRON and Haley and Aldrich, three sediment and site soil combinations were selected for further testing. All of the mixtures prepared on the different dewatered sediment and soil composites were prepared using Type I Portland cement alone, Portland cement combined with CKD, or with CKD alone. The mixture designs and results of testing conducted on these treatment formulations are summarized in **Table 5**.

The mixtures conducted on the composite samples were developed in accordance with the previously outlined mixture development protocol with the exception that the reagent addition was based on the amount of sediment present in the untreated sample. For instance a treatment with Composite 025 which contains a 1:1 ratio of dewatered sediment and site soil, with 10% addition rate of Type I Portland cement, for every 100 grams of dewatered sediment present, 100 grams of native site soil was added and the composite mixture was blended. KEMRON then added 10 grams of dry Portland cement to the composite and the material was blended. When viewed on a total weight basis of the sediment and soil utilized this would represent a 5% Portland addition rate.

The treated materials were then compacted into cylindrical curing molds using standard proctor energy and the samples were cured in a humid environment at ambient temperature. Throughout curing KEMRON performed pocket penetrometer testing at curing intervals of 1, 3, 5 and 7 days of curing. At the 7-day curing interval each mixture was subjected to LRT, paint filter, and UCS testing.

Review of the data presented in Table 5 show that Composites 024, and 025 treated with Portland cement alone and Portland combined with CKD, passed both LRT and paint filter testing, and exceeded the site strength criteria. Treatments prepared on these composites using only CKD indicate that these may be potential candidates for off-site transportation and disposal. However treatments conducted on these two composite materials exhibited very high volumetric expansion values ranging from 56 to 97%.

Testing conducted on the treated Composite 026 material which was a combination of dewatered sediment and site soil blended at a ratio of 80% sediment and 20% site soil showed that the Portland cement alone treatment did not quite meet the site strength requirements, but the Portland and CKD combination mixture had a UCS value of 65.3 psi. Additionally, the Portland and CKD mixture passed both LRT and paint filter testing with a volume increase of 29.48%. The CKD only treatments applied to the 026 composite failed LRT testing but the indicator paper only revealed very limited liquid spotting.

While the evaluations performed on the sediment and soil composites revealed potential treatment options for both on-site treated material placement, and off-site disposal, KEMRON believes that these applications would only be cost effective if full-scale site activities required the removal or incorporation of the native site soil.

3.3 Additional Sediment Treatment Evaluations

Because a potential candidate dewatered sediment treatment had not been identified which was capable of meeting the site strength criteria, KEMRON prepared three additional mixtures using slightly higher reagent addition rates. Specifically, KEMRON prepared a 10% Portland cement alone mixture, and two combinations of Portland cement and CKD utilizing a 5% Portland addition for both treatments and CKD additions of 5 and 7.5%. The results of testing conducted on these additional dewatered sediment mixtures are also summarized in Table 5. These results show that all of the treatments passed both LRT and paint filter testing, but only the 10% Portland cement alone mixture exceeded the strength criteria with a UCS value of 65.3 psi.
The final three mixtures, 043, 044, and 045, which are outlined in Table 5 represent treatment simulations conducted on the raw non-dewatered sediment material from the site to evaluate the effects that moisture content may have on treatment effectiveness. Review of the moisture content data generated from UCS testing of various mixtures during this study indicated that there may not be sufficient moisture present in the dewatered sediment material or in the sediment and soil composite materials to fully hydrate pozzolanic reagents used in the treatments. These three mixtures were developed to evaluate the effect that moisture content has on potential treated strengths. The treatments prepared using the raw site sediment material included a 10% Portland cement treatment, a 5% Portland and 5% CKD mixture, and a 5% Portland and 7.5% CKD addition. The results of testing conducted on these mixtures show that mixtures 043 and 044 passed LRT and paint filter but mixture 045 which contained a higher total reagent addition rate than mixture 044 failed the LRT. The results of LRT evaluations may indicate potential moisture variability in the raw sediment material. Additionally the mixture containing the 10% Portland cement addition achieved a UCS value of 76.1 psi. The additional dewatered sediment and raw sediment treatment mixtures indicate that a 10% Portland cement additions is capable of exceeding the site strength requirements and that a higher strength was achieved on the raw sediment treatment.

4.0 EFFLUENT AND GROUNDWATER TREATMENT EVALUATIONS

KEMRON performed precipitation, carbon adsorption, and filtration treatment simulations on the sediment effluent and site groundwater to evaluate the potential reduction in metals and/or PCBs.

4.1 Precipitation Testing

Precipitation testing was performed to determine the effectiveness of precipitating metals through the addition of chemical and pH adjustment additives. All precipitation testing was conducted on effluent and groundwater.

Initially KEMRON evaluated numerous additives on small batches of approximately 50 ml of the effluent water only. All of the additives were introduced as relatively weak solutions and included:

Ferric Chloride
Ferrous Sulfate
Calcium Chloride
Sodium Sulfate
Sodium Sulfide
Sodium Hydroxide
Hydrated Lime

The results of these preliminary tests indicated that ferric chloride and ferrous sulfate produced a limited amount of precipitate; however, these additives produced significantly discolored water, ranging from green to red depending on the addition rate and reaction time. While these additives did produce some precipitation, the resulting treated water discoloration indicated that these materials may not be the most suitable option for site applications. Testing using calcium chloride, sodium sulfate and sodium sulfide did not produce any visual precipitate. Sodium hydroxide and hydrated lime produced more promising water clarity and precipitate formation at elevated treated pH values ranging from 8.5 to 10.5 standard units (s.u.). The precipitate created from the sodium hydroxide solution and lime slurry was in the form of white fluffy particulates that settled from suspension.

As a result of the preliminary test evaluations, a 0.1 Normal (N) sodium hydroxide solution, and a 1.0 Molar (M) hydrated lime slurry were selected for further testing. KEMRON conducted additional larger batch treatments consisting of 100ml aliquots of the pre-filtered sediment effluent using the sodium hydroxide and lime. The individual additives were introduced into the effluent water to target pH values of 8.5, 9.5 and 10.5 standard units to evaluate visual precipitate formation. In general the additional testing using just the sodium hydroxide solution and lime slurry indicated that the hydrated lime slurry produced significantly more solids than the sodium hydroxide. This is likely due to the fact that the lime slurry introduces lime solids into the treatment system which often aids in the formation of larger particulates, and adds suspended solids to the water. Additionally, KEMRON observed an increase in particulate formation in higher pH treatments.

Because of the trend of visually greater precipitation and better water clarity with increased pH target values, KEMRON prepared additional treatments using a target pH of 11.5 s.u. These treatments indicated that the NaOH treatment did not provide a significant increase in water clarity or flocculent formation at a higher target pH, but the lime slurry treatment produced significantly more precipitate and slightly better water clarity. The suspended solids in 11.5 pH lime slurry treatment did not appear to settle as well as other treatments and KEMRON introduced a coagulant polymer into the water to aid in settling. Specifically, KEMRON added ECA 1350 which is manufactured by Emulsions Control Inc. at a rate of approximately 750 parts per million based on just the quantity of test water being treated. Visual observations indicated that the coagulant increased the rate of settling.

Based on the visual results of all of the preliminary testing conducted by KEMRON, material pH adjustments using sodium hydroxide and hydrated lime slurries were selected for analytical treatment evaluations of the sediment effluent water and groundwater. The following treatment parameters were tested on the water materials:

Untreated Water	Additive	Target pH (s.u.)
Effluent	0.1N NaOH	10.5
Effluent	1.0M Hydrated Lime	9.5
Effluent	1.0M Hydrated Lime	10.5
Effluent	1.0M Hydrated Lime	11.5
Effluent	1.0M Lime Slurry + ECA	10.5
Effluent	1.0M Lime Slurry + ECA	11.5
Groundwater	0.1N NaOH	10.5
Groundwater	1.0M Hydrated Lime	9.5
Groundwater	1.0M Hydrated Lime	10.5
Groundwater	1.0M Hydrated Lime	11.5
Groundwater	1.0M Lime Slurry + ECA	10.5
Groundwater	1.0M Lime Slurry + ECA	11.5

Note that where utilized, the ECA 1350 coagulant was added following pH adjustment. The ECA 1350 was added based on the volume of untreated water being utilized and was added to a target concentration of approximately 750 parts per million (ppm).

Following review of the observations from preliminary testing, KEMRON conducted potential full-scale treatment simulations on both the sediment effluent water and the site groundwater in order to analytically quantify the reduction in metals concentrations. The treatments were conducted by placing 750 ml aliquots of each water type into clean

1,000ml beakers. The sodium hydroxide or hydrated lime slurry was introduced until the target pH value was reached, determined using a handheld digital pH meter. Note that because the lime slurry is a suspension of lime in water and not a true solution, the lime slurry was constantly stirred prior to introducing into the test water. During pH adjustments the test beakers were continually stirred to ensure a stable pH value was reached and maintained. Once the target pH was achieved and stabilized, stirring was discontinued and the material was allowed to settle. For treatments using pH adjustment and the ECA 1350, the appropriate pH value was achieved and then the ECA 1350 was added to the mixture and stirred vigorously for approximately 15 seconds and then allowed to settle. A summary of the 12 water treatments are summarized in **Table 6**. Photographic documentation of the precipitation testing is included in the Photographic Log attached to the report appendices.

Following pH adjustment and settling, the treated materials were then filtered through a 10 micron filter media using a vacuum filtration apparatus. Approximately 250 ml of the filtered water was then sampled for total metals analyses. The remaining water was then filtered through a 0.45 filter media and sampled for dissolved metals analyses. For comparison purposes, KEMON forwarded aliquots of untreated sediment effluent and site groundwater which had been filtered through 10 and 0.45 micron filter media for analytical testing. The results of analytical testing performed on the untreated and precipitation water treatments are included in **Table 7**

Review of Table 6 indicates that the untreated sediment effluent water exhibited detectible concentrations of copper, lead and zinc, with copper detected at the highest concentration of 814 ug/L on a total basis and 818 ug/L as dissolved copper. The results show that the total and dissolved copper and lead concentrations were virtually identical, indicating that these metals are present in the water as dissolved constituents. Approximately one-half of the zinc present was in the dissolved state, and beryllium was not detected above the analytical reporting limits. Review of the treated effluent analytical results show that copper concentrations were significantly reduced in all treatments with the lowest value of 28.9 ug/L recorded for the 11.5 s.u. pH adjustment using the 1.0 M hydrated lime slurry alone. Beryllium, lead and zinc were not detected in any of the treated effluent waters at concentrations above the analytical reporting limits.

The results of precipitation testing conducted on the site groundwater showed that the untreated groundwater exhibited significantly lower concentrations of total and dissolved copper, lead and zinc, and that beryllium was not detected in the untreated material. Review of analyses performed on the treated groundwater materials indicate that all metals were reduced to non-detectible concentrations in the 10.5 s.u. sodium hydroxide treatment, and in the 10.5 and 11.5 s.u. lime slurry treatments. Concentrations of copper were not reduced in the 9.5 s.u. lime slurry treatment or in the lime treatments where the ECA 1350 coagulant was utilized, and zinc was reduced by approximately 50% in the 11.5 s.u. lime slurry treatment followed by coagulation using the ECA 1350 material polymer. Complete analytical reports for the precipitation evaluations are provided in **Appendix G.**

To summarize the precipitation treatment for metals reduction in the sediment effluent and site groundwater materials as documented throughout testing and summarized in Tables 5 and 6 indicate the following:

- The buffering capacity of the sediment effluent is much greater than the groundwater
- The sediment effluent water contains significantly higher concentrations of the metals of concern than the groundwater sample.
- Copper appears to be the most problematic metal contained in the water materials
- Treatment using a 1.0 molar hydrated lime slurry applied to a target pH of 11.5 s.u. reduced copper from a concentration of 814 ug/L in the untreated material to a concentration of 28.9 ug/L., and reduced all other metals to non-detectible concentrations.
- The use of ECA 1350 appears to reduce the effectiveness of pH treatment. The , and significantly lower volumes of hydrated lime is required to adjust the pH in both waters

4.2 Carbon Adsorption Testing

Carbon adsorption testing was conducted to evaluate the potential removal of PCBs from the site groundwater using granular activated carbon (GAC). Because of the non-detectible PCB results reported during Untreated Material Characterization testing, the sediment effluent water was not evaluated during carbon treatment. The site groundwater was passed through two different GAC materials at empty bed contact times (EBCT) of 10 and 20 minutes for a total of four column tests.

KEMRON prepared the four separate treatment columns with the following parameters:

Carbon Type	Water ID	Column Dimensions (1)			EBCT (min)	Groundwater Flow Rate (ml/min)
		Height (cm)	Diameter (cm)	Volume (cm^3)		
OLC 12x40	Groundwater	4.72	2.54	23.92	10	2.39
OLC 12x40	Groundwater	50.8	3.81	579.12	20	28.95
F-400	Groundwater	4.83	2.54	24.47	10	2.44
F-400	Groundwater	50.8	3.81	579.12	20	28.95

NEED SOME ADDITIONAL INFORMATION ABOUT THE CARBON. SUPPLIERS, COAL OR COCONUT BASED, ETC.

Prior to introducing the groundwater into the columns KEMRON passed approximately 1 liter of deionized water through each column in order to prepare the carbon for testing and to adjust the peristaltic pumps to the target water flow rate. The site groundwater was then passed through the carbon columns from the bottom of the column to the top and the effluent from each column was collected and submitted for total PCB analyses. The results of these analyses are presented in **Table 8**. Review of the analytical data shows that no PCB Aroclors were detected at a concentration above the analytical Practical Quantitative Limit in any of the carbon treated groundwater samples. Complete analytical report for carbon adsorption testing is provided in **Appendix H.**

4.3 Water Filtration Testing

KEMRON performed filtration testing on the site groundwater to evaluate potential reductions in metals and PCB concentrations through filtration. Filtration testing was also conducted on an additional sediment effluent material generated from dewatering of a second site sediment sample that potentially contained higher concentrations of PCBs than the original sediment.

Filtration testing was conducted on the site groundwater by filtering the water through filter media with pore sizes of 100, 10, 1.0, 0.45, and 0.1 microns using a vacuum filtration apparatus. Specifically, approximately 8 liters of groundwater was passed through the 100 micron filter media and an aliquot of that filtrate was removed and sampled for total PCBs as well as total and dissolved beryllium, copper, lead and zinc analyses. The remaining water was the filtered through a 10 micron filter media and the analytical samples for PCBs and metals were collected. This process was continued for the remaining filter media. The results of PCB analyses performed on the site groundwater is summarized in **Table 9**, and the results of total and dissolved metals analyses are summarized in **Table 10**.

The additional sediment effluent sample was generated by dewatering using a 50 psi positive pressure baroid filter press application equipped with a 30 micron filter media. The resulting effluent material was then filtered through filter media with pore sizes including 10, 1.0, 0.45, and 0.1 microns. Note that because dewatering activities were performed using a dewatering technique that included a 30 micron filter media KEMRON did not perform filtration evaluations using the 100 micron filter. Filtration was conducted using the previously identified filtration protocol with the exception that only total PCB analyses were performed on the filtered effluent waters. The results of total PCBs are also summarized in **Table 9**.

Review of Tables 9 and 10 show that filtration of the groundwater material had no apparent effect on total and dissolved metals concentrations. The results of PCB analyses indicate that Aroclor 1254 was only reported at a concentration of 0.0865 ug/L for the groundwater filtered through the 10 micron media, and that Aroclor 1262 was detected in all of the filtered groundwater samples. Note that both Aroclor 1254 and 1262 were reported as altered PCB analytical patterns, however, the reported values represent the best matches for these Aroclors. Further review indicates possible heterogeneity in the test samples due to the fact that the 10 micron filtered groundwater exhibited a higher Aroclor 1262 concentration than the 100 micron filtered sample. In general the results indicate that some reduction in Aroclor 1262 may be occurring from subsequent filtration through smaller pore size media but this trend is difficult to verify due to the already low PCB concentrations reported. The results of PCB analyses conducted on the filtration evaluations of the additional effluent material indicate that no PCBs were detected above the analytical Practical Quantitative Limit. Complete analytical reports for filtration evaluations testing are provided in **Appendix I.**

4.4 Combined Effluent and Groundwater Treatment Testing

To evaluate if a single treatment system could meet all of the site criteria for water discharge KEMRON performed testing of a single water Master Composite prepared using a one to one (1:1) ratio of sediment effluent and site groundwater. Once the Master Composite water was prepared, KEMRON submitted aliquots of the water for total PCBs and total and dissolved metals analyses.

The treatment of the Master Composite water consisted of multiple technologies including filtration through a 1.0 micron filter media, GAC adsorption using the F-400 carbon column with a EBCT of 10 minutes, followed by pH adjustment using a 1.0 Molar hydrated lime slurry with a target pH of 11.5 s.u. Specifically, 8 liters of the sediment and 8 liters of the site groundwater were combined and homogenized. Aliquots of this 16 liter Master Composite were then sampled and submitted for total PCBs, total and dissolved metal analyses. The remaining Master Composite material was then passed through a vacuum filtration apparatus equipped with a 1.0 micron filter paper. Following filtration, aliquots of the filtered water were submitted for total PCBs, total and dissolved metals analyses. The remaining filtrate was then passed through the F-400 GAC column and the effluent water was sampled and submitted for PCB and metals analyses. Finally, the remaining pre-treated water, filtered and carbon treated, was adjusted to a pH of 11.5 s.u. using the hydrated lime slurry. This final pH adjusted sample was then filtered through a 10 micron filter media and aliquots of the water were sampled for total PCBs and metals analyses. The remaining water was then filtered through a 0.45 filter media and sampled for dissolved metals analyses.

The results of analytical testing performed on the untreated and treated Master Composite materials are summarized in Tables 11 and 12. Table 11 summarizes the results of total PCB analyses, and shows that Aroclor 1262 was the only PCB Aroclor detected in the untreated Master Composite at a concentration of 1.34 ug/L. Filtration of the Master Composite water reduced the concentration of Aroclor 1262 to 0.0269 ug/L, and carbon treatment using the F400 GAC with an EBCT of 10 minutes further reduced the concentration Aroclor 1262 to below the analytical practical quantitation limit. The metals analyses, summarized in Table 12, shows that copper and lead were the only metals detected in the untreated Master Composite. Copper and zinc were detected at total concentrations of 718 and 205 ug/L respectively. The dissolved concentration of copper was detected at 423 ug/L and dissolved zinc was detected at a concentration of 97.3 ug/L. The untreated Master Composite exhibited higher concentrations of copper that was not in the dissolved state than either the sediment effluent or the site groundwater. This may indicate that some chemical precipitation of copper may have occurred when the two water materials were composited.

The results of analytical testing on the different treatment applications in the treatment train system shows that filtration of the Master Composite using the 1.0 micron media removed virtually all of the copper and zinc that was not in the dissolved state and had little or no effect on the dissolved metals. Carbon treatment with the F400 GAC further reduced concentrations of copper and zinc to below or near the analytical reporting limit. Treatment using a 1.0 Molar hydrated lime slurry to increase the pH of the Master Composite to approximately 11.5 s.u. reduced the copper and zinc to concentrations below the analytical reporting limit.

5.0 CONCLUSIONS AND RECOMMENDATIONS

The Hastings on the Hudson Phase II Treatability Study was performed to evaluate potential treatment applications for on-site re-use or off-site disposal of dewatered sediment solids, and subsequent treatment of effluent water generated from dewatering activities. This report should be reviewed in its entirety including all attachments prior to making decisions concerning a remedial approach. This study is intended to suggest what will occur in the field but does not guarantee the same results.

KEMRON evaluated numerous solidification application mixture formulations designed to either increase the UCS strength of the sediment material to greater than 50 psi for on-site placement of the treated materials, or to reduce any free liquids in the dewatered sediments, as determined by the LRT, in order to safely transport the dewatered material to an off-site disposal facility. Reagents utilized were common, available materials including Type I Portland cement, blast furnace slag, LKD, CKD, fly ash and bottom ash. Review of testing performed on initial mixture designs indicates that none of the treated materials met the 50 psi UCS criteria. The highest UCS achieved was 35.2 psi using a 7% addition of Portland cement. Many of these mixtures however, did pass LRT testing which indicates a potentially suitable material for off-site transportation and disposal. Potential candidate off-site disposal treatments may include a 3% Portland addition, 5% cement kiln dust addition, or a 5% lime kiln dust addition. Note that other mixtures may be suitable for off-site transportation but the mixtures previously outlined above represent materials with low reagent addition rates and that passed the LRT.

KEMRON also evaluated combinations of dewatered sediment combined with site soil. These tests were conducted to determine if the incorporation of native site soil with the sediment material would have any potential benefit for full-scale treatment activities. The results of the sediment and site soil only testing, found in Table 4 shows that none of the test composites passed paint filter or provided any significant increase in UCS strength. The table indicates that composite mixtures utilizing a high ratio of site soil may provide a suitable material for off-site disposal due to very limited liquid released from the test materials during LRT evaluations. However, these composites may not be cost effective alternatives due to the increase in the total volume of material that would be transported and disposed.

Despite the increase in volume created by compositing the sediment and site soil, three sediment and soil composite materials were subjected to solidification treatments because KEMRON understands that it may be necessary to remove a certain amount of native site soil in order to facilitate site activities, and that there is potential for inadvertent incorporation of soil and sediment during full-scale events. The three composite materials included a 50:50 mixture of sediment and site soil, a 60:40 mixture, and an 80:20 composite. Several treatments were identified which met UCS strength requirements and passed the LRT.

Additionally, KEMRON identified that treatment of the dewatered sediment using a 10% addition rate of Portland cement exceeded the 50 psi strength criteria. The highest strength achieved in the entire study was exhibited with a 10% Portland cement addition applied to the non-dewatered raw sediment material. This treatment result indicates that dewatering of the site sediment material may not be required for successful treatment. However, these results may be dependent on the actual moisture content of the dredged sediments. Various testing previously conducted on the non-dewatered raw sediments evaluated by KEMRON indicates an ASTM moisture content ranging from approximately 98 to 110%.

Testing of the sediment effluent water, site groundwater and a Master Composite water comprised of a combination of the two water samples show very good treatment possibilities. For the sediment effluent water, a pH adjustment to 11.5 s.u. using a 1.0 molar hydrated lime slurry was capable of reducing total copper concentrations from 814 ug/L in the untreated effluent water to approximately 30ug/L in the treated sample. The pH adjustment reduced all other metals to concentrations below the analytical reporting limit. The site groundwater exhibited significantly lower metals concentrations than the effluent water, and the hydrated lime slurry pH adjustment to 11.5 s.u. reduced all metals to below the analytical reporting limit.

Carbon adsorption column testing conducted was conducted only on the site groundwater material and the analytical results show that both GAC samples were capable of reducing PCBs to non-detectable concentrations with only a 10 minute EBCT. The results of metals analyses conducted on the carbon treated groundwater.

Filtration testing was performed on the site groundwater and an additional sediment effluent water which was anticipated to contain higher concentrations of PCBs than the original sediment effluent. Determining the effectiveness of PCB reduction through filtration is difficult to establish due to the low concentrations exhibited in the untreated material. However, filtration testing did indicate possible PCB reductions by an order of magnitude using the 100 micron filter media. The additional dewatered sediment water did not exhibit detectible PCBs in any of the filtered waters. Metals analyses conducted on the filtered site groundwater material indicate that no discernable reduction in metals was achieved through filtration treatment.

Evaluation of the Master Composite water material did show a noticeable reduction in the PCB Aroclor 1262 through filtration through a 0.1 micron filter media, and the Aroclor was further reduced by GAC treatment. The metals analyses conducted on the treated Master Composite indicated that some precipitation may have occurred in the only metals, copper and zinc, by combining the sediment effluent and the site groundwater. Filtration through the 1 micron filter media achieved significant reductions in these metals, and copper was reduced to a non-detectable concentration following GAC treatment. The analyses indicates pH adjustment to 11.5 s.u. was necessary to reduce zinc was not reduced to non-detectable concentrations.

If you have any questions concerning the data provided in this report, please do not hesitate to contact us at 404-601-6927.

Sincerely,
KEMRON Environmental Services, Inc.

Mark Clark
Senior Technologist

Tommy A. Jordan, P.G
Program Manager

Table 4

Composite Mixture Evaluations
Mixture Designs, Pocket Penotrometer, Volumetric Expansion, Liquid Release Test, Paint Filter, Unconfined Compressive Strength

KEMRON Sample Number	Reagent Type and Identification Number(s)	Reagent Addition % by Wet Soil wt.	Cure Day	Pocket Penotrometer (TSF)	Volumetric Expansion (%)	Liquid Release Test (Pass/ Fail) EPA 9096	Paint Filter (Pass/Fail) EPA 9095	Unconfined Compressive Strength ASTM D2166: Moisture Content (%)	Unconfined Compressive Strength ASTM D2166: Bulk Density (lb/ft^3)	Unconfined Compressive Strength ASTM D2166: Dry Density (lb/ft^3)	Unconfined Compressive Strength ASTM D2166: UCS (lb/in^2)	Observations
0522-023	Soil-002/ Site Soil-001	40/60	3	0.5	121.93	Fail	PASS	27.2	111.4	87.5	0.6	The soil mixture appears to be free of liquid, not flowable, slightly past optimum, and workable. Appears to be drier than other mixtures. The liquid release test shows only one or two blots on the litmus paper.
0522-024	Soil-002/ Site Soil-001	50/50	3	0	81.40	Fail	PASS	30.5	110.0	84.3	0.6	The soil appears to be slightly past the optimum, no free liquid observed, and very workable. We observe a couple larger drops than mix 0522-023 and some staining on the edges.
0522-025	Soil-002/ Site Soil-001	60/40	3	0.5	54.44	Fail	PASS	33.0	109.4	82.3	0.6	The soil mixute appeared to be free of liquid, slightly wet, and workable. Failed the liquid release test by a few drops of liquid.
0522-026	Soil-002/ Site Soil-001	70/30	3	0.5	33.87	Fail	PASS	33.3	112.0	84.0	0.6	The soil appeared to be free of liquid, but slightly wetter than the previous soil mixtures. Failed the liquid release test with more wet spots on the litmus paper than 0522-025.
0522-027	Soil-002/ Site Soil-001	80/20	3	0	18.69	Fail	PASS	40.9	110.0	78.1	0.6	The soil appears to be wet, softer when pressed compare to other mixtures. Free of liquid, and workable; failed the liquid relese test most noticeabloly.

Notes:
% = Percent
lb/ft^3 = pounds per cubic foot
TSF = Tons per square foot
Wt= Weight
lb/in^2 = pounds per square inch

Table 5

Composite Mixtures Solidification Evaluations
Mixture Designs, Pocket Penotrometer, Volumetric Expansion, Liquid Release Test, Paint Filter, Unconfined Compressive Strength

KEMRON Sample Number	Untreated Material Type	Reagent Type and Identification Number(s)	Reagent Addition % by Wet Soil wt.	Pocket Penotrometer (TSF)			Cure Day	Volumetric Expansion (%)	Liquid Release Test (Pass/ Fail)	Paint Filter (Pass/Fail)	Unconfined Compressive Strength ASTM D2166				Observation
				1 Day	3 Day	5 Day			EPA 9096	EPA 9095	Moisture Content (%)	Bulk Density (lb/ft^3)	Dry Density (lb/ft^3)	UCS (lb/in^2)	
0522-028	Composite 024	Type I Portland Cement #842	12.5	>4.5	>4.5	>4.5	7	97.17	Pass	Pass	25.22	116.1	92.70	71.5	The soil appears to be on the dry side of optimium and does not appear to have flowable qualities. No free liquid observable. Material is workable.
0522-029	Composite 024	Type I Portland Cement #842/Cement Kiln Dust #965	7.5/7.5	>4.5	>4.5	>4.5	7	91.77	Pass	Pass	25.98	114.3	90.8	56.4	The soil appears to be on the dry side of optimium and does not appear to have flowable qualities. No free liquid observable. Material is workable.
0522-030	Composite 024	Cement Kiln Dust #965	5.0	1.5	1.5	3.5	7	86.39	Pass	Pass	27.68	115.4	90.3	9.0	The soil appears to be a litle more moist than SH0522-029, holds the shape when squeezed, no free liquid observed, not flowable, workable.
0522-031	Composite 024	Cement Kiln Dust #965	7.5	3.75	3.0	3.25	7	90.53	Pass	Pass	26.43	115.9	91.6	14.1	The soil appears to be very simillar in dryness compared to the previous soil mixture (0522-030), no significant difference observed.
0522-032	Composite 025	Type I Portland Cement #842	10.0	4.25	>4.5	>4.5	7	88.42	Pass	Pass	26.88	113.1	89.2	63.0	The soil appers to be dry and fairly non-cohesive
0522-033	Composite 025	Type I Portland Cement #842/Cement Kiln Dust #965	7.5/7.5	>4.5	>4.5	>4.5	7	64.61	Pass	Pass	26.33	114.0	90.3	63.4	The soil appears to be dry and non-cohesive
0522-034	Composite 025	Cement Kiln Dust #965	5.0	1.0	1.0	3.0	7	56.02	Fail	Pass	29.64	114.0	87.9	7.4	The soil appears to be mioist, no free liquid observed. Howver it failed the LRT test with one small blot. See photographic log.
0522-035	Composite 025	Cement Kiln Dust #965	7.5	3.0	3.0	>4.5	7	58.98	Pass	Pass	29.33	115.1	89.0	14.2	The soil appears to be moist, but slightly drier than the soil mixture (0522-034)
0522-036	Composite 027	Type I Portland Cement #842	7.5	>4.5	>4.5	>4.5	7	22.00	Pass	Pass	31.70	110.4	83.8	43.1	The soil appears to be dry, fairly non-cohesive.
0522-037	Composite 027	Type I Portland Cement #842/Cement Kiln Dust #965	5.0/7.5	>4.5	>4.5	>4.5	7	29.48	Pass	Pass	28.75	113.4	88.1	55.9	The soil appears to be dry, no free liquid observed, not flowable, workable.
0522-038	Composite 027	Cement Kiln Dust #965	4.0	0.5	1.0	1.0	7	19.48	Fail	Pass	34.93	111.4	82.5	8.0	The soil appears to be moist, fairly cohesive. Failed the LRT test by one wet spot. See photographic log.
0522-039	Composite 027	Cement Kiln Dust #965	6.0	1.0	1.0	2.0	7	19.52	Fail	Pass	39.76	111.4	79.7	11.0	The soil appears to be moist, no noticeable difference compared to previous soil mixture (0522-038).
0522-040	Soil- 002	Type I Portland Cement #842	10.0	>4.5	>4.5	>4.5	7	4.07	Pass	Pass	34.70	110.0	81.7	65.3	The soil appears to be dry, not very cohesive
0522-041	Soil-002	Type I Portland Cement #842/Cement Kiln Dust #965	5.0/5.0	4.5	>4.5	>4.5	7	4.41	Pass	Pass	36.03	110.7	81.4	41.9	The soil appears to be dry, farly non-cohesive
0522-042	Soil-002	Type I Portland Cement #842/Cement Kiln Dust #965	5.0/7.5	>4.5	>4.5	>4.5	7	6.23	Pass	Pass	34.40	111.2	82.8	48.7	The soil appears to be dry, fairly non-cohesive.
0522-043	Raw Sediment	Type I Portland Cement #842	10.0	3.0	>4.5	>4.5	7	18.14	Pass	Pass	55.64	100.6	64.6	76.1	The soil apperas to be dry, formed pepple to cobble size . The soil was gently smashed in order to minimize air space.
0522-044	Raw Sediment	Type I Portland Cement #842/Cement Kiln Dust #965	5.0/5.0	1.0	3.5	4.0	7	15.21	Pass	Pass	54.73	101.8	65.8	32.4	The soil appears to be very similar to the previous soil mixture (0522-043),
0522-045	Raw Sediment	Type I Portland Cement #842/Cement Kiln Dust #965	5.0/7.5	1.0	>4.5	>4.5	7	17.64	Fail	Pass	49.55	102.3	68.4	47.0	The soil appears to be very similar to the previous soil mixtures (0522-043, 0522-044), However, some wet spots were noticed on the LRT paper.

Notes:
s.u. = Standard Units
% = Percent
lb/ft^3 = pounds per cubic foot
lb/in^2 = pounds per square inch
UCS = Unconfined Compressive Strength
TSF = Tons per square foot
Wt= Weight
* = Value may not used due to the variability in the compaction effort applied.

HALEY AND ALDRICH
HASTINGS ON THE HUDSON PHASE II
KEMRON PROJECT No. SH0522-02

Table 6

Summary of Water Precipitation Treatment

KEMRON Sample Number	Water ID	Additive	Treated pH (s.u.)	Additive Addition rate (%)	Observations
#1	Effluent	0.1 Normal NaOH	10.5	21.7	Good flocculent formation
#2	Effluent	1.0 Molar Hydrated Lime Slurry	9.57	1.4	Good flocculent formation
#3	Effluent	1.0 Molar Hydrated Lime Slurry	10.48	1.9	Excellent flocculent formation, water clarity increased
#4	Effluent	1.0 Molar Hydrated Lime Slurry	11.5	3.7	Excellent flocculent formation, flocculent slow to settle, water clarity increased
#5	Effluent	1.0 Molar Hydrated Lime Slurry + ECA 1350 (750 ppm)	10.49	1.9 / 0.075	Excellent flocculent formation, ECA 1350 increased flocculent settling rate, good water clarity
#6	Effluent	1.0 Molar Hydrated Lime Slurry + ECA 1350 (750 ppm)	11.56	3.6 / 0.075	Excellent flocculent formation, ECA 1350 increased flocculent settling rate, slightly better water clarity
#1	Groundwater	0.1 Normal NaOH	10.55	5.33	No precipitation observed
#2	Groundwater	1.0 Molar Hydrated Lime Slurry	9.58	0.07	Very slight precipitation observed
#3	Groundwater	1.0 Molar Hydrated Lime Slurry	10.52	0.13	Very slight precipitation observed
#4	Groundwater	1.0 Molar Hydrated Lime Slurry	11.49	0.23	large flocculent produced
#5	Groundwater	1.0 Molar Hydrated Lime Slurry + ECA 1350 (750 ppm)	10.57	0.15 / 0.075	Very slight precipitation observed with lime addition. Forms large flocculent when ECA 1350 is added.
#6	Groundwater	1.0 Molar Hydrated Lime Slurry + ECA 1350 (750 ppm)	11.51	0.23 / 0.075	Thick flocculent created, settles fairly well.

Notes:
% = Percent
ECA 1350 - Manufactured by Emulsion Control Inc. Whe used, the ECA 1350 was added to a concentration of approximately 750 parts per million to the pH adjusted waters

HALEY AND ALDRICH
HASTINGS ON THE HUDSON PHASE II
KEMRON PROJECT No. SH0522-02

Table 7

Summary of Water Precipitation Treatment Metals Analysis
Total and Dissolved Metals

Sample ID	Water ID	Additive	Treated pH (s.u.)	Summary of Metals Analyses								Total Dissolved / Total Suspended Solids	
				Beryllium ug/L		Copper ug/L		Lead ug/L		Zinc ug/L		TDS mg/L	TSS mg/L
				Total	Dissolved	Total	Dissolved	Total	Dissolved	Total	Dissolved		
Untreated	Effluent	None	NA	ND	ND	**814**	**818**	**25.5**	**27**	**116**	**57.5**	10,299	42
#1	Effluent	0.1 Normal NaOH	10.5	ND	ND	**89.3**	**70.6**	ND	ND	ND	ND	10,027	8
#2	Effluent	1.0 Molar Hydrated Lime Slurry	9.57	ND	ND	**120**	**111**	ND	ND	ND	ND	10,160	3
#3	Effluent	1.0 Molar Hydrated Lime Slurry	10.48	ND	ND	**40.7**	**37**	ND	ND	ND	ND	10,151	4
#4	Effluent	1.0 Molar Hydrated Lime Slurry	11.5	ND	ND	**28.9**	**31**	ND	ND	ND	ND	9,543	2
#5	Effluent	1.0 Molar Hydrated Lime Slurry + ECA 1350 (750 ppm)	10.49	ND	ND	**64.5**	**64.1**	ND	ND	ND	ND	10,329	6
#6	Effluent	1.0 Molar Hydrated Lime Slurry + ECA 1350 (750 ppm)	11.56	ND	ND	**58.8**	**58.8**	ND	ND	ND	ND	10,675	0
Untreated	Groundwater	None	NA	ND	ND	**4.1 J**	**5.6 J**	**2.4 J**	**2.0 J**	**24.2 J**	**17.1 J**	1,575	261
#1	Groundwater	0.1 Normal NaOH	10.55	ND	ND	ND	ND	ND	ND	ND	ND	1,087	0
#2	Groundwater	1.0 Molar Hydrated Lime Slurry	9.58	ND	ND	**5.2**	**7.5**	ND	ND	ND	ND	1,452	0
#3	Groundwater	1.0 Molar Hydrated Lime Slurry	10.52	ND	ND	ND	ND	ND	ND	ND	ND	1,059	2
#4	Groundwater	1.0 Molar Hydrated Lime Slurry	11.49	ND	ND	ND	ND	ND	ND	ND	ND	726	4
#5	Groundwater	1.0 Molar Hydrated Lime Slurry + ECA 1350 (750 ppm)	10.57	ND	ND	**6.6**	**8.5**	ND	ND	ND	ND	1,184	7
#6	Groundwater	1.0 Molar Hydrated Lime Slurry + ECA 1350 (750 ppm)	11.51	ND	ND	NR	**6.1**	ND	ND	**11.6**	ND	1,319	6

Notes:
Analytical results were provided to KEMRON by Haley and Aldrich
ug/L - Micrograms per liter
NA - Not Applicable
ND - Not detected above the analytical limits
NR - Not reported
J - Estimated concentration detected between the analtytical reporting limit (RL) and the method detection limit (MDL)

HALEY AND ALDRICH
HASTINGS ON THE HUDSON PHASE II
KEMRON PROJECT No. SH0522-02

Table 8

Groundwater Carbon Adsorption Treatment
Summary of Total PCBs

Carbon Type	Water ID	EBCT (min)	PCB Arocolor (ug/L)								
			1016	1221	1232	1242	1248	1254	1260	1262	1268
OLC	Groundwater	10	ND	ND	ND	ND	ND	ND	ND	ND	ND
OLC	Groundwater	20	ND	ND	ND	ND	ND	ND	ND	ND	ND
F-400	Groundwater	10	ND	ND	ND	ND	ND	ND	ND	ND	ND
F-400	Groundwater	20	ND	ND	ND	ND	ND	ND	ND	ND	ND

Notes:
ug/L = Micrograms per Liter
ND = Not detected above the analytical Practical Quantitative Limit
OLC = Granular activated carbon provided by Calgon Carbon
F-400 = Granular activated carbon provided by Calgon Carbon

Table 9

Water Filtration Evaluations
Summary of Total PCBs

KEMRON Sample Number	Water ID	PCB Arocolor (ug/L)								
		1016	1221	1232	1242	1248	1254	1260	1262	1268
100 micron	Groundwater	ND	ND	ND	ND	ND	ND	ND	0.0469 AH	ND
10 micron	Groundwater	ND	ND	ND	ND	ND	0.0865 AF	ND	0.311 AH	ND
1 micron	Groundwater	ND	ND	ND	ND	ND	ND	ND	0.0469 AH	ND
0.45 micron	Groundwater	ND	ND	ND	ND	ND	ND	ND	0.0161 AH	ND
0.1 micron	Groundwater	ND	ND	ND	ND	ND	ND	ND	0.0127 AH	ND
10 micron	Additional Effluent	ND	ND	ND	ND	ND	ND	ND	ND	ND
1 micron	Additional Effluent	ND	ND	ND	ND	ND	ND	ND	ND	ND
0.45 micron	Additional Effluent	ND	ND	ND	ND	ND	ND	ND	ND	ND
0.1 micron	Additional Effluent	ND	ND	ND	ND	ND	ND	ND	ND	ND

Notes:
ug/L = Micrograms per Liter
Additional Effluent = Effluent collected from dewatering of a second site sediment material provided by Haley and Aldrich
AH = Aroclor 1262 is being reported as the best aroclor match. The sample exhibits an altered PCB pattern.
AF = Aroclor 1254 is being reported as the best aroclor match. The sample exhibits an altered PCB pattern.

HALEY AND ALDRICH
HASTINGS ON THE HUDSON PHASE II
KEMRON PROJECT No. SH0522-02

Table 10

Water Filtration Evaluations
Summary of Metals Analyses

Sample ID	**Water ID**	**Summary of Metals Analyses**							
		Beryllium ug/L		**Copper ug/L**		**Lead ug/L**		**Zinc ug/L**	
		Total	**Dissolved**	**Total**	**Dissolved**	**Total**	**Dissolved**	**Total**	**Dissolved**
100 micron	Groundwater	< 5.0	< 5.0	4.2 J	**4.2 J**	**5.4**	**3.5 J**	**27.6**	**26.3**
10 micron	Groundwater	< 5.0	< 5.0	**6.6 J**	**4.8 J**	4.7 J	5.9	23.7	31.7
1 micron	Groundwater	< 5.0	< 5.0	**5.1 J**	**5.7 J**	4.3 J	4.9J	37.1	37.4
0.45 micron	Groundwater	< 5.0	< 5.0	**6.3 J**	**4.6 J**	4.8 J	4.2 J	39.3	30.7
0.1 micron	Groundwater	< 5.0	< 5.0	**7.8 J**	**26.3**	5.0	5.8	28.2	37.8

Notes:
Analytical results were provided to KEMRON by Haley and Aldrich
ug/L - Micrograms per liter
J - Estimated concentration detected between the analtytical reporting limit (RL) and the method detection limit (MDL)

HALEY AND ALDRICH
HASTINGS ON THE HUDSON PHASE II
KEMRON PROJECT No. SH0522-02

Table 11

Combined Water Treatment System
Summary of Total PCBs

KEMRON Sample Number	Water ID	PCB Arocolor (ug/L)								
		1016	1221	1232	1242	1248	1254	1260	1262	1268
Untreated	Master Composite	ND	ND	ND	ND	ND	ND	ND	1.34	ND
1 micron	Master Composite	ND	ND	ND	ND	ND	ND	ND	0.0269	ND
F400	Master Composite	ND	ND	ND	ND	ND	ND	ND	ND	ND
Final	Master Composite	ND	ND	ND	ND	ND	ND	ND	ND	ND

Notes:
ug/L = Micrograms per Liter
Master Composite = A 1:1 ratio of sediment effluent water and site groundwater.
ND = Not detected above the analytical Practical Qualitative Limit (PQL)

HALEY AND ALDRICH
HASTINGS ON THE HUDSON PHASE II
KEMRON PROJECT No. SH0522-02

Table 12

Combined Water Treatment System
Summary of Metals Analyses

Sample ID	Water ID	Summary of Metals Analyses							
		Beryllium ug/L		Copper ug/L		Lead ug/L		Zinc ug/L	
		Total	Dissolved	Total	Dissolved	Total	Dissolved	Total	Dissolved
Untreated	Master Comosite	< 1.0	< 1.0	**718**	**423**	< 10.0	< 10.0	**205**	**97.3**
1 Micron	Master Comosite	< 1.0	< 1.0	**405**	**393**	< 10.0	< 10.0	**112**	**99.0**
1 Micron DUP	Master Comosite	< 1.0	< 1.0	**405**	**392**	< 10.0	< 10.0	**111**	**99.4**
F400	Master Comosite	< 1.0	< 1.0	< 5.0	**6.4**	< 10.0	< 10.0	**11.0**	**10.7**
F400 DUP	Master Comosite	< 1.0	< 1.0	**5.6**	**7.2**	< 10.0	< 10.0	**10.8**	**10.7**
Final	Master Comosite	< 1.0	< 1.0	< 5.0	< 5.0	< 10.0	< 10.0	< 10.0	< 10.0

Notes:
Analytical results were provided to KEMRON by Haley and Aldrich
ug/L - Micrograms per liter
J - Estimated concentration detected between the analtytical reporting limit (RL) and the method detection limit (MDL)